

ECE 404-TD / 504-TD

ST: T&D APPLICATIONS OF  
VOLTAGE SOURCE CONVERTERS

SESSION no. 16

|   |   |  |   |  |
|---|---|--|---|--|
| 1 | $-\frac{\pi}{6} < \omega_e t < \frac{\pi}{6}$   |  | $v_{qs}^s = \frac{2}{3}v_i$ $v_{ds}^s = 0$ $i_i = i_{qs}^s$   | $v_{qds}^s = \frac{2}{3}v_i e^{j0}$              |
| 2 | $\frac{\pi}{6} < \omega_e t < \frac{\pi}{2}$    |  | $v_{qs}^s = \frac{v_i}{3}$ $v_{ds}^s = -\frac{v_i}{\sqrt{3}}$ $i_i = \frac{1}{2}i_{qs}^s - \frac{\sqrt{3}}{2}i_{ds}^s$  | $v_{qds}^s = \frac{2}{3}v_i e^{j\frac{\pi}{3}}$  |
| 3 | $\frac{\pi}{2} < \omega_e t < \frac{5\pi}{6}$   |  | $v_{qs}^s = -\frac{v_i}{3}$ $v_{ds}^s = \frac{v_i}{\sqrt{3}}$ $i_i = -\frac{1}{2}i_{qs}^s - \frac{\sqrt{3}}{2}i_{ds}^s$ | $v_{qds}^s = \frac{2}{3}v_i e^{j\frac{2\pi}{3}}$ |
| 4 | $\frac{5\pi}{6} < \omega_e t < \frac{7\pi}{6}$  |  | $v_{qs}^s = -\frac{2}{3}v_i$ $v_{ds}^s = 0$ $i_i = -i_{qs}^s$   | $v_{qds}^s = \frac{2}{3}v_i e^{j\pi}$            |
| 5 | $\frac{7\pi}{6} < \omega_e t < \frac{3\pi}{2}$  |  | $v_{qs}^s = -\frac{v_i}{3}$ $v_{ds}^s = \frac{v_i}{\sqrt{3}}$ $i_i = -\frac{1}{2}i_{qs}^s + \frac{\sqrt{3}}{2}i_{ds}^s$ | $v_{qds}^s = \frac{2}{3}v_i e^{j\frac{4\pi}{3}}$ |
| 6 | $\frac{3\pi}{2} < \omega_e t < \frac{11\pi}{6}$ |  | $v_{qs}^s = \frac{v_i}{3}$ $v_{ds}^s = \frac{v_i}{\sqrt{3}}$ $i_i = \frac{1}{2}i_{qs}^s + \frac{\sqrt{3}}{2}i_{ds}^s$   | $v_{qds}^s = \frac{2}{3}v_i e^{j\frac{5\pi}{3}}$ |

Handwritten notes on the right side of the page:

$$\frac{2}{3}v_i$$

$$- \frac{v_{dc}}{6}$$

$$+ \frac{v_{dc}}{2}$$

$$- \frac{v_{dc}}{6}$$

$$+ \frac{v_{dc}}{2}$$

$$- \frac{v_{dc}}{6}$$

$$+ \frac{v_{dc}}{2}$$

Figure 3.1 d,q equations for the six modes of a VSI

$$V_{60} = \frac{2}{3} \left[ \frac{1}{2} \left( \frac{V_{dc}}{2} \right) + \frac{1}{2} \left( -\frac{V_{dc}}{2} \right) + \frac{1}{2} \left( -\frac{V_{dc}}{2} \right) \right]$$

