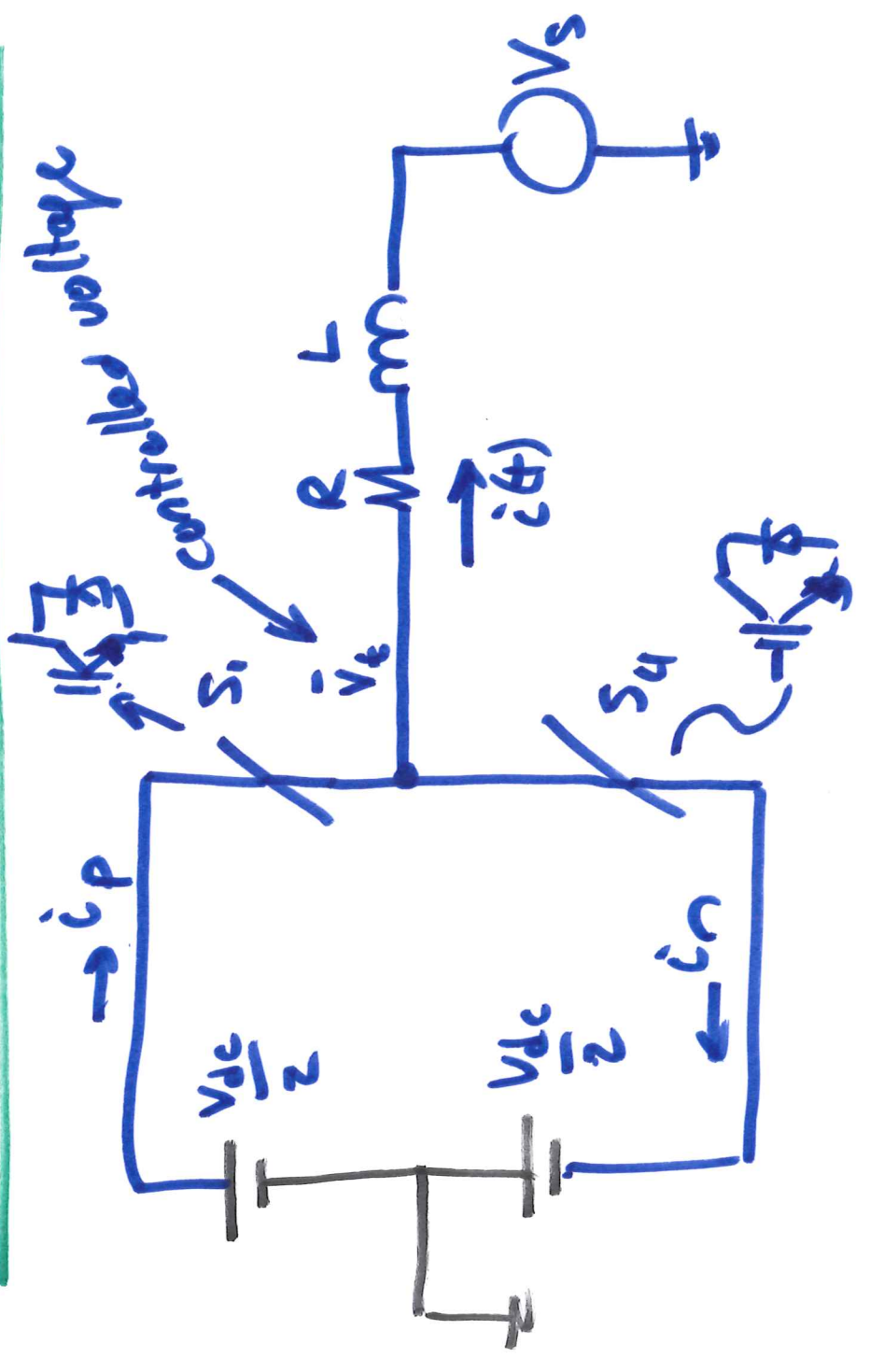


ECE 404-TD / 504-TD

ST: T&D APPLICATIONS OF
VOLTAGE SOURCE CONVERTERS

SESSION no. 29

Averaged Models of Power Converters



$$i(t) \rightarrow v_f(t) - v_s(t) = R i(t) + L \frac{di}{dt}$$

~~$v_f(t)$~~

$$v_f = \frac{1}{T_s} \int_0^{T_s} v_f(\tau) d\tau + \sum_{h=1}^{\infty} a_h \cos(h\omega t) + b_h \sin(h\omega t)$$

harmonics

$$L \frac{d\bar{i}}{dt} + R\bar{i} = \frac{1}{T_s} \int_0^{T_s} v_4(\tau) d\tau - V_s$$

$$L \frac{d\tilde{i}}{dt} + R\tilde{i} = \sum_{h=1}^{\infty} a_h \cos(h\omega_s t) + b_h \sin(h\omega_s t) - V_s$$

