

Unbalanced Fault Analysis Examples

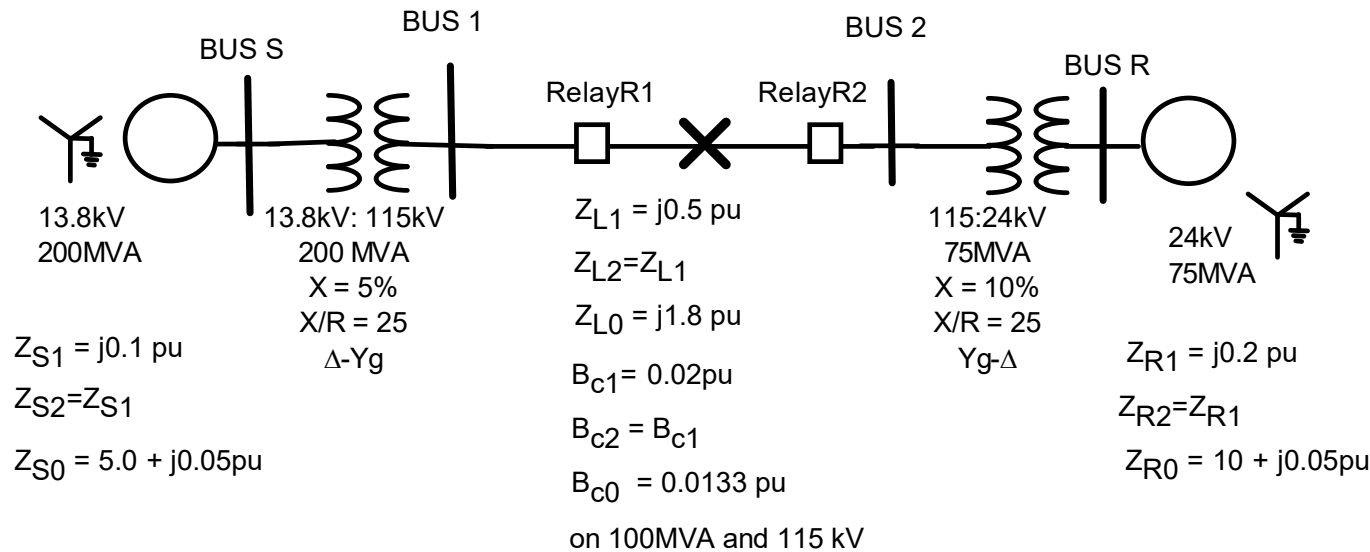
Define units: MVA := 1000kW MVAR := MVA
 MW := MVA pu := 1

$$a := 1 \cdot e^{j \cdot 120 \text{deg}}$$

$$A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix}$$

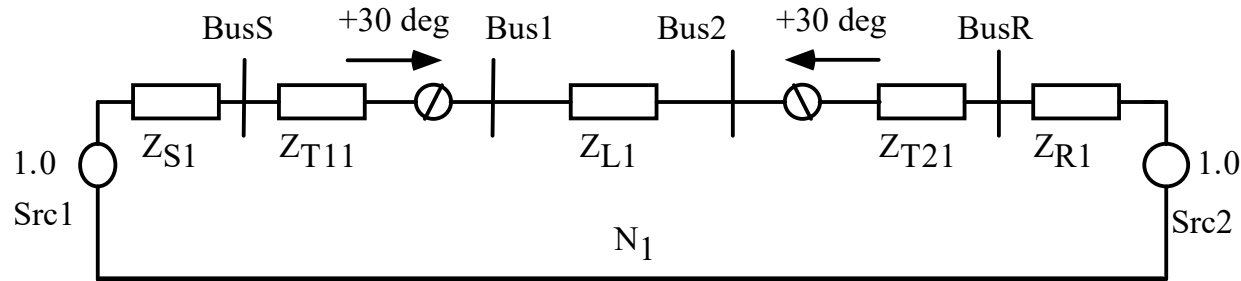
$$\angle(\text{mag}, \text{ang}) := \text{mag} \cdot \cos(\text{ang} \cdot \text{deg}) + j \cdot \text{mag} \cdot \sin(\text{ang} \cdot \text{deg})$$

System Description:



Per Unit Change of Base Calculations (hidden, to view double click on the arrow)





- Positive sequence Ybus

$$Y_1(M) := \begin{bmatrix} \frac{1}{jX_{G11}} + \frac{1}{Z_{T11}} & \frac{-1 \cdot e^{-j \cdot 30 \text{deg}}}{Z_{T11}} & 0 & 0 & 0 \\ \frac{-1 \cdot e^{j \cdot 30 \text{deg}}}{Z_{T11}} & \frac{1}{Z_{T11}} + \frac{1}{M \cdot Z_{L11}} & 0 & 0 & \frac{-1}{M \cdot Z_{L11}} \\ 0 & 0 & \frac{1}{Z_{T21}} + \frac{1}{(1-M) \cdot Z_{L11}} & \frac{-1 \cdot e^{j \cdot 30 \text{deg}}}{Z_{T21}} & \frac{-1}{(1-M) \cdot Z_{L11}} \\ 0 & 0 & \frac{-1 \cdot e^{-j \cdot 30 \text{deg}}}{Z_{T21}} & \frac{1}{Z_{T21}} + \frac{1}{jX_{G21}} & 0 \\ 0 & \frac{-1}{M \cdot Z_{L11}} & \frac{-1}{(1-M) \cdot Z_{L11}} & 0 & \frac{1}{M \cdot Z_{L11}} + \frac{1}{(1-M) \cdot Z_{L11}} \end{bmatrix}$$