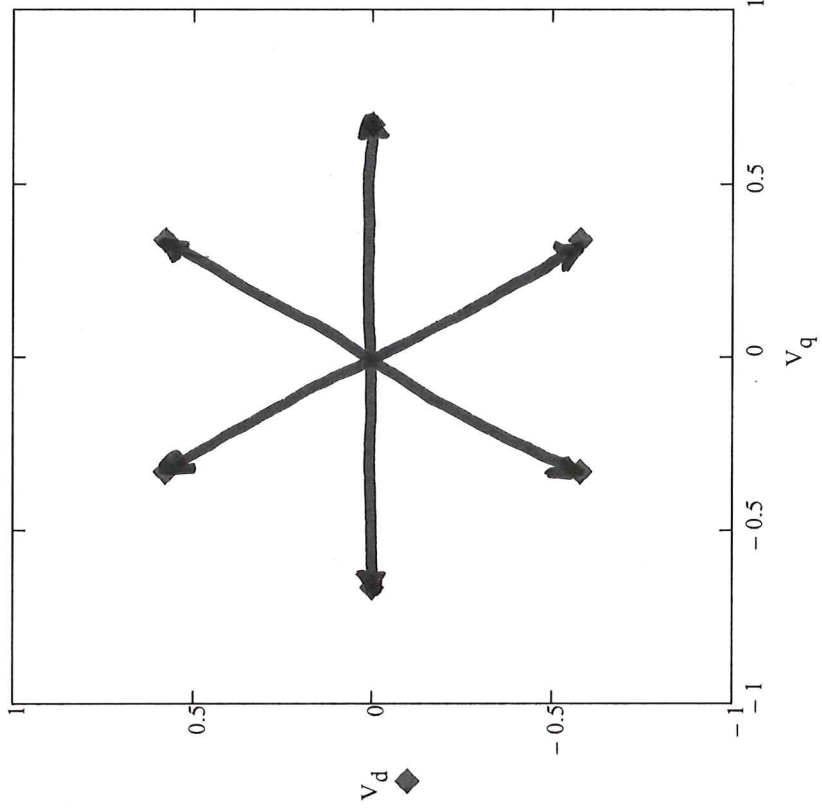
$$V_{60} = \frac{2}{3} \cdot \frac{1}{2} \left[ -\frac{V_{dc}}{2} \right]$$

$$V_{60} = -\frac{V_{dc}}{6}$$

# Voltage Sourced Converter: Space Vectors, Two-Level

$$V_q := \begin{pmatrix} \frac{2}{3} & \frac{1}{3} & \frac{1}{3} & \frac{2}{3} & \frac{1}{3} & \frac{1}{3} \end{pmatrix}$$

$$V_d := \begin{pmatrix} 0 & \frac{1}{\sqrt{3}} & \frac{1}{\sqrt{3}} & 0 & \frac{1}{\sqrt{3}} & \frac{1}{\sqrt{3}} \end{pmatrix}$$

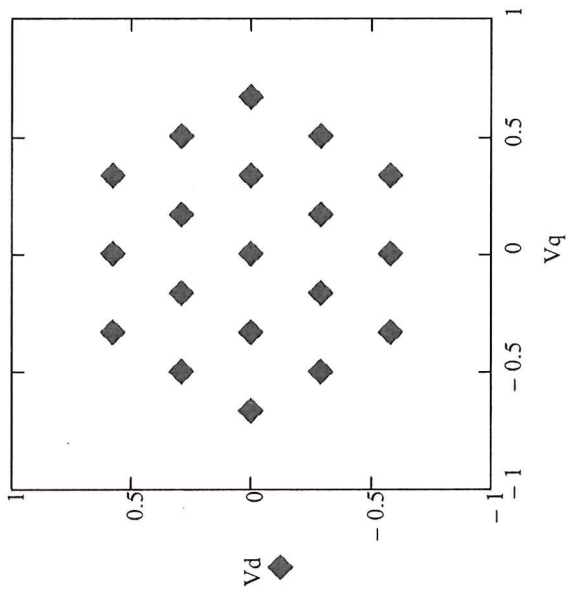


$$\begin{pmatrix}
 0 \\
 -0.288675135 \\
 -0.577350269 \\
 -0.577350269 \\
 -0.577350269 \\
 -0.288675135 \\
 0 \\
 0.288675135 \\
 0.577350269 \\
 0.577350269 \\
 0.577350269 \\
 0.288675135 \\
 0 \\
 -0.288675135 \\
 -0.288675135 \\
 0.288675135 \\
 0.288675135 \\
 0 \\
 -0.288675135 \\
 -0.288675135 \\
 0 \\
 0.288675135 \\
 0.288675135 \\
 0 \\
 0 \\
 0
 \end{pmatrix}$$

