

ECE 523
Symmetrical Components

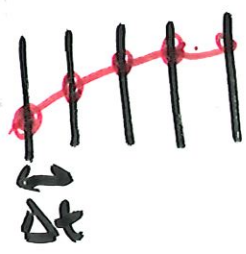
Session 20

20/25
L20

U I	ECE 523 Lecture 19	
	<h2>EMTP Variants</h2>	
<ul style="list-style-type: none">• Original version mainly modeled RLC elements switches, ideal sources and lines• Many extensions and several versions<ul style="list-style-type: none">» ATP: Alternate transients program (http://www.emtp.org)» EMTP-RV (http://www.emtp.com) latest from DCG» EMTDC: student version available free from their web site (http://www.pscad.com/)» RTDS: Real time digital simulator (cost)» SimPowerSystems blockset for Matlab		
Intro to EMTP simulation 7 Fall 2023		

*Hypersim
(Opal-RT)*

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U I	ECE 523 Lecture 19	
	<h2>Using EMT Programs</h2>	
<ul style="list-style-type: none">• Outputs are voltage, current, power, and energy versus time• Control variables are available if controls are modeled• Can model simple controls using EMTs control models or can interface to FORTRAN (in some cases C or Matlab too)<ul style="list-style-type: none">» Programs have internal control modeling» Graphical user interface		
Intro to EMTP simulation 8 Fall 2023		

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U I	The ATP Version		ECE 523 Lecture 19
	<ul style="list-style-type: none">• ATP is essentially free. A license application needs to be filled out (do not choose student license)<ul style="list-style-type: none">» https://www.atp-empt.org/» The purpose is to limit access to parties that have participated in "EMTP-Commerce"		
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U I	ATPDraw		ECE 523 Lecture 19
	<ul style="list-style-type: none">• Available for download from ATP distribution sites• Follow link for ATPDraw for information about the program<ul style="list-style-type: none">» Latest versions are version 7.4» File format not backward compatible» http://www.atpdraw.net/ (ATPDraw only, not ATP itself)• Get the program and the patch files (update to fix bugs in executable)• Manual and introduction presentation for download		
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U I	PSCAD/EMTDC	ECE 523 Lecture 19
		<ul style="list-style-type: none">• Education version available in ECE labs• Free Student Edition (15 node limit)<ul style="list-style-type: none">» Go to: http://www.pscad.com/» Create account and get set up to download<ul style="list-style-type: none">– Download the Program itself– Includes free Fortran Compiler<ul style="list-style-type: none">□ Need unless you have compatible one installed• Website also has tutorials• Remote access on UI computers
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U I	EMTP-RV	ECE 523 Lecture 19
		<ul style="list-style-type: none">• Available in ECE labs• Remotely available on University of Idaho computers• Tutorials available at https://www.emtp-software.com/
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Validation of Models... and Results

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Lecture 19

- Need to have a basic idea of what the transient response should look like
- Test your system with some very predictable cases
- Start from steady-state operating point
- Understanding behavior will be one of the focuses of this course