- 2 equations to find components
of current

→ for most applications the
part with harmonics isn't a concern

Goal - design a controller
to regulate \bar{I}

→ don't want details of
switching behavior, want
the averaged behavior

Switching functions

Switch 1 $\rightarrow \bar{S}_1 = d$

contributes

$d \cdot V_{dc} \rightarrow V_t$

Switch 4 $\bar{S}_4 = (-d)$

contributes $-(-d) \cdot V_{dc} \rightarrow V_t$

Based on the above discussion

- to get output

$$\bar{V}_f = d \frac{V_{dc}}{2} - (1-d) \frac{V_{dc}}{2}$$

$$= \frac{V_{dc}}{2} (2d-1)$$

$$\bar{I}_p = d \cdot i_c$$

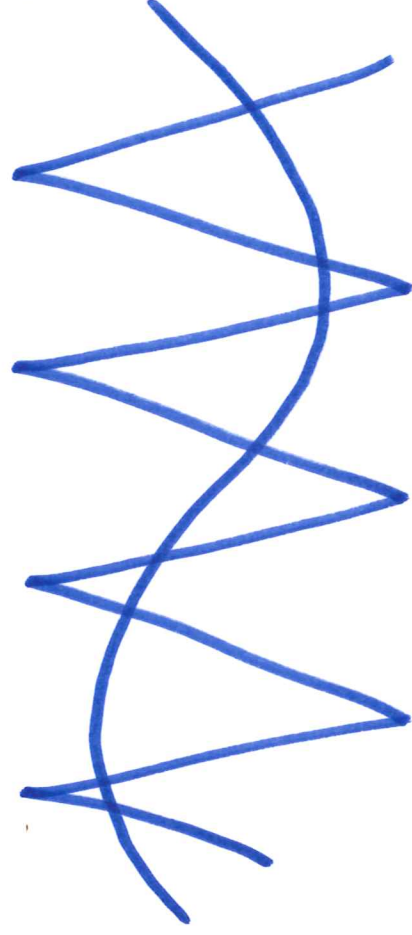
$$\bar{I}_n = (1-d) i_c$$

$$P_{DC} = \frac{V_{dc}}{2} (i_p - i_n) = \frac{V_{dc}}{2} (2d-1) i_c$$

$$P_t = V_f \bar{i} = \frac{V_{dc}}{2} (2d-1)$$