$$Z_1(M) := Y_1(M)^{-1}$$

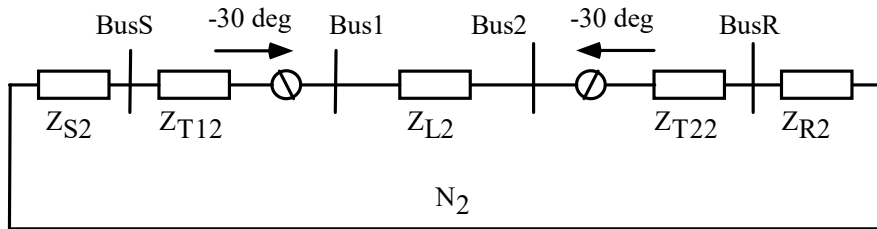
$$V_S := 1.0 \text{pu}$$

$$V_R := 1.0 \text{pu}$$

$$V_f := 1.0 \text{pu}$$

Negative Sequence Ybus

- All of the impedance values are the same in this case.
- Only change is in the Δ -Y phase shifts.
- Equivalent circuit looks the same, but no sources.

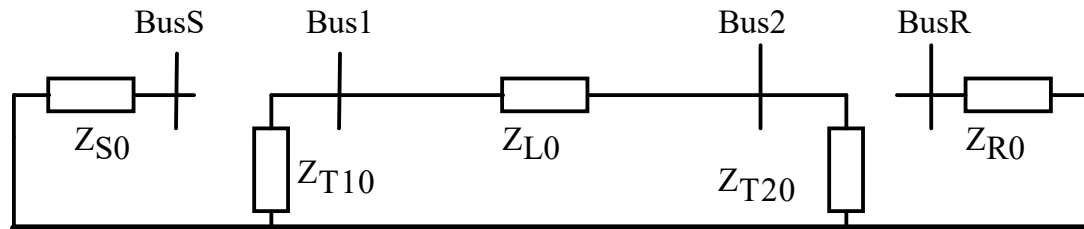


$$Y_2(M) := \begin{bmatrix} \frac{1}{jX_{G12}} + \frac{1}{Z_{T12}} & \frac{-1 \cdot e^{j \cdot 30 \text{deg}}}{Z_{T12}} & 0 & 0 & 0 \\ \frac{-1 \cdot e^{-j \cdot 30 \text{deg}}}{Z_{T12}} & \frac{1}{Z_{T12}} + \frac{1}{M \cdot Z_{L12}} & 0 & 0 & \frac{-1}{M \cdot Z_{L12}} \\ 0 & 0 & \frac{1}{Z_{T22}} + \frac{1}{(1-M) \cdot Z_{L12}} & \frac{-1 \cdot e^{-j \cdot 30 \text{deg}}}{Z_{T22}} & \frac{-1}{(1-M) \cdot Z_{L12}} \\ 0 & 0 & \frac{-1 \cdot e^{j \cdot 30 \text{deg}}}{Z_{T22}} & \frac{1}{Z_{T22}} + \frac{1}{jX_{G22}} & 0 \\ 0 & \frac{-1}{M \cdot Z_{L12}} & \frac{-1}{(1-M) \cdot Z_{L12}} & 0 & \frac{1}{M \cdot Z_{L12}} + \frac{1}{(1-M) \cdot Z_{L12}} \end{bmatrix}$$

$$Z_2(M) := Y_2(M)^{-1}$$

Zero Sequence Ybus

- Impedance values differ
- Model the transformer zero sequence connections
- Different looking equivalent circuit.



$$Y_0(M) := \begin{bmatrix} \frac{1}{Z_{G10}} & 0 & 0 & 0 & 0 \\ 0 & \frac{1}{Z_{T10}} + \frac{1}{M \cdot Z_{L10}} & 0 & 0 & \frac{-1}{M \cdot Z_{L10}} \\ 0 & 0 & \frac{1}{Z_{T20}} + \frac{1}{(1-M) \cdot Z_{L10}} & 0 & \frac{-1}{(1-M) \cdot Z_{L10}} \\ 0 & 0 & 0 & \frac{1}{Z_{G20}} & 0 \\ 0 & \frac{-1}{M \cdot Z_{L10}} & \frac{-1}{(1-M) \cdot Z_{L10}} & 0 & \frac{1}{M \cdot Z_{L10}} + \frac{1}{(1-M) \cdot Z_{L10}} \end{bmatrix}$$

$$Z_0(M) := Y_0(M)^{-1}$$

SLG Fault:

$$I_{0_SLG}(M, R_f) := \frac{V_f}{Z_1(M)_{4,4} + Z_2(M)_{4,4} + Z_0(M)_{4,4} + 3 \cdot R_f}$$

$$|I_{0_SLG}(0.5, 0)| = 1.0853$$

$$\arg(I_{0_SLG}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{1_SLG}(M, R_f) := I_{0_SLG}(M, R_f)$$

$$I_{2_SLG}(M, R_f) := I_{0_SLG}(M, R_f)$$

$$I_{ABC_SLG}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_SLG}(M, R_f) \\ I_{1_SLG}(M, R_f) \\ I_{2_SLG}(M, R_f) \end{pmatrix} \quad \overrightarrow{|I_{ABC_SLG}(0.5, 0)|} = \begin{pmatrix} 3.2558 \\ 0 \\ 0 \end{pmatrix} \cdot \text{pu} \quad \overrightarrow{\arg(I_{ABC_SLG}(0.5, 0))} = \begin{pmatrix} -90 \\ 18.4349 \\ 18.4349 \end{pmatrix} \cdot \text{deg}$$

