

ECE 404-TD / 504-TD

ST: T&D APPLICATIONS OF
VOLTAGE SOURCE CONVERTERS

SESSION no. 33

1. Implement a 3 ϕ VSC
 - averaged model } open loop control
 - switch model }

In ATP or EMTOC - measure P, Q

2. Given commands for P, Q or change in V_{dc} & θ_{ac}
 - determine current set points $I_{a^*}, I_{d^*}, I_{B^*}$ or i_{d^*}, i_{q^*}

3. ECE 504 students: closed loop control of NPC converter in ATP/EMTOC

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Three Phase VSC Locked Loop (PLL)

Cases where synchronization is needed

- Non-PWM switching schemes
- Synchronous PWM switching schemes
- When control loop operates in the synchronous DQ reference frame
- Control loop for α - β may or may not need synchronizing reference
 - Frequency comes along with measured α and β terms
 - May need depending on method for determining current references

Park's Transform Based (PLL) → commonly applied scheme for tracking frequency of a measured signal

- Measured voltages

$$v_{sd} = V_s \cdot \cos(\omega_0 \cdot t + \theta_0 - \rho(t))$$

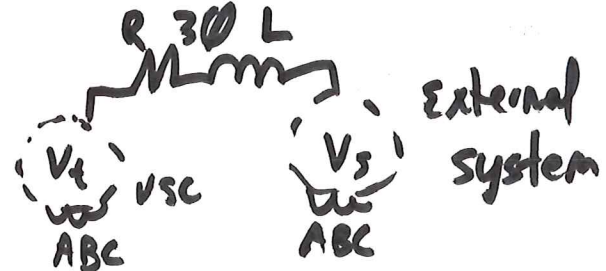
$$v_{sq} = V_s \cdot \sin(\omega_0 \cdot t + \theta_0 - \rho(t))$$

rot. reference

- Output current equations in transformed domain

$$L \cdot \left(\frac{d}{dt} i_d \right) = L \cdot \omega(t) \cdot i_q - (R + r_{on}) \cdot i_d + (v_{td} - v_{sd})$$

$$L \cdot \left(\frac{d}{dt} i_q \right) = L \cdot \omega(t) \cdot i_d - (R + r_{on}) \cdot i_q + (v_{tq} - v_{sq})$$



switching device resistance - conduction loss

- The choice of $\rho(t)$ makes a big difference. If it 0, stay in α - β frame (no rotation)
- In this case we want:

