

## Line Constants for Untransposed and Transposed Lines

### A. Original Case

AC Resistance from table:

$$R_{ac} := 0.278 \frac{\text{ohm}}{\text{mi}} \quad \text{at 25 C and} \quad \text{freq} := 60\text{Hz}$$

$$\mu_0 := 4 \cdot \pi \cdot 10^{-7} \frac{\text{H}}{\text{m}} \quad \rho := 100 \text{ohm} \cdot \text{m} \quad \text{Conductor GMR from table:}$$

$$D_s := 0.01668 \text{ft}$$

$$\text{CarsonsResistConst} := 9.869 \times 10^{-7} \frac{\text{ohm}}{\text{m} \cdot \text{Hz}}$$

$$R_d := \text{CarsonsResistConst} \cdot \text{freq} \quad R_d = 0.0953 \cdot \frac{\text{ohm}}{\text{mi}}$$

$$R_{\text{self}} := R_{ac} + R_d \quad R_{\text{self}} = 0.3733 \cdot \frac{\text{ohm}}{\text{mi}}$$

$$R_{\text{perlength}} := \begin{pmatrix} R_{\text{self}} & R_d & R_d \\ R_d & R_{\text{self}} & R_d \\ R_d & R_d & R_{\text{self}} \end{pmatrix}$$

$$R_{\text{perlength}} = \begin{pmatrix} 0.3733 & 0.0953 & 0.0953 \\ 0.0953 & 0.3733 & 0.0953 \\ 0.0953 & 0.0953 & 0.3733 \end{pmatrix} \cdot \frac{\text{ohm}}{\text{mi}}$$

$$D_{e\_const} := 2160 \cdot \frac{\text{ft} \cdot \text{Hz}^{0.5}}{(\text{ohm} \cdot \text{m})^{0.5}}$$

$$D_e := D_{e\_const} \sqrt{\frac{\rho}{\text{freq}}} \quad D_e = 2.7885 \times 10^3 \cdot \text{ft}$$

$$D_{ab} := 10\text{ft} \quad D_{ac} := 20\text{ft} \quad D_{bc} := 10\text{ft}$$

$$L_{\text{perlength}} := \frac{\mu_0}{2 \cdot \pi} \cdot \begin{pmatrix} \ln\left(\frac{D_e}{D_s}\right) & \ln\left(\frac{D_e}{D_{ab}}\right) & \ln\left(\frac{D_e}{D_{ac}}\right) \\ \ln\left(\frac{D_e}{D_{ab}}\right) & \ln\left(\frac{D_e}{D_s}\right) & \ln\left(\frac{D_e}{D_{bc}}\right) \\ \ln\left(\frac{D_e}{D_{ac}}\right) & \ln\left(\frac{D_e}{D_{bc}}\right) & \ln\left(\frac{D_e}{D_s}\right) \end{pmatrix}$$

$$L_{\text{perlength}} = \begin{pmatrix} 3.8711 & 1.8123 & 1.5892 \\ 1.8123 & 3.8711 & 1.8123 \\ 1.5892 & 1.8123 & 3.8711 \end{pmatrix} \cdot \frac{\text{mH}}{\text{mi}}$$

$$Z' := R_{\text{perlength}} + j \cdot 2 \cdot \pi \cdot \text{freq} \cdot L_{\text{perlength}}$$

$$Z' = \begin{pmatrix} 0.373 + 1.459i & 0.095 + 0.683i & 0.095 + 0.599i \\ 0.095 + 0.683i & 0.373 + 1.459i & 0.095 + 0.683i \\ 0.095 + 0.599i & 0.095 + 0.683i & 0.373 + 1.459i \end{pmatrix} \cdot \frac{\text{ohm}}{\text{mi}}$$

$$\text{If length} = 40 \text{ miles:} \quad Z_{\text{line}} := Z' \cdot 40\text{mi}$$