- Angles meaningless when magnitude is 0

- Now find voltages in each sequence component)

$$\Delta V_{1_SLG}(M, R_f) := Z_1(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{1_SLG}(M, R_f) \end{pmatrix} \quad \overrightarrow{|\Delta V_{1_SLG}(0.5, 0)|} = \begin{pmatrix} 0.0362 \\ 0.0543 \\ 0.1447 \\ 0.0965 \\ 0.2351 \end{pmatrix} \quad \overrightarrow{\arg(\Delta V_{1_SLG}(0.5, 0))} = \begin{pmatrix} 150 \\ 180 \\ -180 \\ 150 \\ 180 \end{pmatrix} \cdot \text{deg}$$

- Now when we find V1 we need to *include the transformer phase shift* in the prefault voltages

$$V1_{\text{SLG}}(M, R_f) := \begin{pmatrix} 1.0e^{-j \cdot 30\text{deg}} \\ 1.0 \\ 1.0 \\ 1.0 \cdot e^{-j \cdot 30\text{deg}} \\ 1.0 \end{pmatrix} + \Delta V1_{\text{SLG}}(M, R_f) \quad \xrightarrow{|\overline{V1_{\text{SLG}}(0.5, 0)}|} \begin{pmatrix} 0.9638 \\ 0.9457 \\ 0.8553 \\ 0.9035 \\ 0.7649 \end{pmatrix} \quad \xrightarrow{\arg(\overline{V1_{\text{SLG}}(0.5, 0)})} \begin{pmatrix} -30 \\ 0 \\ 0 \\ -30 \\ 0 \end{pmatrix} \cdot \text{deg}$$

$$\Delta V2_{\text{SLG}}(M, R_f) := Z_2(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I2_{\text{SLG}}(M, R_f) \end{pmatrix} \quad \xrightarrow{|\overline{\Delta V2_{\text{SLG}}(0.5, 0)}|} \begin{pmatrix} 0.0362 \\ 0.0543 \\ 0.1447 \\ 0.0965 \\ 0.2351 \end{pmatrix} \quad \xrightarrow{\arg(\overline{\Delta V2_{\text{SLG}}(0.5, 0)})} \begin{pmatrix} -150 \\ -180 \\ -180 \\ -150 \\ -180 \end{pmatrix} \cdot \text{deg}$$

Note the -30 degree shift...

$$V2_{\text{SLG}}(M, R_f) := \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} + \Delta V2_{\text{SLG}}(M, R_f) \quad \bullet \text{ No prefault voltage, so enter 0.}$$

$$\Delta V_{0\text{SLG}}(M, R_f) := Z_0(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ -I_{0\text{SLG}}(M, R_f) \end{pmatrix} \quad \Delta V_{0\text{SLG}}(0.5, 0) = \begin{pmatrix} 0 \\ -0.0143 \\ -0.0683 \\ 0 \\ -0.5297 \end{pmatrix} \quad V_{0\text{SLG}}(M, R_f) := \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} + \Delta V_{0\text{SLG}}(M, R_f)$$

Again, no pre-fault voltage

- ABC Voltages at Bus 1

$$V_{\text{ABC}1.\text{SLG}}(M, R_f) := A_{012} \cdot \begin{pmatrix} V_{0\text{SLG}}(M, R_f)_1 \\ V_{1\text{SLG}}(M, R_f)_1 \\ V_{2\text{SLG}}(M, R_f)_1 \end{pmatrix} \xrightarrow{|\text{V}_{\text{ABC}1.\text{SLG}}(0.5, 0)|} = \begin{pmatrix} 0.8772 \\ 0.9806 \\ 0.9806 \end{pmatrix} \cdot \text{pu} \quad \arg(V_{\text{ABC}1.\text{SLG}}(0.5, 0)) = \begin{pmatrix} 0 \\ -117.9783 \\ 117.9783 \end{pmatrix} \cdot \text{deg}$$

- ABC Voltages at Bus S

$$V_{\text{ABC}S.\text{SLG}}(M, R_f) := A_{012} \cdot \begin{pmatrix} V_{0\text{SLG}}(M, R_f)_0 \\ V_{1\text{SLG}}(M, R_f)_0 \\ V_{2\text{SLG}}(M, R_f)_0 \end{pmatrix} \xrightarrow{|\text{V}_{\text{ABC}S.\text{SLG}}(0.5, 0)|} = \begin{pmatrix} 0.9463 \\ 0.9463 \\ 1 \end{pmatrix} \cdot \text{pu} \quad \arg(V_{\text{ABC}S.\text{SLG}}(0.5, 0)) = \begin{pmatrix} -31.8973 \\ -148.1027 \\ 90 \end{pmatrix} \cdot \text{deg}$$