$$\rho(t) = \omega_0 \cdot t + \theta_0$$

or another angle

- Then $\frac{d}{dt} \rho(t) = \omega_0$

- If this is the case, then

$$v_{sq} = 0 \quad \text{and} \quad v_{sd} = V_s$$

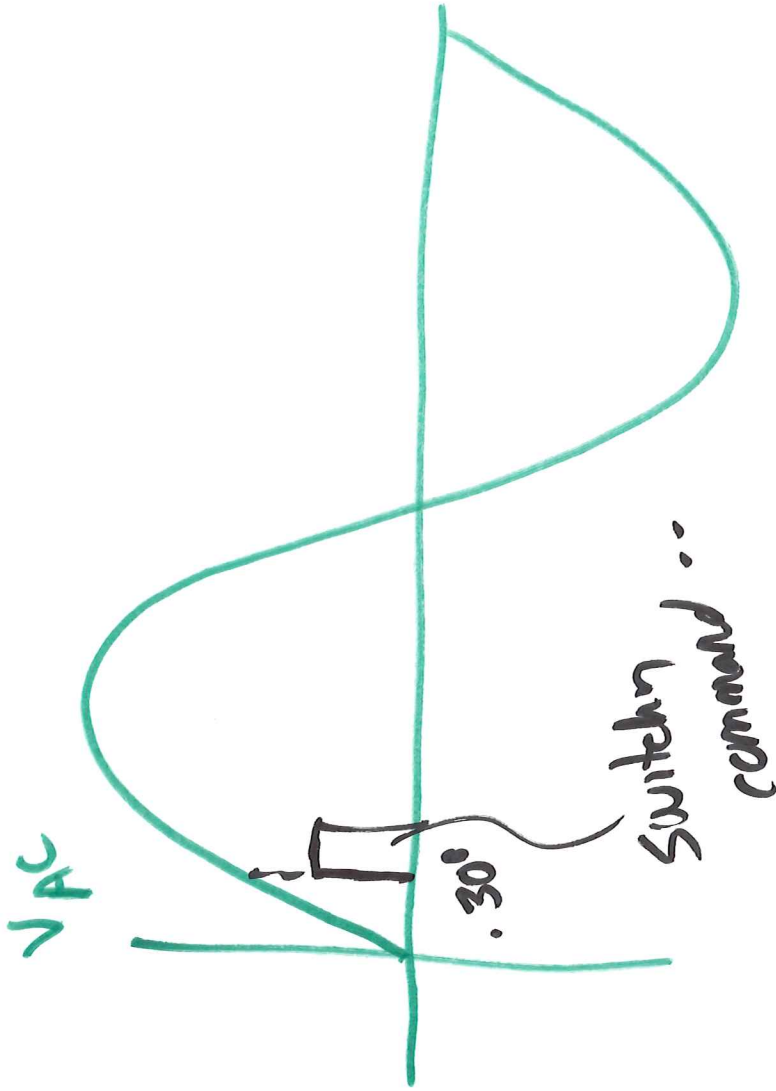
- Design a feedback controller to regulate v_{sq} to be 0

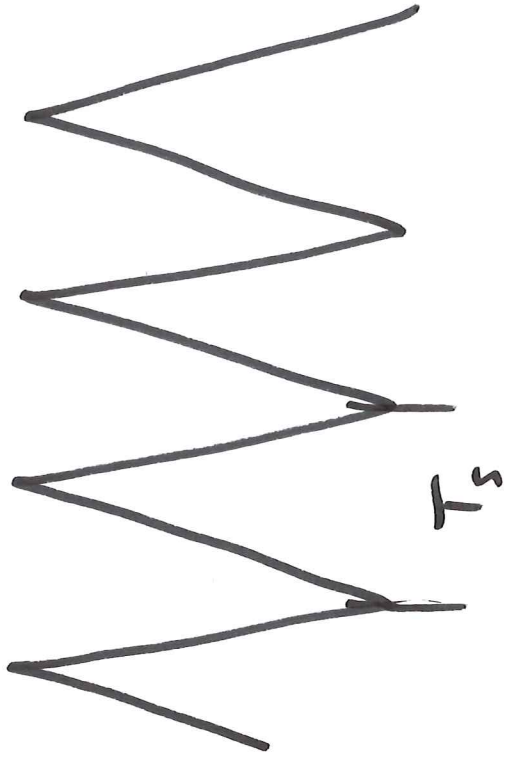
$$\omega(t) = H(p) \cdot v_{sq}(t) \quad \text{where} \quad H(p) \text{ is a linear transfer function}$$