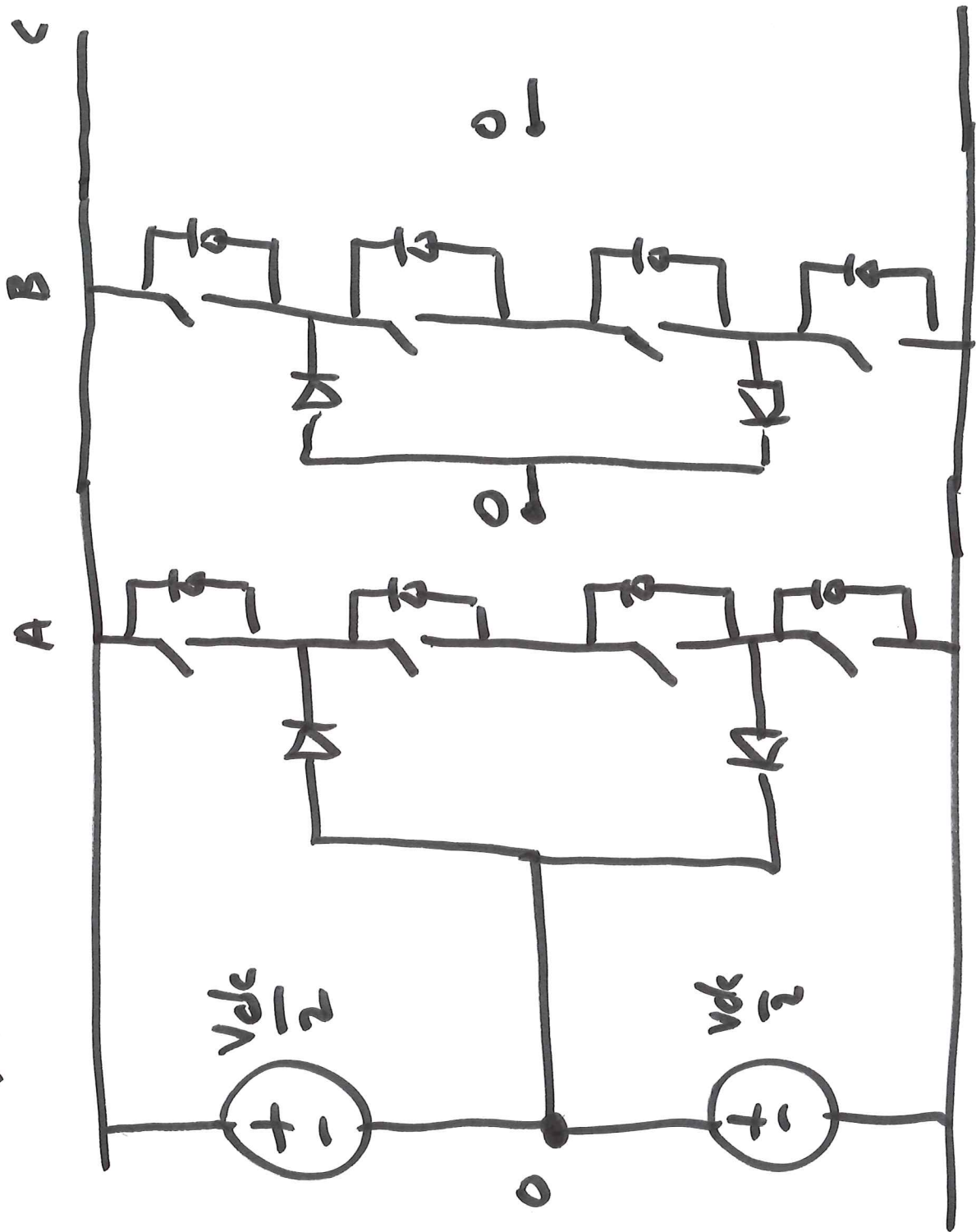
Vd :=

$$\begin{pmatrix}
 0.666666667 \\
 0.5 \\
 0.333333333 \\
 0 \\
 -0.333333333 \\
 -0.5 \\
 -0.666666667 \\
 -0.5 \\
 -0.333333333 \\
 0 \\
 0.333333333 \\
 0.5 \\
 0.333333333 \\
 0.166666667 \\
 -0.166666667 \\
 -0.333333333 \\
 -0.166666667 \\
 0.166666667 \\
 0.333333333 \\
 0.166666667 \\
 -0.166666667 \\
 -0.333333333 \\
 -0.166666667 \\
 0.166666667 \\
 0 \\
 0 \\
 0
 \end{pmatrix}$$