$$Z_{\text{line}} = \begin{pmatrix} 14.932 + 58.374i & 3.812 + 27.33i & 3.812 + 23.965i \\ 3.812 + 27.33i & 14.932 + 58.374i & 3.812 + 27.33i \\ 3.812 + 23.965i & 3.812 + 27.33i & 14.932 + 58.374i \end{pmatrix} \Omega$$

$$a := 1 \cdot e^{j \cdot \frac{2 \cdot \pi}{3}} \quad A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix}$$

$$Z_{012} := A_{012}^{-1} \cdot Z_{\text{line}} \cdot A_{012}$$

$$Z_{012} = \begin{pmatrix} 22.5555 + 110.7903i & 0.9712 - 0.5607i & -0.9712 - 0.5607i \\ -0.9712 - 0.5607i & 11.12 + 32.1661i & -1.9424 + 1.1214i \\ 0.9712 - 0.5607i & 1.9424 + 1.1214i & 11.12 + 32.1661i \end{pmatrix} \Omega$$

By comparison:

$$D_m := (D_{ab} \cdot D_{bc} \cdot D_{ac})^{\frac{1}{3}}$$

$$Z_1 := \left( R_{ac} + j \cdot 2 \cdot \pi \cdot \text{freq} \cdot \frac{\mu_0}{2 \cdot \pi} \cdot \ln \left( \frac{D_m}{D_s} \right) \right) \cdot 40 \text{mi} \quad Z_1 = (11.12 + 32.1661i) \Omega$$

- **Transposition**

$$R_p := \begin{pmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix}$$

Example 1:

$$f_1 := 0.2 \quad f_2 := 0.3 \quad f_3 := 0.5$$

$$Z_{\text{net}} := f_1 \cdot Z_{\text{line}} + f_2 \cdot R_p^{-1} \cdot Z_{\text{line}} \cdot R_p + f_3 \cdot R_p \cdot Z_{\text{line}} \cdot R_p^{-1}$$

$$Z_{\text{net}} = \begin{pmatrix} 14.9318 + 58.3742i & 3.8118 + 25.6473i & 3.8118 + 26.6566i \\ 3.8118 + 25.6473i & 14.9318 + 58.3742i & 3.8118 + 26.3202i \\ 3.8118 + 26.6566i & 3.8118 + 26.3202i & 14.9318 + 58.3742i \end{pmatrix} \Omega$$

$$Z_{0121} := A_{012}^{-1} \cdot Z_{\text{net}} \cdot A_{012}$$

$$Z_{0121} = \begin{pmatrix} 22.5555 + 110.7903i & -0.2914 - 0.0561i & 0.2914 - 0.0561i \\ 0.2914 - 0.0561i & 11.12 + 32.1661i & 0.5827 + 0.1121i \\ -0.2914 - 0.0561i & -0.5827 + 0.1121i & 11.12 + 32.1661i \end{pmatrix} \Omega$$

Example 2

$$f_{16} := \frac{1}{3} \quad f_{26} := \frac{1}{3} \quad f_{36} := \frac{1}{3}$$

$$Z_{\text{net}6} := f_{16} \cdot Z_{\text{line}} + f_{26} \cdot R_p^{-1} \cdot Z_{\text{line}} \cdot R_p + f_{36} \cdot R_p \cdot Z_{\text{line}} \cdot R_p^{-1}$$

$$Z_{\text{net6}} = \begin{pmatrix} 14.9318 + 58.3742i & 3.8118 + 26.2081i & 3.8118 + 26.2081i \\ 3.8118 + 26.2081i & 14.9318 + 58.3742i & 3.8118 + 26.2081i \\ 3.8118 + 26.2081i & 3.8118 + 26.2081i & 14.9318 + 58.3742i \end{pmatrix} \Omega$$

$$Z_{0126} := A_{012}^{-1} \cdot Z_{\text{net6}} \cdot A_{012}$$

$$Z_{0126} = \begin{pmatrix} 22.555 + 110.79i & 0 & 0 \\ 0 & 11.12 + 32.166i & 0 \\ 0 & 0 & 11.12 + 32.166i \end{pmatrix} \Omega$$