Von of the device ignored because small

Use voltage synchronizing to as reference

Vs is a space phase





$$f_s = \frac{1}{T_s}$$

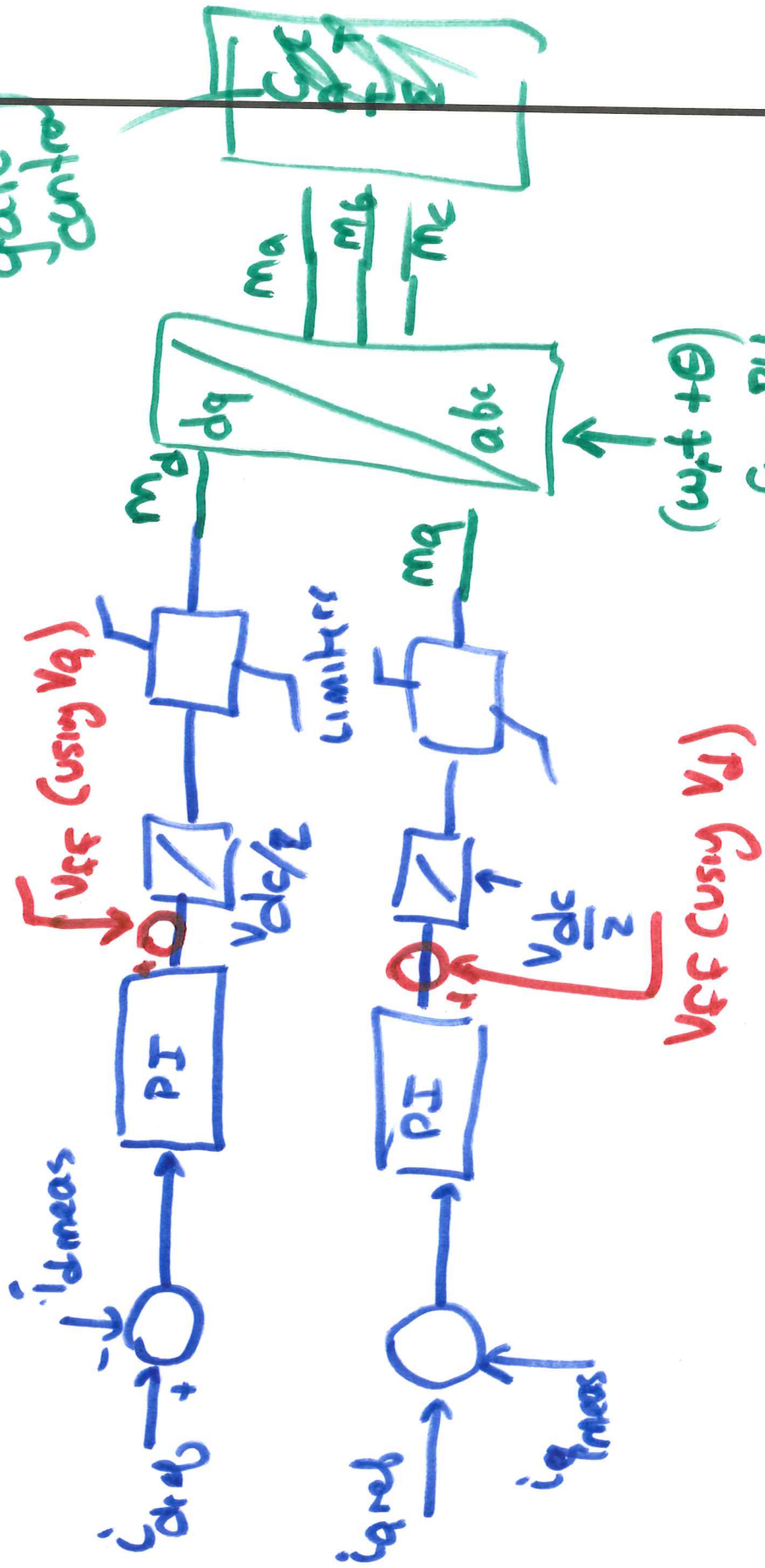