- Branch currents

- Relay 1 currents

$$I_{1_B1.SLG}(M, R_f) := \frac{V_{1SLG}(M, R_f)_1 - V_{1SLG}(M, R_f)_4}{M \cdot Z_{L11}} \quad |I_{1_B1.SLG}(0.5, 0)| = 0.7235 \quad \arg(I_{1_B1.SLG}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{2_B1.SLG}(M, R_f) := \frac{V_{2SLG}(M, R_f)_1 - V_{2SLG}(M, R_f)_4}{M \cdot Z_{L12}} \quad |I_{2_B1.SLG}(0.5, 0)| = 0.7235 \quad \arg(I_{2_B1.SLG}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{0_B1.SLG}(M, R_f) := \frac{V_{0SLG}(M, R_f)_1 - V_{0SLG}(M, R_f)_4}{M \cdot Z_{L10}} \quad |I_{0_B1.SLG}(0.5, 0)| = 0.5727 \quad \arg(I_{0_B1.SLG}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{ABC_B1.SLG}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_B1.SLG}(M, R_f) \\ I_{1_B1.SLG}(M, R_f) \\ I_{2_B1.SLG}(M, R_f) \end{pmatrix} \xrightarrow{|I_{ABC_B1.SLG}(0.5, 0)|} \begin{pmatrix} 2.0197 \\ 0.1509 \\ 0.1509 \end{pmatrix} \cdot \text{pu} \quad \arg(I_{ABC_B1.SLG}(0.5, 0)) = \begin{pmatrix} -90 \\ 90 \\ 90 \end{pmatrix} \cdot \text{deg}$$

- LVside of transformer (Bus S)

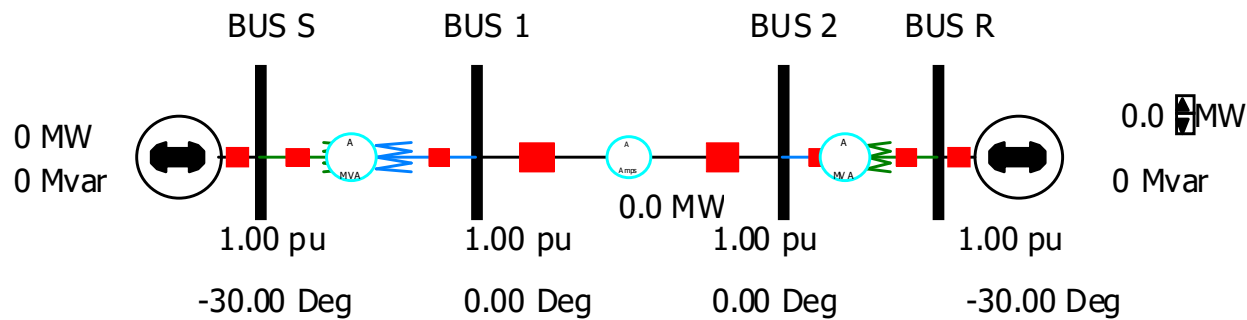
$$I_{1_BS.SLG}(M, R_f) := \frac{V_S \cdot e^{-j \cdot 30 \text{deg}} - V_{1SLG}(M, R_f)_0}{jX_{G11}} \quad |I_{1_BS.SLG}(0.5, 0)| = 0.7235 \cdot \text{pu} \quad \arg(I_{1_BS.SLG}(0.5, 0)) = -120 \cdot \text{deg}$$

$$I_{2_BS.SLG}(M, R_f) := \frac{0 - V_{2SLG}(M, R_f)_0}{jX_{G12}} \quad |I_{2_BS.SLG}(0.5, 0)| = 0.7235 \cdot \text{pu} \quad \arg(I_{2_BS.SLG}(0.5, 0)) = -60 \cdot \text{deg}$$

$$I_{0_BS.SLG} := 0$$

$$I_{ABC_BS.SLG}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_BS.SLG} \\ I_{1_BS.SLG}(M, R_f) \\ I_{2_BS.SLG}(M, R_f) \end{pmatrix} \xrightarrow{|I_{ABC_BS.SLG}(0.5, 0)|} = \begin{pmatrix} 1.2532 \\ 1.2532 \\ 0 \end{pmatrix} \cdot \text{pu} \quad \arg(I_{ABC_BS.SLG}(0.5, 0)) = \begin{pmatrix} -90 \\ 90 \\ 38.6598 \end{pmatrix} \cdot \text{deg}$$

• **Circuit implementation in Powerworld**



• **Powerworld Results**

$$I_{AFSLG} := 3.256 \angle (-90\text{deg})$$

| Fault Data - Buses | | | | | | |
|--------------------|--------------|-------------|--------------|-------------|--------------|-------------|
| Name | Phase Volt A | Phase Ang A | Phase Volt B | Phase Ang B | Phase Volt C | Phase Ang C |
| BUS S | 0.94625 | -31.9 | 0.94625 | -148.1 | 1 | 90 |
| BUS 1 | 0.87716 | 0 | 0.98064 | -117.98 | 0.98064 | 117.98 |
| BUS 2 | 0.64224 | 0 | 0.96409 | -116.07 | 0.96409 | 116.07 |
| BUS R | 0.85937 | -35.58 | 0.85937 | -144.42 | 1 | 90 |
| FaultPt | 0 | 0 | 1.1753 | -132.54 | 1.1753 | 132.54 |

| Fault Data - Lines | | | | | | | |
|--------------------|---------|------------------|------------------|------------------|------------------|------------------|------------------|
| From Name | To Name | Phase Cur A From | Phase Ang A From | Phase Cur B From | Phase Ang B From | Phase Cur C From | Phase Ang C From |
| BUS S | BUS 1 | 1.25318 | -90 | 1.25318 | 90 | 0 | 0 |
| BUS 1 | BUS 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| BUS 1 | FaultPt | 2.0197 | -90 | 0.15086 | 90 | 0.15086 | 90 |
| BUS R | BUS 2 | 0.62659 | -90 | 0.62659 | 90 | 0 | 0 |
| FaultPt | BUS 2 | 1.23615 | 90 | 0.15086 | 90 | 0.15086 | 90 |

Good match with calculations above.