Intro to EMTP simulation

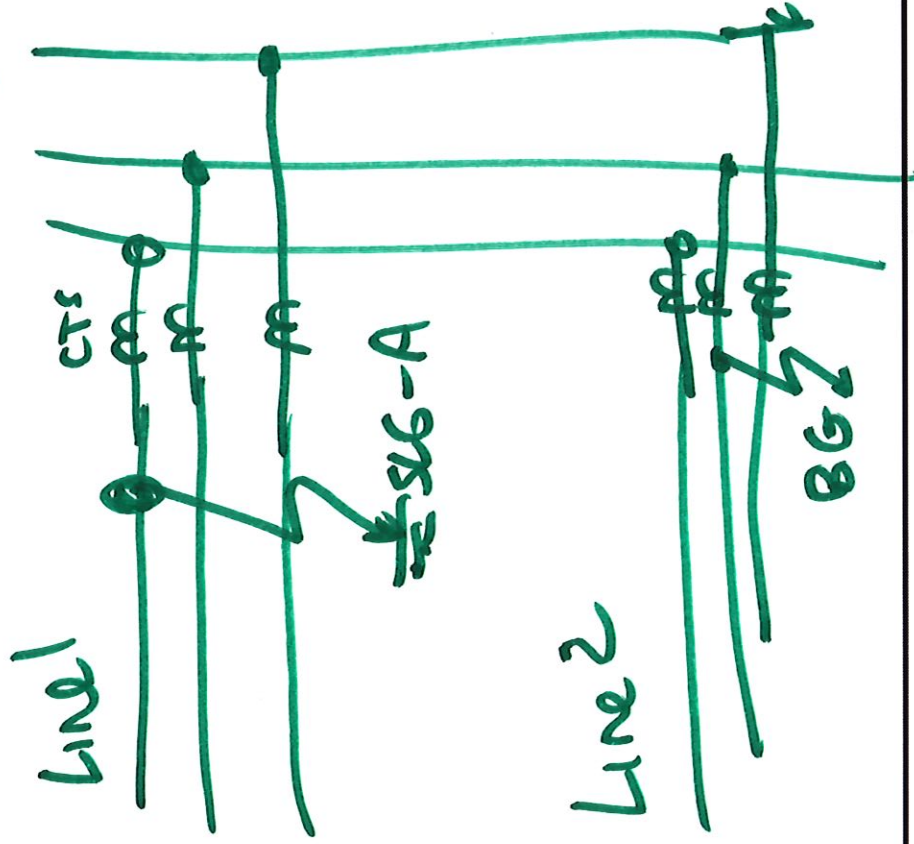
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Simultaneous Faults

- Almost all faults are a single event at a single location



→ two close together faults on different lines

- faults not on system very long

- sometimes two faults are present at same time

that are ~~not~~ unrelated

- or related - for example

• a fault that has a broken conductor → that falls to the ground

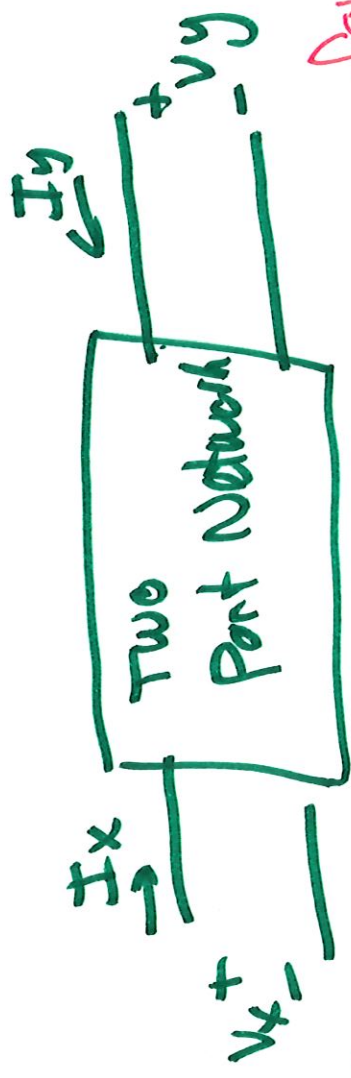
Analysis of Simultaneous Faults

- for faults at one location
or different locations
- 2 part Thevenin Equivalent
 - looking between locations
- we also need to translate
between symmetrical component
reference frames in some cases.

for example

- AG fault at one location \rightarrow A ref components
- and BG at another one - B ref components