for relatively low
Pwm frequencies

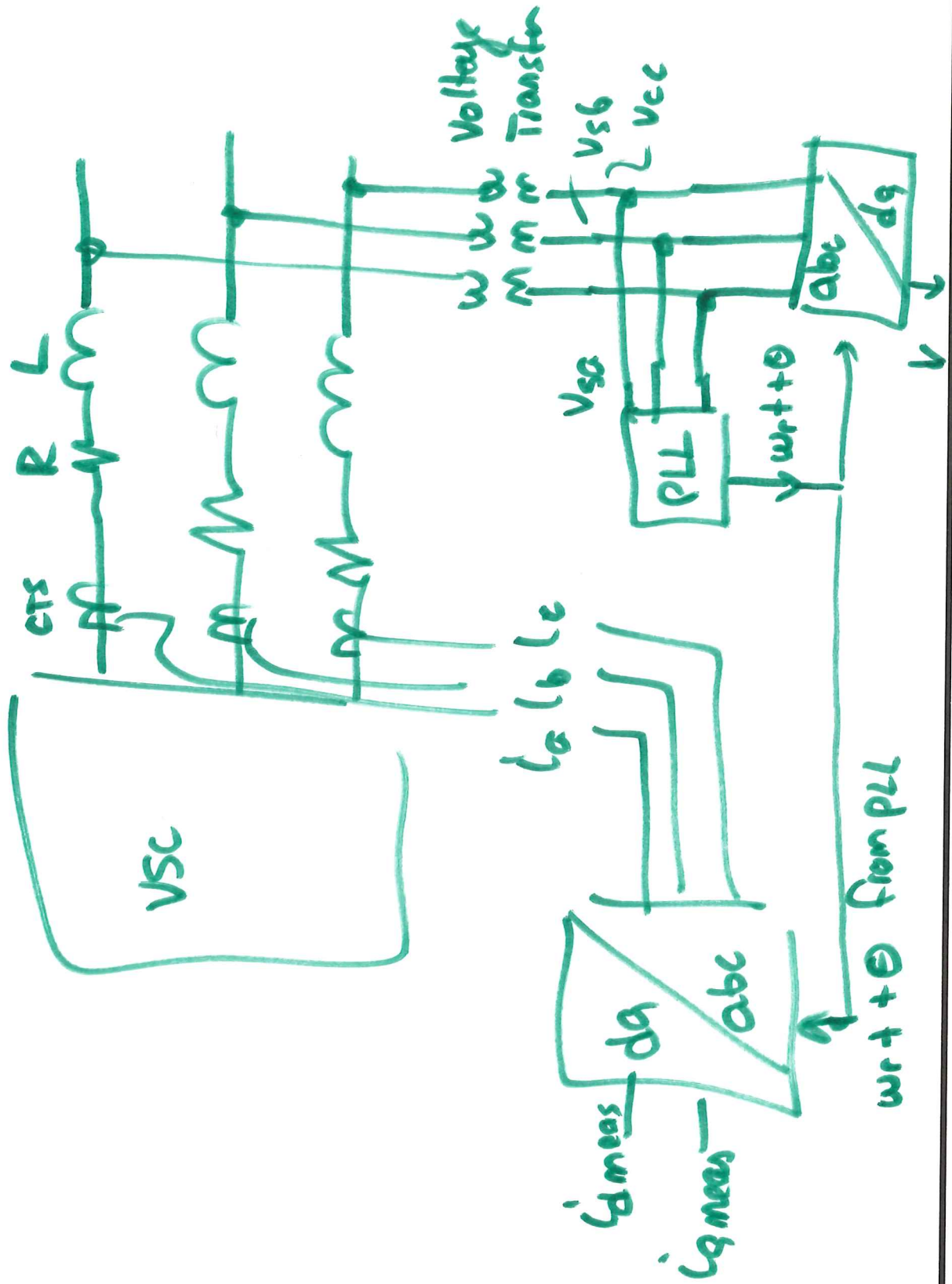
to have integer

$$f_s = n f_0$$

Power system freq

3rd VSC controller (inner)