LL Fault:

$$I_{1_LL}(M, R_f) := \frac{V_f}{Z_1(M)_{4,4} + Z_2(M)_{4,4} + R_f}$$

$$|I_{1_LL}(0.5, 0)| = 2.3077$$

$$\arg(I_{1_LL}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{2_LL}(M, R_f) := -I_{1_LL}(M, R_f)$$

$$I_{0_LL} := 10^{-15} \quad \text{Approximately zero, works better with MathCAD.}$$

$$I_{ABC_LL}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_LL} \\ I_{1_LL}(M, R_f) \\ I_{2_LL}(M, R_f) \end{pmatrix} \quad \overrightarrow{|I_{ABC_LL}(0.5, 0)|} = \begin{pmatrix} 0 \\ 3.997 \\ 3.997 \end{pmatrix} \cdot \text{pu} \quad \overrightarrow{\arg(I_{ABC_LL}(0.5, 0))} = \begin{pmatrix} 0 \\ 180 \\ 0 \end{pmatrix} \cdot \text{deg}$$

Note: $\frac{I_{ABC_LL}(0.5,0)_1}{I_{1_LL}(0.5,0)} = -1.7321i$

- Now find voltages in each sequence component)

$$\Delta V_{1LL}(M, R_f) := Z_1(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{1_LL}(M, R_f) \end{pmatrix} \xrightarrow{|\Delta V_{1LL}(0.5,0)|} \begin{pmatrix} 0.0769 \\ 0.1154 \\ 0.3077 \\ 0.2051 \\ 0.5 \end{pmatrix} \xrightarrow{\arg(\Delta V_{1LL}(0.5,0))} \begin{pmatrix} 150 \\ 180 \\ -180 \\ 150 \\ 180 \end{pmatrix} \cdot \text{deg}$$

- Again, when we find V1 we need to *include the transformer phase shift* in the prefault voltages

$$V_{1LL}(M, R_f) := \begin{pmatrix} 1.0e^{-j \cdot 30\text{deg}} \\ 1.0 \\ 1.0 \\ 1.0 \cdot e^{-j \cdot 30\text{deg}} \\ 1.0 \end{pmatrix} + \Delta V_{1LL}(M, R_f) \xrightarrow{|V_{1LL}(0.5,0)|} \begin{pmatrix} 0.9231 \\ 0.8846 \\ 0.6923 \\ 0.7949 \\ 0.5 \end{pmatrix} \xrightarrow{\arg(V_{1LL}(0.5,0))} \begin{pmatrix} -30 \\ 0 \\ 0 \\ -30 \\ 0 \end{pmatrix} \cdot \text{deg}$$

$$\Delta V_{2LL}(M, R_f) := Z_2(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{2_LL}(M, R_f) \end{pmatrix} \xrightarrow{|\Delta V_{2LL}(0.5, 0)|} \begin{pmatrix} 0.0769 \\ 0.1154 \\ 0.3077 \\ 0.2051 \\ 0.5 \end{pmatrix} \xrightarrow{\arg(\Delta V_{2LL}(0.5, 0))} \begin{pmatrix} 30 \\ 0 \\ 0 \\ 30 \\ 0 \end{pmatrix} \cdot \text{deg}$$

Note the -30 degree shift...

$$V_{2LL}(M, R_f) := \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} + \Delta V_{2LL}(M, R_f)$$

$$\Delta V_{0LL}(M, R_f) := Z_0(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{0_LL} \end{pmatrix} \quad \Delta V_{0LL}(0.5, 0) = \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \quad V_{0LL}(M, R_f) := \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} + \Delta V_{0LL}(M, R_f)$$

- ABC Voltages at Bus 1

$$V_{\text{ABC}B1.LL}(M, R_f) := A_{012} \cdot \begin{pmatrix} V_{0LL}(M, R_f)_1 \\ V_{1LL}(M, R_f)_1 \\ V_{2LL}(M, R_f)_1 \end{pmatrix} \xrightarrow{|V_{\text{ABC}B1.LL}(0.5, 0)|} = \begin{pmatrix} 1 \\ 0.8329 \\ 0.8329 \end{pmatrix} \cdot \text{pu} \quad \arg(V_{\text{ABC}B1.LL}(0.5, 0)) = \begin{pmatrix} 0 \\ -126.8903 \\ 126.8903 \end{pmatrix} \cdot \text{deg}$$

- ABC Voltages at Bus S

$$V_{\text{ABC}BS.LL}(M, R_f) := A_{012} \cdot \begin{pmatrix} V_{0LL}(M, R_f)_0 \\ V_{1LL}(M, R_f)_0 \\ V_{2LL}(M, R_f)_0 \end{pmatrix} \xrightarrow{|V_{\text{ABC}BS.LL}(0.5, 0)|} = \begin{pmatrix} 0.9638 \\ 0.9638 \\ 0.8462 \end{pmatrix} \cdot \text{pu} \quad \arg(V_{\text{ABC}BS.LL}(0.5, 0)) = \begin{pmatrix} -26.0368 \\ -153.9632 \\ 90 \end{pmatrix} \cdot \text{deg}$$