**Double Circuit Line:**

Two parallel lines, 100 feet apart (center to center). Each has flat spacing

**A. Resistance Matrix**

AC Resistance from table:

$$R_{ac} := 0.278 \frac{\text{ohm}}{\text{mi}} \quad \text{at 25 C and} \quad \text{freq} := 60\text{Hz}$$

$$\text{CarsonsResistConst} := 9.869 \times 10^{-7} \frac{\text{ohm}}{\text{m} \cdot \text{Hz}}$$

$$R_d := \text{CarsonsResistConst} \cdot \text{freq} \quad R_d = 0.0953 \cdot \frac{\text{ohm}}{\text{mi}}$$

$$R_{self} := R_{ac} + R_d \quad R_{self} = 0.3733 \cdot \frac{\text{ohm}}{\text{mi}}$$

$$R' := \begin{pmatrix} R_{self} & R_d & R_d & R_d & R_d & R_d \\ R_d & R_{self} & R_d & R_d & R_d & R_d \\ R_d & R_d & R_{self} & R_d & R_d & R_d \\ R_d & R_d & R_d & R_{self} & R_d & R_d \\ R_d & R_d & R_d & R_d & R_{self} & R_d \\ R_d & R_d & R_d & R_d & R_d & R_{self} \end{pmatrix}$$

$$R' = \begin{pmatrix} 0.3733 & 0.0953 & 0.0953 & 0.0953 & 0.0953 & 0.0953 \\ 0.0953 & 0.3733 & 0.0953 & 0.0953 & 0.0953 & 0.0953 \\ 0.0953 & 0.0953 & 0.3733 & 0.0953 & 0.0953 & 0.0953 \\ 0.0953 & 0.0953 & 0.0953 & 0.3733 & 0.0953 & 0.0953 \\ 0.0953 & 0.0953 & 0.0953 & 0.0953 & 0.3733 & 0.0953 \\ 0.0953 & 0.0953 & 0.0953 & 0.0953 & 0.0953 & 0.3733 \end{pmatrix} \cdot \frac{\text{ohm}}{\text{mi}}$$

## B. Inductance Matrix

$$\mu_0 := 4 \cdot \pi \cdot 10^{-7} \frac{\text{H}}{\text{m}} \quad \rho := 100 \text{ohm} \cdot \text{m}$$

Calculate GMR from conductor diameter

$$\text{dia} := 0.528 \text{in} \quad \text{GMR} := e^{\frac{-1}{4}} \cdot \frac{\text{dia}}{2} \quad \text{GMR} = 0.01713 \cdot \text{ft}$$

Conductor GMR from table:

$$D_s := 0.01668 \text{ft}$$

$$D_e := 2160 \cdot \frac{\text{ft} \cdot \text{Hz}^{0.5}}{(\text{ohm} \cdot \text{m})^{0.5}}$$

$$D_e := D_e \cdot \sqrt{\frac{\rho}{\text{freq}}} \quad D_e = 2.7885 \times 10^3 \cdot \text{ft}$$

$Da1b1 := 10\text{ft}$      $Da1c1 := 20\text{ft}$      $Db1c1 := 10\text{ft}$      $Da1a2 := 100\text{ft}$      $Db1b2 := 100\text{ft}$      $Dc1c2 := 100\text{ft}$   
 $Da2b2 := 10\text{ft}$      $Da2c2 := 20\text{ft}$      $Db2c2 := 10\text{ft}$      $Da1b2 := 110\text{ft}$      $Da1c2 := 120\text{ft}$      $Db1a2 := 90\text{ft}$   
 $Db1c2 := 100\text{ft}$      $Dc1a2 := 80\text{ft}$      $Dc1b2 := 90\text{ft}$