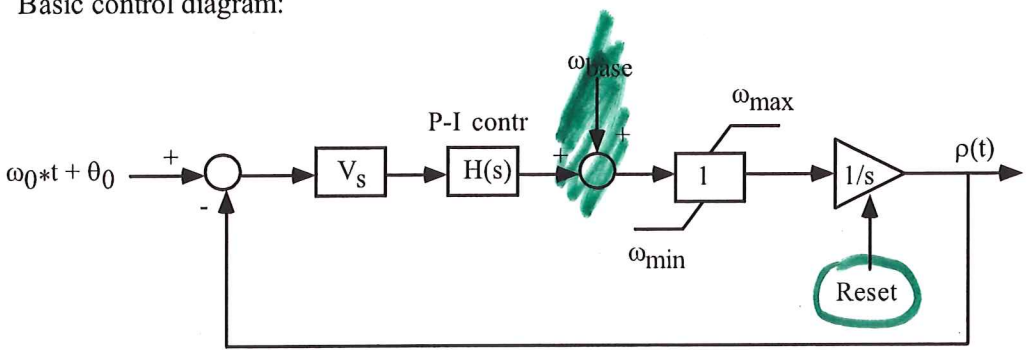


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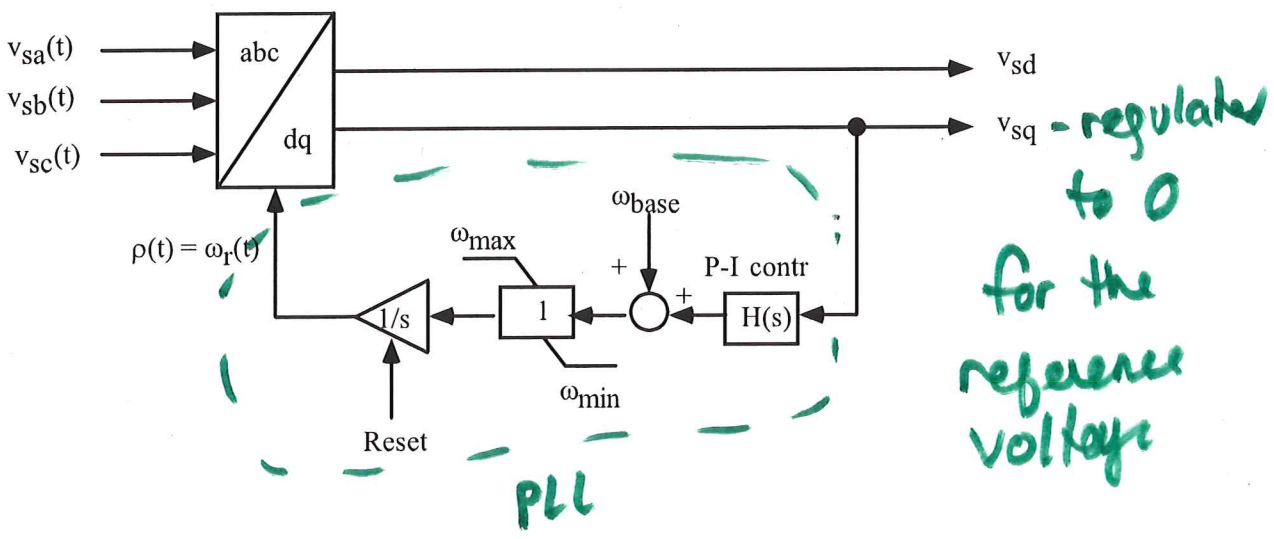
- Start it out from $\omega(0) = \omega_0$
- Limit frequency range to narrow variation from $\omega_{min} < \omega < \omega_{max}$
- Small frequency variations imply $\sin(\omega_0 \cdot t + \theta_0 - \rho(t))$ approximately $(\omega_0 \cdot t + \theta_0 - \rho(t))$ which simplifies control loop design

$$\frac{d}{dt} \rho(t) = V_s \cdot H(p) \cdot (\omega_0 \cdot t + \theta_0 - \rho(t))$$