- Branch currents
- Relay 1 currents

$$I_{1_B1.LL}(M, R_f) := \frac{V_{1LL}(M, R_f)_1 - V_{1LL}(M, R_f)_4}{M \cdot Z_{L11}} \quad |I_{1_B1.LL}(0.5, 0)| = 1.5385 \quad \arg(I_{1_B1.LL}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{2_B1.LL}(M, R_f) := \frac{V_{2LL}(M, R_f)_1 - V_{2LL}(M, R_f)_4}{M \cdot Z_{L12}} \quad |I_{2_B1.LL}(0.5, 0)| = 1.5385 \quad \arg(I_{2_B1.LL}(0.5, 0)) = 90 \cdot \text{deg}$$

$$I_{0_B1.LL}(M, R_f) := \frac{V_{0LL}(M, R_f)_1 - V_{0LL}(M, R_f)_4}{M \cdot Z_{L10}}$$

$$|I_{0_B1.LL}(0.5, 0)| = 0$$

$$\arg(I_{0_B1.LL}(0.5, 0)) = 0 \cdot \text{deg}$$

$$I_{ABC_B1.LL}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_B1.LL}(M, R_f) \\ I_{1_B1.LL}(M, R_f) \\ I_{2_B1.LL}(M, R_f) \end{pmatrix}$$

$$\overrightarrow{|I_{ABC_B1.LL}(0.5, 0)|} = \begin{pmatrix} 0 \\ 2.6647 \\ 2.6647 \end{pmatrix} \cdot \text{pu}$$

$$\arg(I_{ABC_B1.LL}(0.5, 0)) = \begin{pmatrix} 21.2839 \\ 180 \\ 0 \end{pmatrix} \cdot \text{deg}$$

- LVside of transformer (Bus S)

$$I_{1_BS.LL}(M, R_f) := \frac{V_S \cdot e^{-j \cdot 30 \text{deg}} - V_{1LL}(M, R_f)_0}{jX_{G11}}$$

$$|I_{1_BS.LL}(0.5, 0)| = 1.5385 \cdot \text{pu}$$

$$\arg(I_{1_BS.LL}(0.5, 0)) = -120 \cdot \text{deg}$$

$$I_{2_BS.LL}(M, R_f) := \frac{0 - V_{2LL}(M, R_f)_0}{jX_{G12}}$$

$$|I_{2_BS.LL}(0.5, 0)| = 1.5385 \cdot \text{pu}$$

$$\arg(I_{2_BS.LL}(0.5, 0)) = 120 \cdot \text{deg}$$

$$I_{0_BS.LL} := 0$$

$$I_{ABC_BS.LL}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_BS.LL} \\ I_{1_BS.LL}(M, R_f) \\ I_{2_BS.LL}(M, R_f) \end{pmatrix}$$

$$\overrightarrow{|I_{ABC_BS.LL}(0.5, 0)|} = \begin{pmatrix} 1.5385 \\ 1.5385 \\ 3.0769 \end{pmatrix} \cdot \text{pu}$$

$$\arg(I_{ABC_BS.LL}(0.5, 0)) = \begin{pmatrix} 180 \\ 180 \\ 0 \end{pmatrix} \cdot \text{deg}$$

• **Powerworld Results**

$I_{BFL} := 3.997 \angle (180\text{deg})$

| Fault Data - Buses | | | | | | |
|--------------------|--------------|-------------|--------------|-------------|--------------|-------------|
| Name | Phase Volt A | Phase Ang A | Phase Volt B | Phase Ang B | Phase Volt C | Phase Ang C |
| BUS S | 0.96384 | -26.04 | 0.96384 | -153.96 | 0.84615 | 90 |
| BUS 1 | 1 | 0 | 0.83294 | -126.89 | 0.83294 | 126.89 |
| BUS 2 | 1 | 0 | 0.60079 | -146.33 | 0.60079 | 146.33 |
| BUS R | 0.91485 | -18.8 | 0.91485 | -161.2 | 0.58974 | 90 |
| FaultPt | 1 | 0 | 0.5 | 180 | 0.5 | -180 |

| Fault Data - Lines | | | | | | | |
|--------------------|---------|------------------|------------------|------------------|------------------|------------------|------------------|
| From Name | To Name | Phase Cur A From | Phase Ang A From | Phase Cur B From | Phase Ang B From | Phase Cur C From | Phase Ang C From |
| BUS S | BUS 1 | 1.53846 | -180 | 1.53846 | -180 | 3.07692 | 0 |
| BUS 1 | BUS 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| BUS 1 | FaultPt | 0 | 0 | 2.66469 | -180 | 2.66469 | 0 |
| BUS R | BUS 2 | 0.76923 | -180 | 0.76923 | -180 | 1.53846 | 0 |
| FaultPt | BUS 2 | 0 | 0 | 1.33235 | 0 | 1.33235 | -180 |

DLG Fault:

$$I_{1_DLG}(M, R_f) := \frac{V_f}{(Z_1(M)_{4,4}) + \left[\frac{1}{Z_2(M)_{4,4}} + \frac{1}{(Z_0(M)_{4,4} + 3 \cdot R_f)} \right]^{-1}}$$

$$|I_{1_DLG}(0.5, 0)| = 2.7269 \quad \arg(I_{1_DLG}(0.5, 0)) = -90 \cdot \text{deg}$$