Vq :=



$$V_{ck} = 0, \quad -\frac{V_{dc}}{2}$$





| Va <sub>n</sub> | Vb <sub>n</sub> | Vc <sub>n</sub> | Vq <sub>n</sub> | Vd <sub>n</sub> | Von        |
|-----------------|-----------------|-----------------|-----------------|-----------------|------------|
|                 |                 |                 |                 |                 |            |
| 0.5             | -0.5            | -0.5            | 0.6666667       | 0               | -0.3333333 |
| 0.5             | 0               | -0.5            | 0.5             | -0.2886751      | 0          |
| 0.5             | 0.5             | -0.5            | 0.3333333       | -0.5773503      | 0.3333333  |
| 0               | 0.5             | -0.5            | 0               | -0.5773503      | 0          |
| -0.5            | 0.5             | -0.5            | -0.3333333      | -0.5773503      | -0.3333333 |
| -0.5            | 0.5             | 0               | -0.5            | -0.2886751      | 0          |
| -0.5            | 0.5             | 0.5             | -0.6666667      | 0               | 0.3333333  |
| -0.5            | 0               | 0.5             | -0.5            | 0.2886751       | 0          |
| -0.5            | -0.5            | 0.5             | -0.3333333      | 0.5773503       | -0.3333333 |
| 0               | -0.5            | 0.5             | 0               | 0.5773503       | 0          |
| 0.5             | -0.5            | 0.5             | 0.3333333       | 0.5773503       | 0.3333333  |
| 0.5             | -0.5            | 0               | 0.5             | 0.2886751       | 0          |
| 0               | -0.5            | -0.5            | 0.3333333       | 0               | -0.6666667 |
| 0               | 0               | -0.5            | 0.1666667       | -0.2886751      | -0.3333333 |
| -0.5            | 0               | -0.5            | -0.1666667      | -0.2886751      | -0.6666667 |
| -0.5            | 0               | 0               | -0.3333333      | 0               | -0.3333333 |
| -0.5            | -0.5            | 0               | -0.1666667      | 0.2886751       | -0.6666667 |
| 0               | -0.5            | 0               | 0.1666667       | 0.2886751       | -0.3333333 |
| 0.5             | 0               | 0               | 0.3333333       | 0               | 0.3333333  |
| 0.5             | 0.5             | 0               | 0.1666667       | -0.2886751      | 0.6666667  |
| 0               | 0.5             | 0               | -0.1666667      | -0.2886751      | 0.3333333  |
| 0               | 0.5             | 0.5             | -0.3333333      | 0               | 0.6666667  |
| 0               | 0               | 0.5             | -0.1666667      | 0.2886751       | 0.3333333  |
| 0               | -0.5            | 0               | 0.1666667       | 0.2886751       | -0.3333333 |
| 0.5             | 0.5             | 0.5             | 0               | 0               | 1          |
| 0               | 0               | 0               | 0               | 0               | 0          |
| -0.5            | -0.5            | -0.5            | 0               | 0               | -1         |