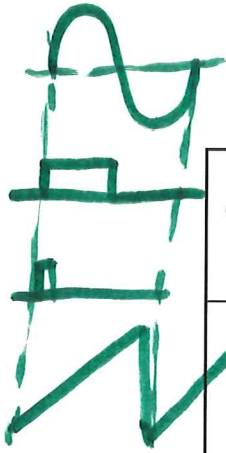
- Basic control diagram:



- Three phase implementation:



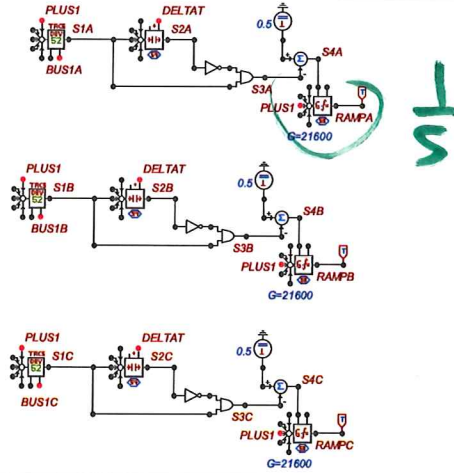
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ATPDraw Implementation: Simple Zero Crossing Based : Three Phase

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Synchronization

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Phase Correction

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- Create an orthogonal pair of vectors
 - » Park's transformation if three phase measurement
 - » Phase rotation (delay) if single phase input
- Need instantaneous angle reference ($\omega_r t = \theta_r$)
- Phase Error = $-V_d \sin(\theta_r) + V_q \cos(\theta_r)$

Synchronization

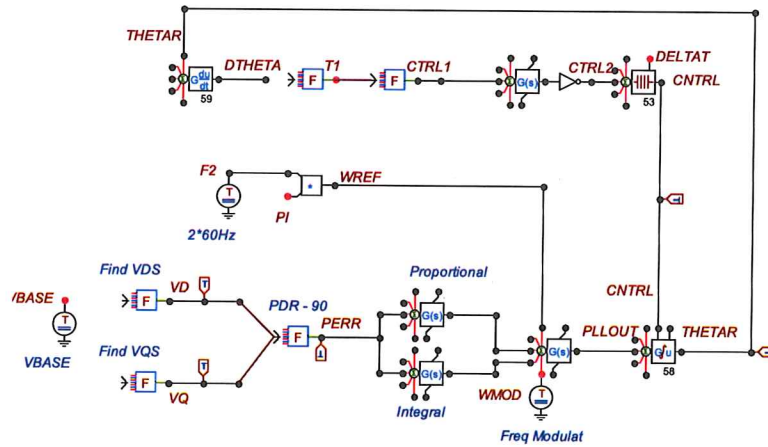
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U_I ATPDraw Implementation: Phase Locked Loop: Phase A

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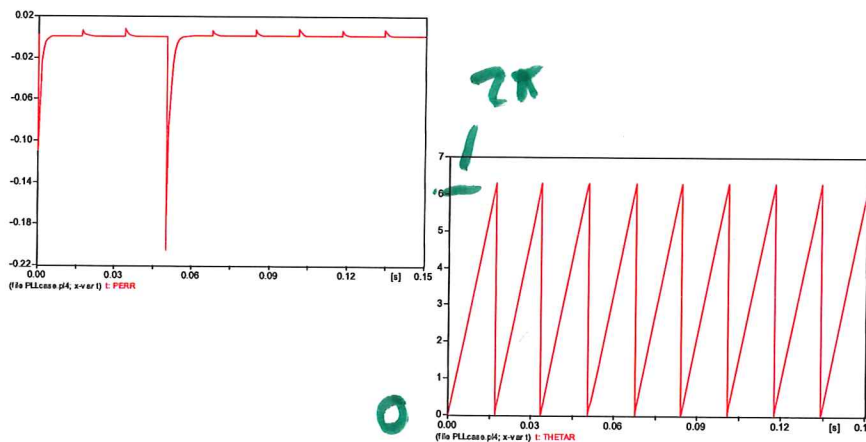
Synchronization