$$L' := \frac{\mu_0}{2 \cdot \pi} \cdot \begin{pmatrix} \ln\left(\frac{De}{Ds}\right) & \ln\left(\frac{De}{Da1b1}\right) & \ln\left(\frac{De}{Da1c1}\right) & \ln\left(\frac{De}{Da1a2}\right) & \ln\left(\frac{De}{Da1b2}\right) & \ln\left(\frac{De}{Da1c2}\right) \\ \ln\left(\frac{De}{Da1b1}\right) & \ln\left(\frac{De}{Ds}\right) & \ln\left(\frac{De}{Db1c1}\right) & \ln\left(\frac{De}{Db1a2}\right) & \ln\left(\frac{De}{Db1b2}\right) & \ln\left(\frac{De}{Db1c2}\right) \\ \ln\left(\frac{De}{Da1c1}\right) & \ln\left(\frac{De}{Db1c1}\right) & \ln\left(\frac{De}{Ds}\right) & \ln\left(\frac{De}{Dc1a2}\right) & \ln\left(\frac{De}{Dc1b2}\right) & \ln\left(\frac{De}{Dc1c2}\right) \\ \ln\left(\frac{De}{Da1a2}\right) & \ln\left(\frac{De}{Db1a2}\right) & \ln\left(\frac{De}{Dc1a2}\right) & \ln\left(\frac{De}{Ds}\right) & \ln\left(\frac{De}{Da2b2}\right) & \ln\left(\frac{De}{Da2c2}\right) \\ \ln\left(\frac{De}{Da1b2}\right) & \ln\left(\frac{De}{Db1b2}\right) & \ln\left(\frac{De}{Dc1b2}\right) & \ln\left(\frac{De}{Da2b2}\right) & \ln\left(\frac{De}{Ds}\right) & \ln\left(\frac{De}{Db2c2}\right) \\ \ln\left(\frac{De}{Da1c2}\right) & \ln\left(\frac{De}{Db1c2}\right) & \ln\left(\frac{De}{Dc1c2}\right) & \ln\left(\frac{De}{Da2c2}\right) & \ln\left(\frac{De}{Db2c2}\right) & \ln\left(\frac{De}{Ds}\right) \end{pmatrix}$$

$$L' = \begin{pmatrix} 3.8711 & 1.8123 & 1.5892 & 1.0712 & 1.0405 & 1.0125 \\ 1.8123 & 3.8711 & 1.8123 & 1.1051 & 1.0712 & 1.0712 \\ 1.5892 & 1.8123 & 3.8711 & 1.143 & 1.1051 & 1.0712 \\ 1.0712 & 1.1051 & 1.143 & 3.8711 & 1.8123 & 1.5892 \\ 1.0405 & 1.0712 & 1.1051 & 1.8123 & 3.8711 & 1.8123 \\ 1.0125 & 1.0712 & 1.0712 & 1.5892 & 1.8123 & 3.8711 \end{pmatrix} \cdot \frac{\text{mH}}{\text{mi}}$$



$$Z' := R' + j \cdot 2 \cdot \pi \cdot \text{freq} \cdot L'$$

$$Z' = \begin{pmatrix} 0.373 + 1.459i & 0.095 + 0.683i & 0.095 + 0.599i & 0.095 + 0.404i & 0.095 + 0.392i & 0.095 + 0.382i \\ 0.095 + 0.683i & 0.373 + 1.459i & 0.095 + 0.683i & 0.095 + 0.417i & 0.095 + 0.404i & 0.095 + 0.404i \\ 0.095 + 0.599i & 0.095 + 0.683i & 0.373 + 1.459i & 0.095 + 0.431i & 0.095 + 0.417i & 0.095 + 0.404i \\ 0.095 + 0.404i & 0.095 + 0.417i & 0.095 + 0.431i & 0.373 + 1.459i & 0.095 + 0.683i & 0.095 + 0.599i \\ 0.095 + 0.392i & 0.095 + 0.404i & 0.095 + 0.417i & 0.095 + 0.683i & 0.373 + 1.459i & 0.095 + 0.683i \\ 0.095 + 0.382i & 0.095 + 0.404i & 0.095 + 0.404i & 0.095 + 0.599i & 0.095 + 0.683i & 0.373 + 1.459i \end{pmatrix} \cdot \frac{\text{ohm}}{\text{mi}}$$