Current dividers for I_0 and I_2

$$I_{0_DLG}(M, R_f) := -I_{1_DLG}(M, R_f) \cdot \left[\frac{Z_2(M)_{4,4}}{Z_2(M)_{4,4} + (Z_0(M)_{4,4} + 3 \cdot R_f)} \right]$$

$$I_{2_DLG}(M, R_f) := -I_{1_DLG}(M, R_f) \cdot \left[\frac{Z_0(M)_{4,4} + 3 \cdot R_f}{Z_2(M)_{4,4} + (Z_0(M)_{4,4} + 3 \cdot R_f)} \right]$$

$$I_{ABC_DLG}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_DLG}(M, R_f) \\ I_{1_DLG}(M, R_f) \\ I_{2_DLG}(M, R_f) \end{pmatrix} \quad \xrightarrow{|I_{ABC_DLG}(0.5, 0)|} = \begin{pmatrix} 0 \\ 4.1902 \\ 4.1902 \end{pmatrix} \cdot \text{pu} \quad \xrightarrow{\arg(I_{ABC_DLG}(0.5, 0))} = \begin{pmatrix} -90 \\ 162.5359 \\ 17.4641 \end{pmatrix} \cdot \text{deg}$$

- Angles meaningless when magnitude is 0

- Now find voltages in each sequence component)

$$\Delta V_{1\text{DLG}}(M, R_f) := Z_1(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{1\text{DLG}}(M, R_f) \end{pmatrix} \xrightarrow{|\Delta V_{1\text{DLG}}(0.5, 0)|} \begin{pmatrix} 0.0909 \\ 0.1363 \\ 0.3636 \\ 0.2424 \\ 0.5908 \end{pmatrix} \xrightarrow{\arg(\Delta V_{1\text{DLG}}(0.5, 0))} \begin{pmatrix} 150 \\ 180 \\ -180 \\ 150 \\ 180 \end{pmatrix} \cdot \text{deg}$$

- Now when we find V1 we need to *include the transformer phase shift* in the prefault voltages

$$V_{1\text{DLG}}(M, R_f) := \begin{pmatrix} 1.0e^{-j \cdot 30\text{deg}} \\ 1.0 \\ 1.0 \\ 1.0 \cdot e^{-j \cdot 30\text{deg}} \\ 1.0 \end{pmatrix} + \Delta V_{1\text{DLG}}(M, R_f) \xrightarrow{|V_{1\text{DLG}}(0.5, 0)|} \begin{pmatrix} 0.9091 \\ 0.8637 \\ 0.6364 \\ 0.7576 \\ 0.4092 \end{pmatrix} \xrightarrow{\arg(V_{1\text{DLG}}(0.5, 0))} \begin{pmatrix} -30 \\ 0 \\ 0 \\ -30 \\ 0 \end{pmatrix} \cdot \text{deg}$$

$$\Delta V_{2_DLG}(M, R_f) := Z_2(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{2_DLG}(M, R_f) \end{pmatrix} \xrightarrow{|\Delta V_{2_DLG}(0.5, 0)|} \begin{pmatrix} 0.063 \\ 0.0944 \\ 0.2518 \\ 0.1679 \\ 0.4092 \end{pmatrix} \xrightarrow{\arg(\Delta V_{2_DLG}(0.5, 0))} \begin{pmatrix} 30 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} \cdot \text{deg}$$

$$V_{2_DLG}(M, R_f) := \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} + \Delta V_{2_DLG}(M, R_f) \quad \bullet \quad \text{No prefault voltage, so enter 0.}$$

$$\Delta V_{0_DLG}(M, R_f) := Z_0(M) \cdot \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ -I_{0_DLG}(M, R_f) \end{pmatrix} \quad \Delta V_{0_DLG}(0.5, 0) = \begin{pmatrix} 0 \\ 0.0111 \\ 0.0528 \\ 0 \\ 0.4092 \end{pmatrix} \quad V_{0_DLG}(M, R_f) := \begin{pmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{pmatrix} + \Delta V_{0_DLG}(M, R_f)$$

Again, no prefault voltage

- ABC Voltages at Bus 1

$$V_{\text{ABCBS.DLG}}(M, R_f) := A_{012} \cdot \begin{pmatrix} V_{0\text{DLG}}(M, R_f)_1 \\ V_{1\text{DLG}}(M, R_f)_1 \\ V_{2\text{DLG}}(M, R_f)_1 \end{pmatrix} \xrightarrow{|\text{V}_{\text{ABCBS.DLG}}(0.5, 0)|} = \begin{pmatrix} 0.9691 \\ 0.8141 \\ 0.8141 \end{pmatrix} \cdot \text{pu} \quad \arg(\text{V}_{\text{ABCBS.DLG}}(0.5, 0)) = \begin{pmatrix} 0 \\ -125.0878 \\ 125.0878 \end{pmatrix} \cdot \text{deg}$$

- ABC Voltages at Bus S

$$V_{\text{ABCBS.DLG}}(M, R_f) := A_{012} \cdot \begin{pmatrix} V_{0\text{DLG}}(M, R_f)_0 \\ V_{1\text{DLG}}(M, R_f)_0 \\ V_{2\text{DLG}}(M, R_f)_0 \end{pmatrix} \xrightarrow{|\text{V}_{\text{ABCBS.DLG}}(0.5, 0)|} = \begin{pmatrix} 0.9422 \\ 0.9422 \\ 0.8462 \end{pmatrix} \cdot \text{pu} \quad \arg(\text{V}_{\text{ABCBS.DLG}}(0.5, 0)) = \begin{pmatrix} -26.6828 \\ -153.3172 \\ 90 \end{pmatrix} \cdot \text{deg}$$