Two Port Networks



fault at y

fault at x
 fault at y

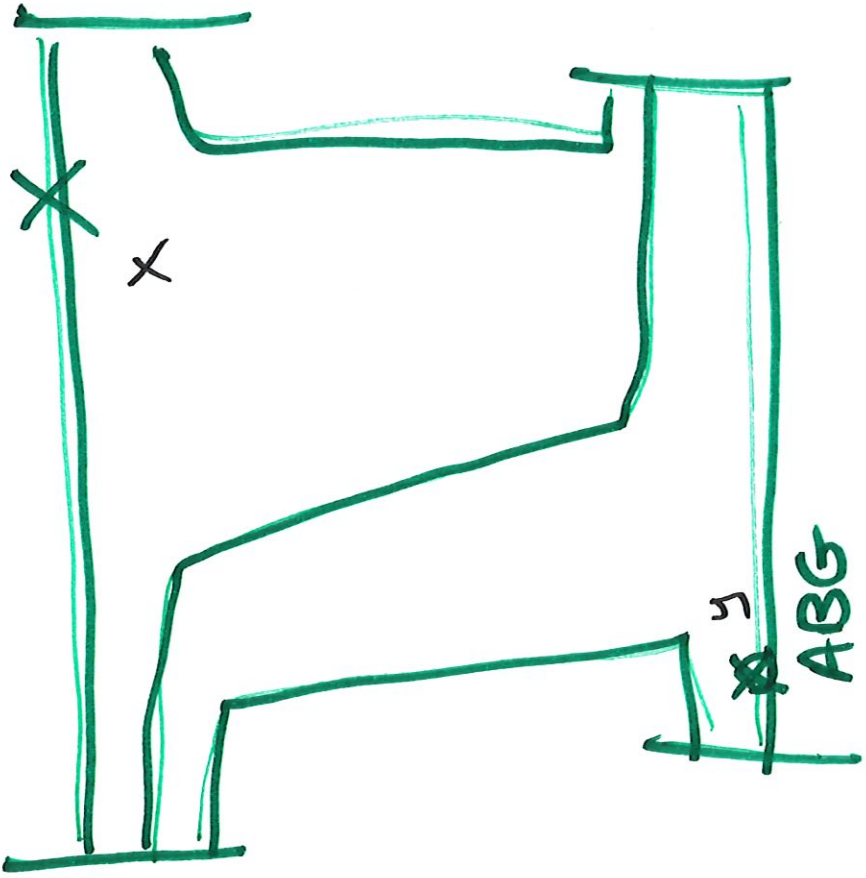
Equivalent

Pos } 3 networks
 Neg }
 Zero }

connectors & P_{in}
 between power system

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SLG-A



- Three types of two port networks for circuit analysis (Section 9.1 + 9.2 in Anderson book)

1. Impedance type (Z-type)

$$\begin{bmatrix} V_{x_{01z}} \\ V_{y_{01z}} \end{bmatrix} = \begin{bmatrix} Z_{xx_{01z}} & Z_{xy_{01z}} \\ Z_{yx_{01z}} & Z_{yy_{01z}} \end{bmatrix} \begin{bmatrix} \bar{I}_{x_{01z}} \\ \bar{I}_{y_{01z}} \end{bmatrix}$$

→ 3 - one each for pos. neg, zero

2. Admittance (Y-type)

$$\begin{bmatrix} \bar{I}_x \\ \bar{I}_y \end{bmatrix} = \begin{bmatrix} \bar{Y}_{xx} & \bar{Y}_{xy} \\ \bar{Y}_{yx} & \bar{Y}_{yy} \end{bmatrix} \begin{bmatrix} V_x \\ V_y \end{bmatrix}$$

3. Hybrid \rightarrow H-type (H-parameters)

$$\begin{bmatrix} V_x \\ I_y \end{bmatrix} = \begin{bmatrix} H_{xx} & H_{xy} \\ H_{yx} & H_{yy} \end{bmatrix} \begin{bmatrix} I_x \\ V_y \end{bmatrix}$$

\rightarrow Some work better series faults
others for shunts

\rightarrow Also voltage source versus current source

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Example: Fault X is SLG on phase A