## EXAMPLES

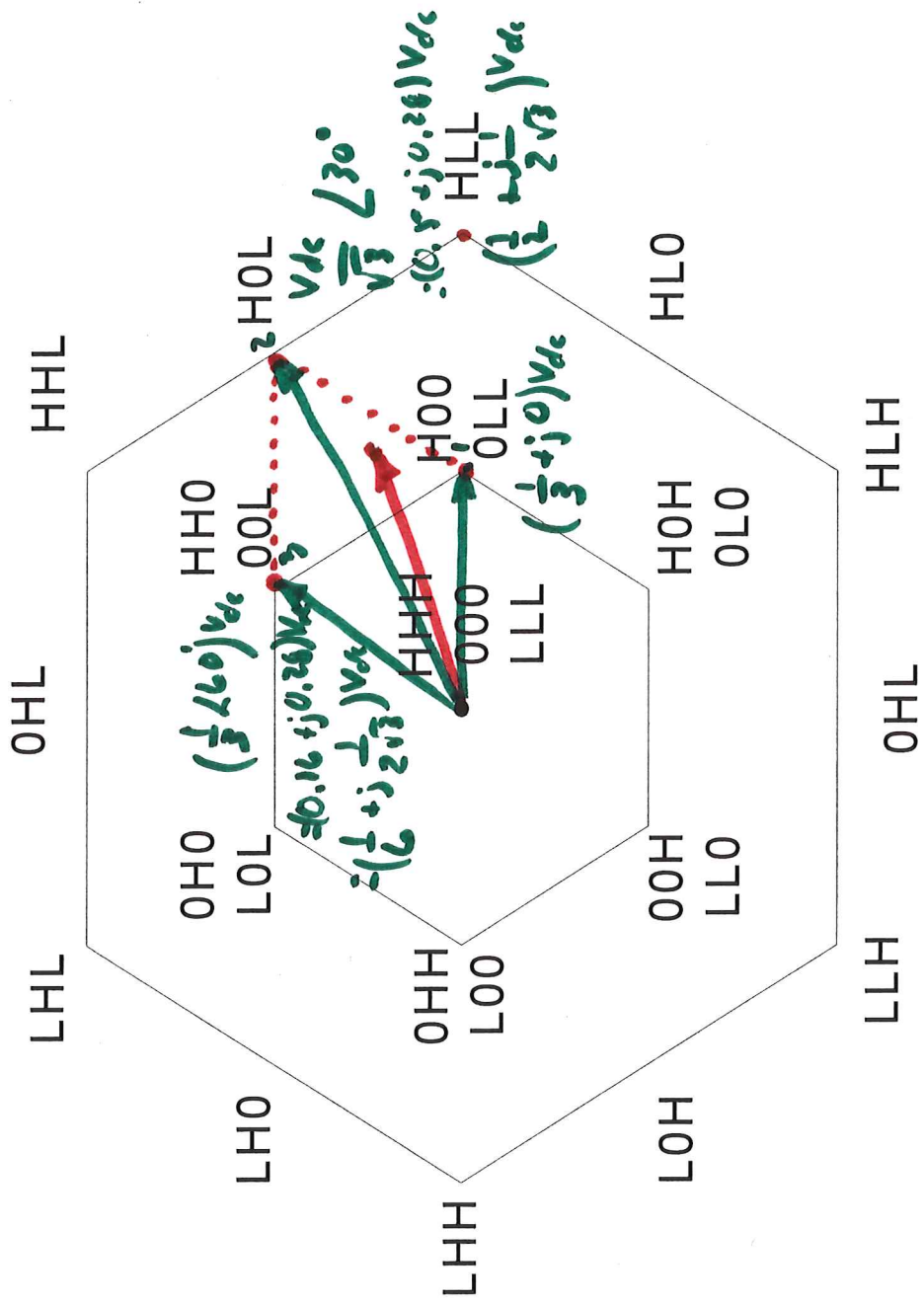
• USE A MULTISIM

CONVERSION TO SYNTHESIS

A VECTOR  $V_X = 0.4 V_{dc} \angle 25^\circ$

$$V_X = (0.363 + j0.169) V_{dc}$$

FIND SOME VECTORS



$$V_1 = (0.333 + j0) V_{dc}$$

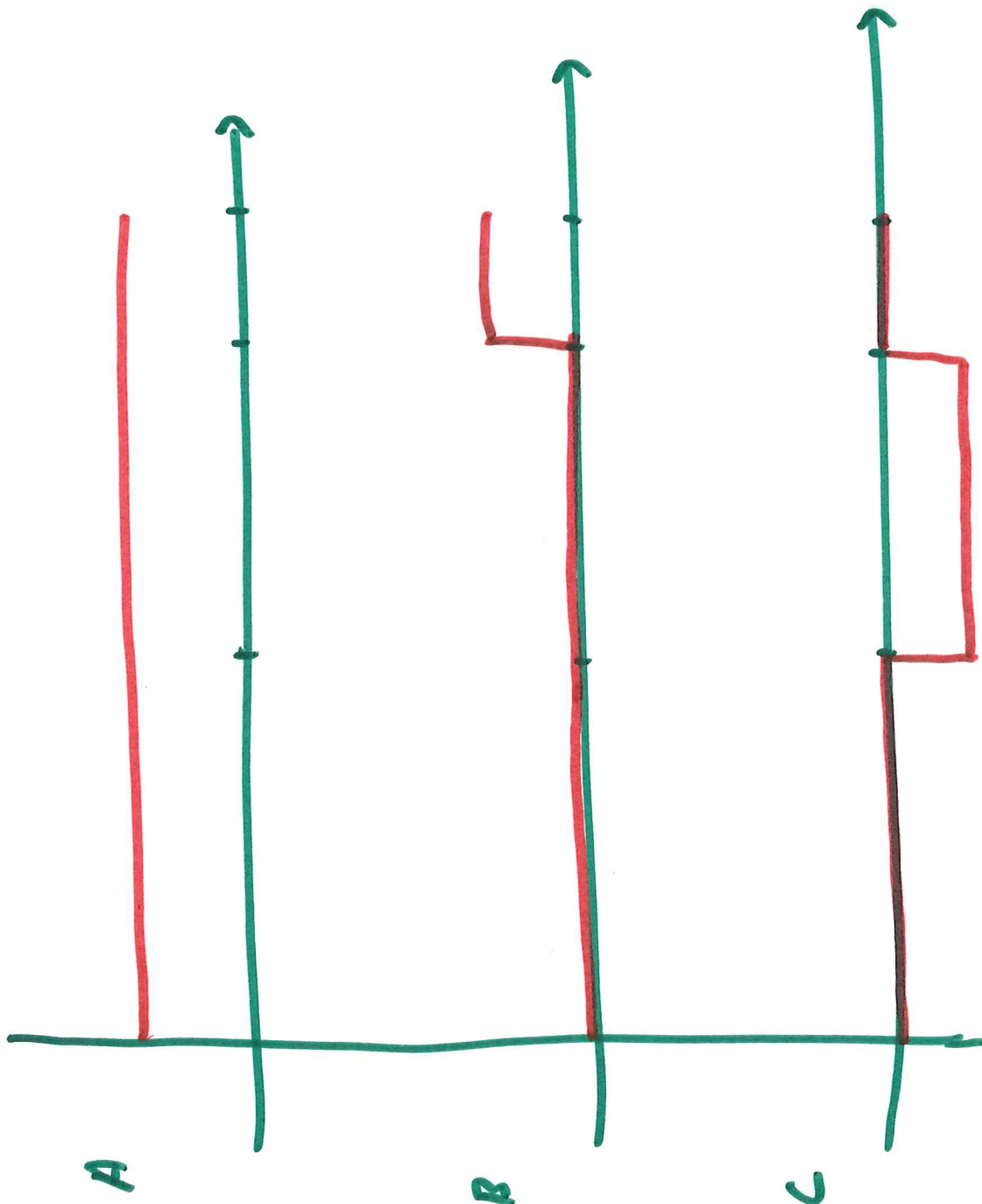
$$V_2 = (0.50 + j0.289) V_{dc}$$

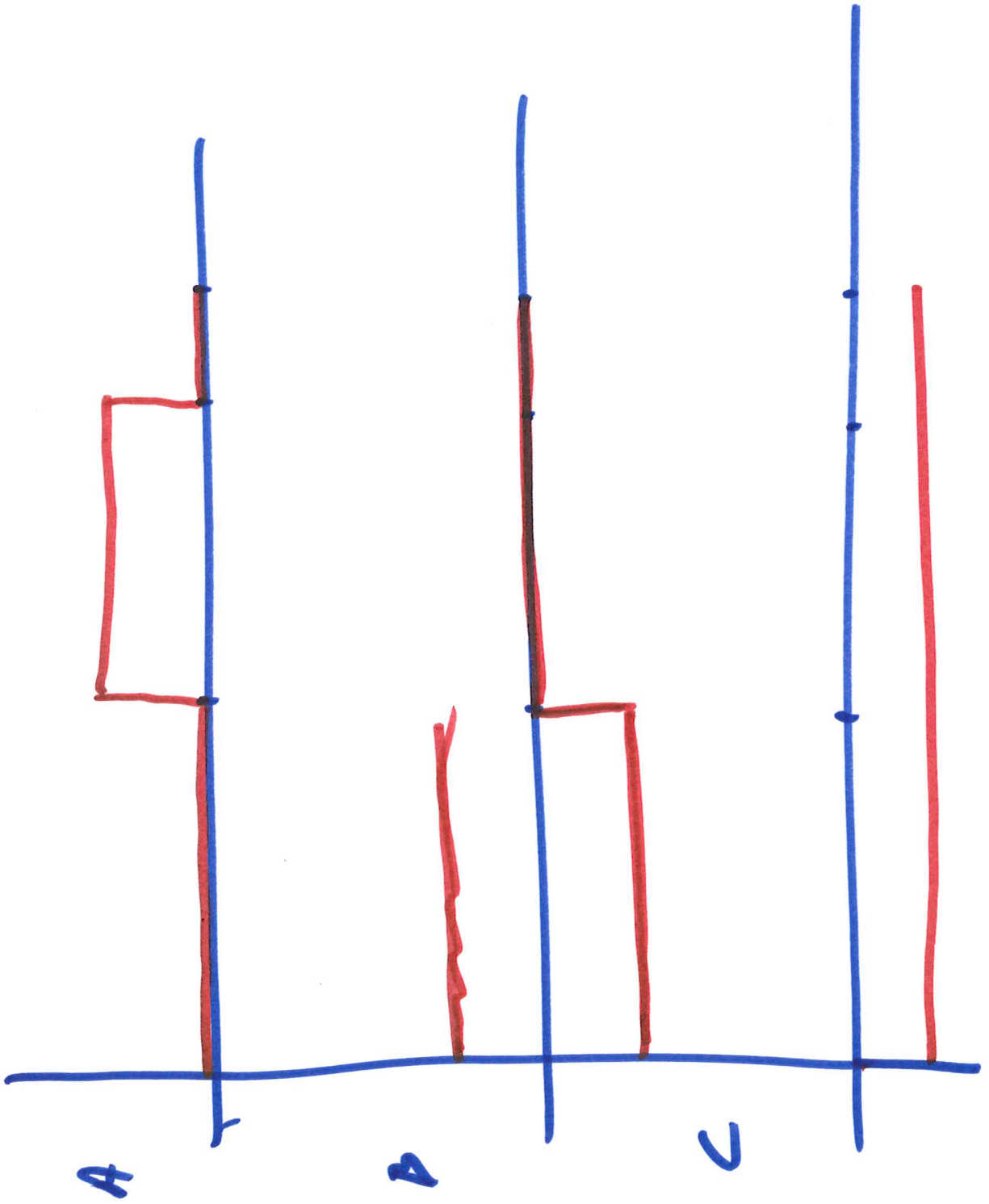
$$V_3 = (0.167 + j0.299) V_{dc}$$

$$\begin{bmatrix} \operatorname{Re}(v_1) & \operatorname{Re}(v_2) & \operatorname{Re}(v_3) \\ \operatorname{Im}(v_1) & \operatorname{Im}(v_2) & \operatorname{Im}(v_3) \\ 1 & 1 & 1 \end{bmatrix} \begin{bmatrix} t_1 \\ t_2 \\ t_3 \end{bmatrix} = \begin{bmatrix} \operatorname{Re}(V_{ref}) \\ \operatorname{Im}(V_{ref}) \\ 1 \end{bmatrix}$$

$$\begin{bmatrix} t_1 \\ t_2 \\ t_3 \end{bmatrix} = \begin{bmatrix} 0.415 \\ 0.379 \\ 0.207 \end{bmatrix}$$

|   |   |   |   |   |   |   |
|---|---|---|---|---|---|---|
| 1 | H | D | D | 0 | L | L |
| 2 | H | O | L | H | O | L |
| 3 | H | A | O | O | O | L |





**ECE 404 / 504**

**T & D Applications of Voltage  
Sourced Converters**

**Lesson 16**

**Ref: Dynamics of Electrical  
Drives by Novotny and Lipo**