- Branch currents

- Relay 1 currents

$$I_{1_B1.DLG}(M, R_f) := \frac{V_{1\text{DLG}}(M, R_f)_1 - V_{1\text{DLG}}(M, R_f)_4}{M \cdot Z_{L11}} \quad |I_{1_B1.DLG}(0.5, 0)| = 1.8179 \quad \arg(I_{1_B1.DLG}(0.5, 0)) = -90 \cdot \text{deg}$$

$$I_{2_B1.DLG}(M, R_f) := \frac{V_{2\text{DLG}}(M, R_f)_1 - V_{2\text{DLG}}(M, R_f)_4}{M \cdot Z_{L12}} \quad |I_{2_B1.DLG}(0.5, 0)| = 1.259 \quad \arg(I_{2_B1.DLG}(0.5, 0)) = 90 \cdot \text{deg}$$

$$I_{0_B1.DLG}(M, R_f) := \frac{V_{0DLG}(M, R_f)_1 - V_{0DLG}(M, R_f)_4}{M \cdot Z_{L10}} \quad |I_{0_B1.DLG}(0.5, 0)| = 0.4424 \quad \arg(I_{0_B1.DLG}(0.5, 0)) = 90 \cdot \text{deg}$$

$$I_{ABC_B1.DLG}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_B1.DLG}(M, R_f) \\ I_{1_B1.DLG}(M, R_f) \\ I_{2_B1.DLG}(M, R_f) \end{pmatrix} \xrightarrow{|I_{ABC_B1.DLG}(0.5, 0)|} = \begin{pmatrix} 0.1165 \\ 2.7607 \\ 2.7607 \end{pmatrix} \cdot \text{pu} \quad \arg(I_{ABC_B1.DLG}(0.5, 0)) = \begin{pmatrix} -90 \\ 164.8436 \\ 15.1564 \end{pmatrix} \cdot \text{deg}$$

- LVside of transformer (Bus S)

$$I_{1_BS.DLG}(M, R_f) := \frac{V_S \cdot e^{-j \cdot 30 \text{deg}} - V_{1DLG}(M, R_f)_0}{jX_{G11}} \quad |I_{1_BS.DLG}(0.5, 0)| = 1.8179 \cdot \text{pu} \quad \arg(I_{1_BS.DLG}(0.5, 0)) = -120 \cdot \text{deg}$$

$$I_{2_BS.DLG}(M, R_f) := \frac{0 - V_{2DLG}(M, R_f)_0}{jX_{G12}} \quad |I_{2_BS.DLG}(0.5, 0)| = 1.259 \cdot \text{pu} \quad \arg(I_{2_BS.DLG}(0.5, 0)) = 120 \cdot \text{deg}$$

$$I_{0_BS.DLG} := 0$$

$$I_{ABC_BS.DLG}(M, R_f) := A_{012} \cdot \begin{pmatrix} I_{0_BS.DLG} \\ I_{1_BS.DLG}(M, R_f) \\ I_{2_BS.DLG}(M, R_f) \end{pmatrix} \xrightarrow{|I_{ABC_BS.DLG}(0.5, 0)|} = \begin{pmatrix} 1.6128 \\ 1.6128 \\ 3.0769 \end{pmatrix} \cdot \text{pu} \quad \arg(I_{ABC_BS.DLG}(0.5, 0)) = \begin{pmatrix} -162.5359 \\ 162.5359 \\ 0 \end{pmatrix} \cdot \text{deg}$$

- Powerworld Results**

Powerworld does not give a useful number for the fault current.

| Fault Data - Buses | | | | | | |
|--------------------|--------------|-------------|--------------|-------------|--------------|-------------|
| Name | Phase Volt A | Phase Ang A | Phase Volt B | Phase Ang B | Phase Volt C | Phase Ang C |
| BUS S | 0.94216 | -26.68 | 0.94216 | -153.32 | 0.84615 | 90 |
| BUS 1 | 0.96914 | 0 | 0.81412 | -125.09 | 0.81412 | 125.09 |
| BUS 2 | 0.94102 | 0 | 0.51388 | -139.6 | 0.51388 | 139.6 |
| BUS R | 0.85401 | -20.2 | 0.85401 | -159.8 | 0.58974 | 90 |
| FaultPt | 1.22754 | 0 | 0 | 0 | 0 | 0 |

| Fault Data - Lines | | | | | | | |
|--------------------|---------|------------------|------------------|------------------|------------------|------------------|------------------|
| From Name | To Name | Phase Cur A From | Phase Ang A From | Phase Cur B From | Phase Ang B From | Phase Cur C From | Phase Ang C From |
| BUS S | BUS 1 | 1.6128 | -162.54 | 1.6128 | 162.54 | 3.07692 | 0 |
| BUS 1 | BUS 2 | 0 | 0 | 0 | 0 | 0 | 0 |
| BUS 1 | FaultPt | 0.11653 | -90 | 2.76072 | 164.84 | 2.76072 | 15.16 |
| BUS R | BUS 2 | 0.8064 | -162.54 | 0.8064 | 162.54 | 1.53846 | 0 |
| FaultPt | BUS 2 | 0.11653 | -90 | 1.43601 | -21.9 | 1.43601 | -158.1 |