fault Y is BC fault

SLG on A

- A neg components

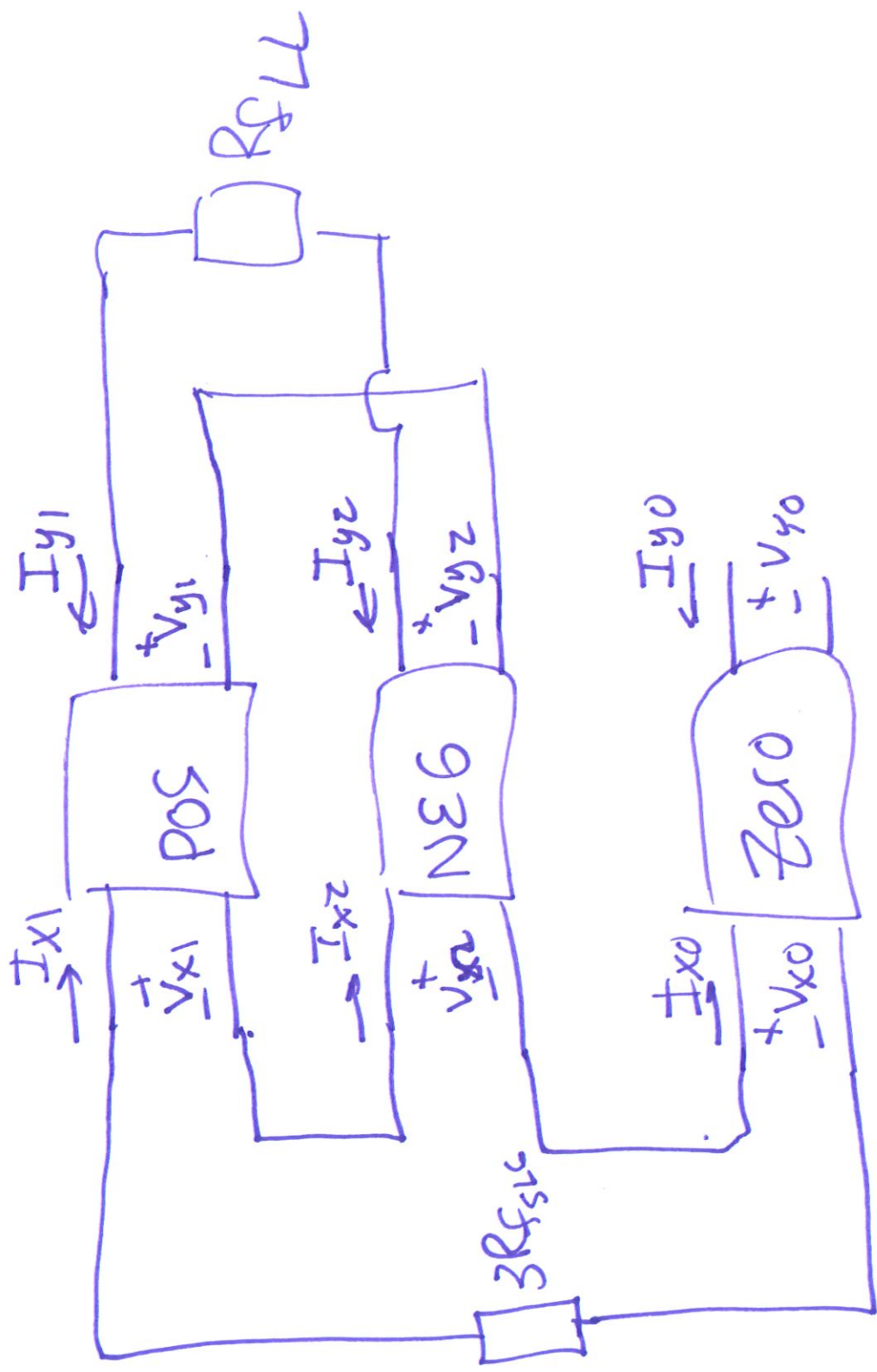
- $I_0 = I_1 = I_2$ at fault locat-

$V_0 + V_1 + V_2 = 3I_0 R_f$ ✓