AC side switch \rightarrow No converter losses

If we define our switching based on carrier



$$m = 2d - 1$$

$$V_f = m V_{dc} \frac{2}{\pi}$$

$$i_p = (m+1) \frac{2}{\pi} ?$$

$$i_n = (1-m) \frac{2}{\pi} ?$$

$$P_{dc} = P_i = m \frac{V_{dc}}{2} i$$

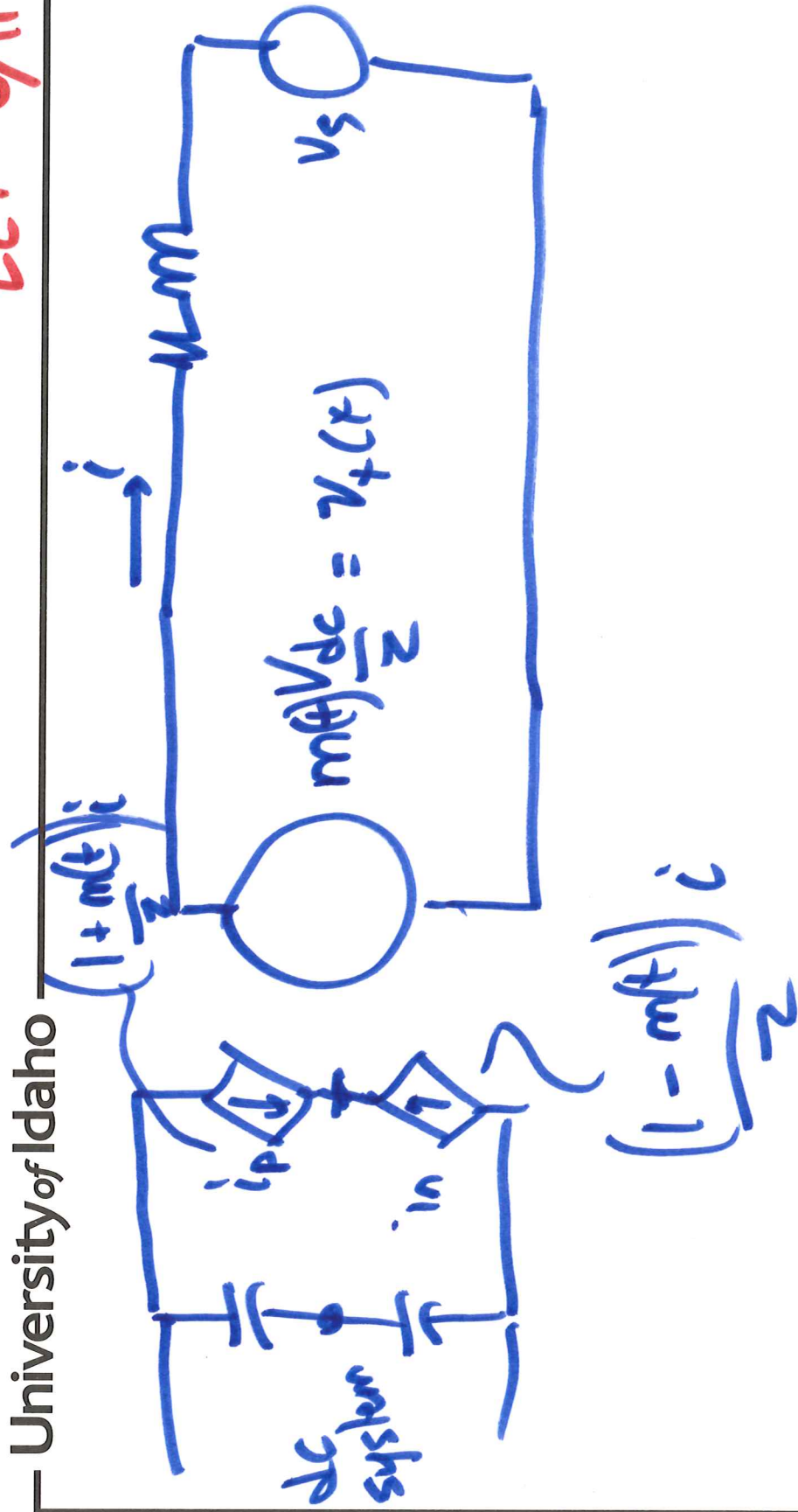


→ m can be (1) constant, quasi dc value

(2) sinusoidal reference



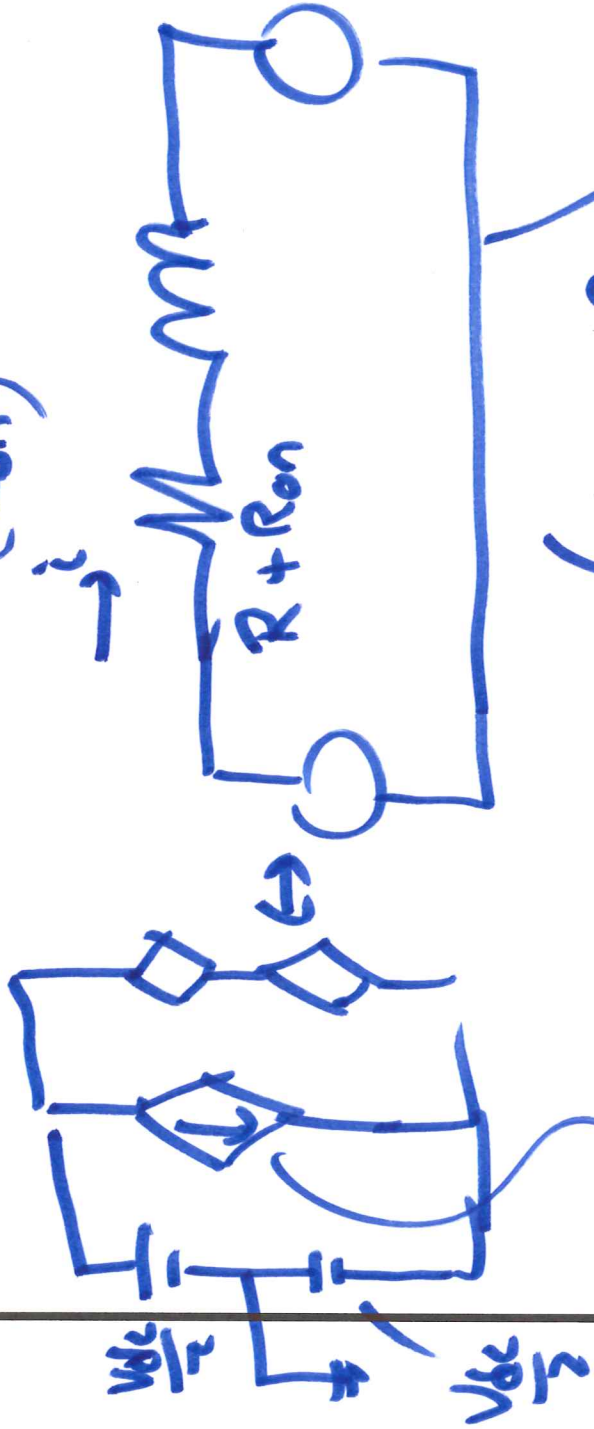
$$\sqrt{2} |V| \cos(\omega t + \phi)$$



Adding losses in converter

→ conduction losses

(R_{on})



switching losses $\left(\frac{Q_{rr} + Q_{fc}}{T_s} \right) \cdot V_{dc}$

in most cases these are neglected

fig 2.17 in text

AC Current regulation (inner control)

- inner control loop is a current regulator
- Outer control determines commands