If length = 40 miles:

$$Z_{\text{line}} := Z' \cdot 40 \text{mi}$$

$$Z_{\text{line}} = \begin{pmatrix} 14.932 + 58.374i & 3.812 + 27.33i & 3.812 + 23.965i & 3.812 + 16.154i & 3.812 + 15.691i & 3.812 + 15.269i \\ 3.812 + 27.33i & 14.932 + 58.374i & 3.812 + 27.33i & 3.812 + 16.665i & 3.812 + 16.154i & 3.812 + 16.154i \\ 3.812 + 23.965i & 3.812 + 27.33i & 14.932 + 58.374i & 3.812 + 17.237i & 3.812 + 16.665i & 3.812 + 16.154i \\ 3.812 + 16.154i & 3.812 + 16.665i & 3.812 + 17.237i & 14.932 + 58.374i & 3.812 + 27.33i & 3.812 + 23.965i \\ 3.812 + 15.691i & 3.812 + 16.154i & 3.812 + 16.665i & 3.812 + 27.33i & 14.932 + 58.374i & 3.812 + 27.33i \\ 3.812 + 15.269i & 3.812 + 16.154i & 3.812 + 16.154i & 3.812 + 23.965i & 3.812 + 27.33i & 14.932 + 58.374i \end{pmatrix} \Omega$$

$$a := 1 \cdot e^{j \cdot \frac{2 \cdot \pi}{3}}$$

$$A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix}$$

$$Z_a := \text{submatrix}(Z_{\text{line}}, 0, 2, 0, 2) \quad Z_b := \text{submatrix}(Z_{\text{line}}, 0, 2, 3, 5)$$

$$Z_c := \text{submatrix}(Z_{\text{line}}, 3, 5, 0, 2) \quad Z_d := \text{submatrix}(Z_{\text{line}}, 3, 5, 3, 5)$$

$$Z_{a012} := A_{012}^{-1} \cdot Z_a \cdot A_{012} \quad Z_{b012} := A_{012}^{-1} \cdot Z_b \cdot A_{012}$$

$$Z_{c012} := A_{012}^{-1} \cdot Z_c \cdot A_{012} \quad Z_{d012} := A_{012}^{-1} \cdot Z_d \cdot A_{012}$$

Build the matrix by stacking and augmenting submatrices

$$Z_{012\text{left}} := \text{stack}(Z_{a012}, Z_{c012})$$

$$Z_{012\text{right}} := \text{stack}(Z_{b012}, Z_{d012})$$

$$Z_{012} := \text{augment}(Z_{012\text{left}}, Z_{012\text{right}})$$

Note the off-diagonal subblocks and their coupling.

$$Z_{012} = \left( \begin{array}{cccccc} 22.555 + 110.79i & 0.971 - 0.561i & -0.971 - 0.561i & 11.435 + 48.713i & 0.27 + 0.671i & -0.27 + 0.671i \\ -0.971 - 0.561i & 11.12 + 32.166i & -1.942 + 1.121i & 0.313 - 0.8i & 0.139 - 0.126i & 0.043 + 0.129i \\ 0.971 - 0.561i & 1.942 + 1.121i & 11.12 + 32.166i & -0.313 - 0.8i & -0.043 + 0.129i & -0.139 - 0.126i \\ 11.435 + 48.713i & -0.313 - 0.8i & 0.313 - 0.8i & 22.555 + 110.79i & 0.971 - 0.561i & -0.971 - 0.561i \\ -0.27 + 0.671i & -0.139 - 0.126i & 0.043 + 0.129i & -0.971 - 0.561i & 11.12 + 32.166i & -1.942 + 1.121i \\ 0.27 + 0.671i & -0.043 + 0.129i & 0.139 - 0.126i & 0.971 - 0.561i & 1.942 + 1.121i & 11.12 + 32.166i \end{array} \right) \Omega$$

Now try transposing one or both of the lines

$$R_p := \begin{pmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix}$$

First, use the exact same scheme on both lines, so the  $Z_b$  and  $Z_c$  are kept simpler.