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U_I PERR and THETAR with phase jump due to load change

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Synchronization

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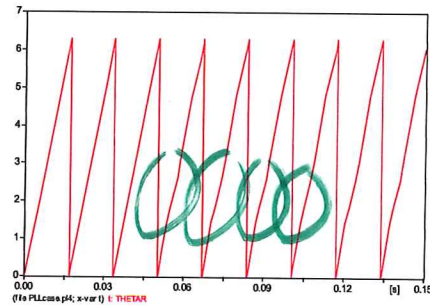
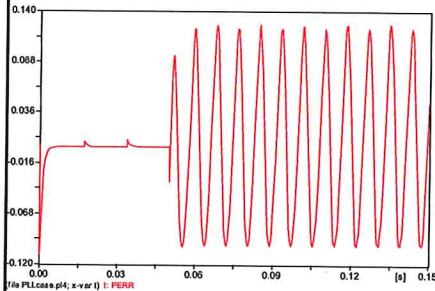
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PERR and THETAR with sustained SLG Fault

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Synchronization

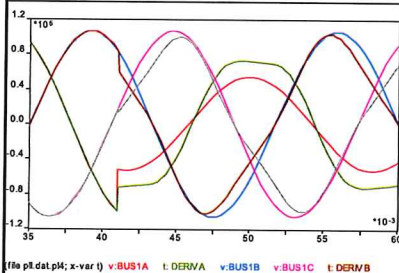
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Results with PLL--SLG Fault

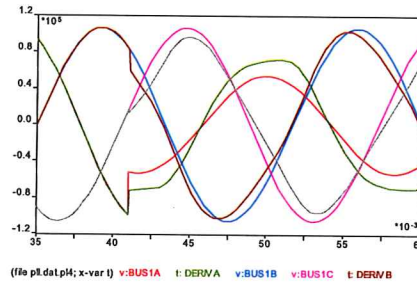
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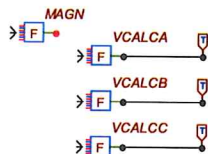
$K_p=100, T_i=8.3E-3$

$-\frac{1}{k_i}$

$K_p=1000, T_i=8.3E-4$



Response Example



Synchronization

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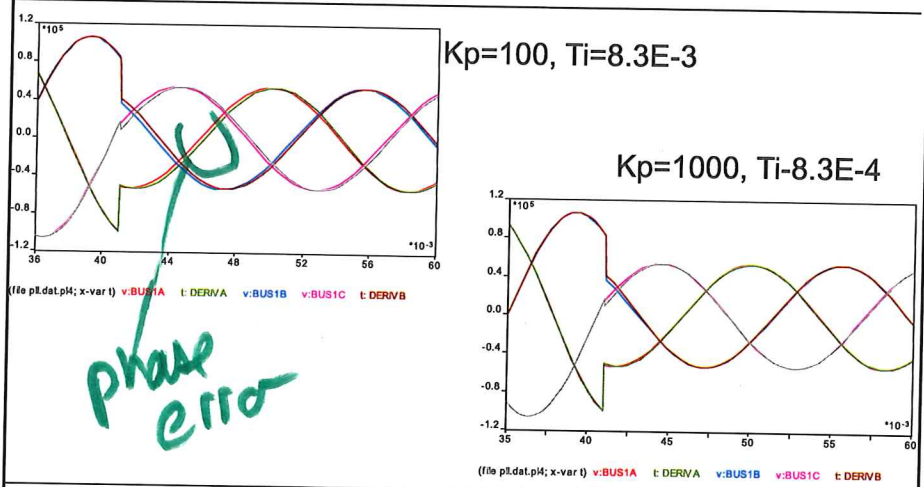
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Results with PLL-- Three Phase Fault

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Compare ωt with PLL THETAR (phase jump case)

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