$$f_1 := \frac{1}{3} \quad f_2 := \frac{1}{3} \quad f_3 := \frac{1}{3}$$

$$Z_{anet} := f_1 \cdot Z_a + f_2 \cdot R_p^{-1} \cdot Z_a \cdot R_p + f_3 \cdot R_p \cdot Z_a \cdot R_p^{-1}$$

$$Z_{bnet} := f_1 \cdot Z_b + f_2 \cdot R_p^{-1} \cdot Z_b \cdot R_p + f_3 \cdot R_p \cdot Z_b \cdot R_p^{-1}$$

$$Z_{cnet} := f_1 \cdot Z_c + f_2 \cdot R_p^{-1} \cdot Z_c \cdot R_p + f_3 \cdot R_p \cdot Z_c \cdot R_p^{-1}$$

$$Z_{dnet} := f_1 \cdot Z_d + f_2 \cdot R_p^{-1} \cdot Z_d \cdot R_p + f_3 \cdot R_p \cdot Z_d \cdot R_p^{-1}$$

$$Z_{anet} = \begin{pmatrix} 14.932 + 58.374i & 3.812 + 26.208i & 3.812 + 26.208i \\ 3.812 + 26.208i & 14.932 + 58.374i & 3.812 + 26.208i \\ 3.812 + 26.208i & 3.812 + 26.208i & 14.932 + 58.374i \end{pmatrix} \Omega$$

$$Z_{bnet} = \begin{pmatrix} 3.812 + 16.154i & 3.812 + 16.36i & 3.812 + 16.199i \\ 3.812 + 16.199i & 3.812 + 16.154i & 3.812 + 16.36i \\ 3.812 + 16.36i & 3.812 + 16.199i & 3.812 + 16.154i \end{pmatrix} \Omega$$

$$Z_{cnet} = \begin{pmatrix} 3.812 + 16.154i & 3.812 + 16.199i & 3.812 + 16.36i \\ 3.812 + 16.36i & 3.812 + 16.154i & 3.812 + 16.199i \\ 3.812 + 16.199i & 3.812 + 16.36i & 3.812 + 16.154i \end{pmatrix} \Omega$$

$$Z_{dnet} = \begin{pmatrix} 14.932 + 58.374i & 3.812 + 26.208i & 3.812 + 26.208i \\ 3.812 + 26.208i & 14.932 + 58.374i & 3.812 + 26.208i \\ 3.812 + 26.208i & 3.812 + 26.208i & 14.932 + 58.374i \end{pmatrix} \Omega$$

$$Z_{a0121} := A_{012}^{-1} \cdot Z_{anet} \cdot A_{012}$$

$$Z_{b0121} := A_{012}^{-1} \cdot Z_{bnet} \cdot A_{012}$$

$$Z_{c0121} := A_{012}^{-1} \cdot Z_{cnet} \cdot A_{012}$$

$$Z_{d0121} := A_{012}^{-1} \cdot Z_{dnet} \cdot A_{012}$$

Build the matrix by stacking and augmenting submatrices

$$Z_{012left1} := \text{stack}(Z_{a0121}, Z_{c0121})$$

$$Z_{012right1} := \text{stack}(Z_{b0121}, Z_{d0121})$$

$$Z_{0121} := \text{augment}(Z_{012left1}, Z_{012right1})$$

$$Z_{0121} = \begin{pmatrix} 22.555 + 110.79i & 0 & 0 & 11.435 + 48.713i & 0 & 0 \\ 0 & 11.12 + 32.166i & 0 & 0 & 0.139 - 0.126i & 0 \\ 0 & 0 & 11.12 + 32.166i & 0 & 0 & -0.139 - 0.126i \\ 11.435 + 48.713i & 0 & 0 & 22.555 + 110.79i & 0 & 0 \\ 0 & -0.139 - 0.126i & 0 & 0 & 11.12 + 32.166i & 0 \\ 0 & 0 & 0.139 - 0.126i & 0 & 0 & 11.12 + 32.166i \end{pmatrix} \Omega$$

- Notice what this has done to the cross-coupling terms. The positive and negative sequence coupling between the two lines is very small relative to the zero sequence cross-coupling.