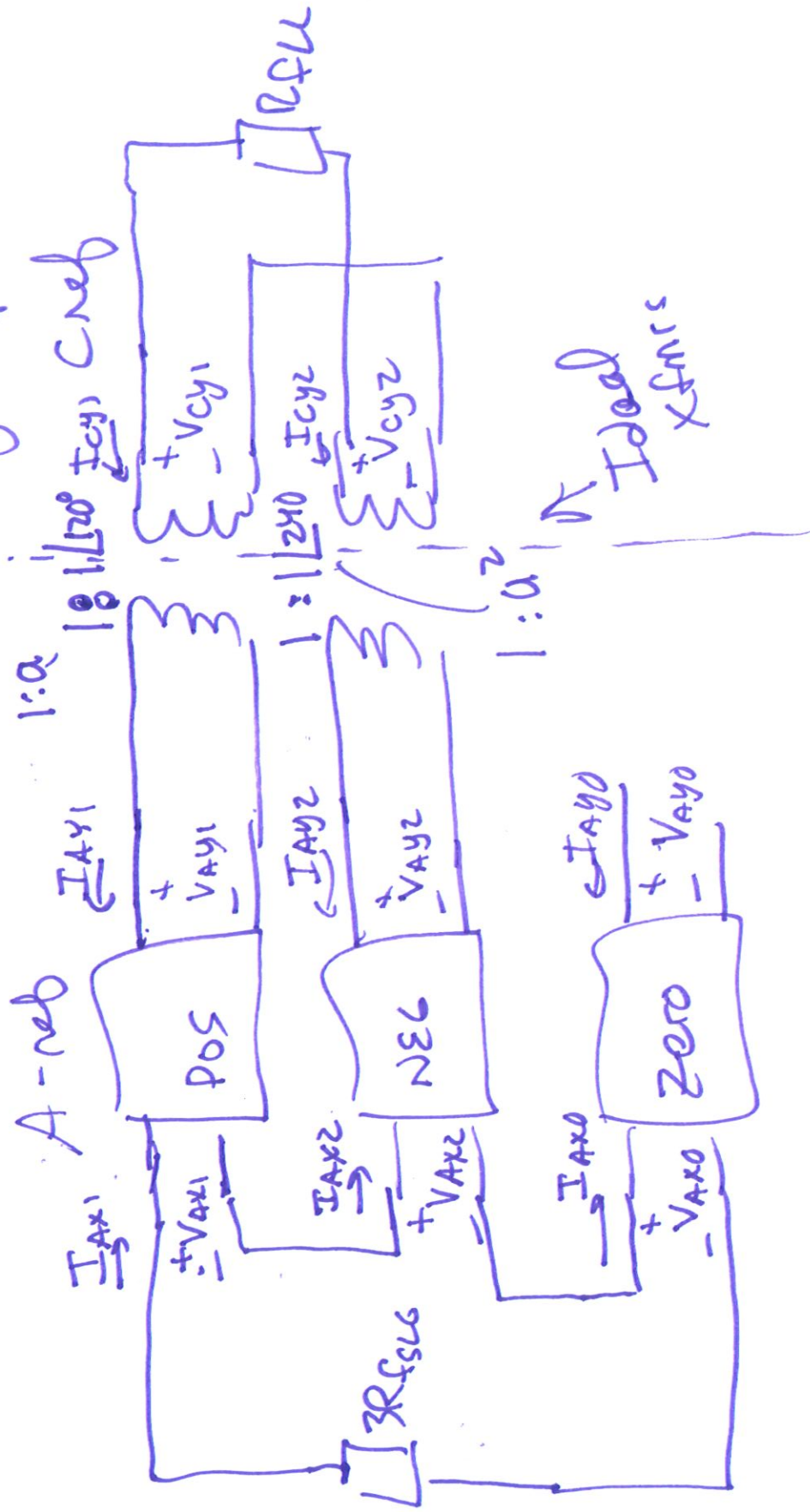
BC $I_1 = -I_2$

$V_1 - V_2 = I_1 R_f$

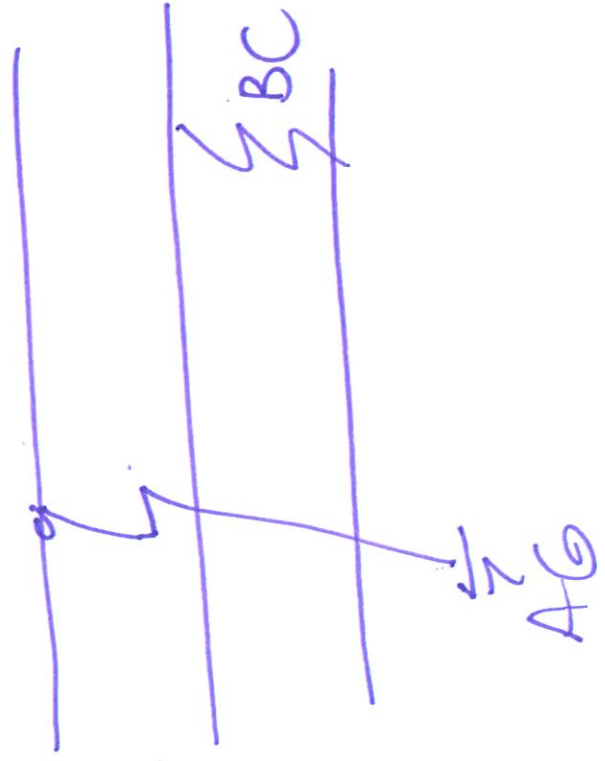
A neg components



Suppose the LL fault is AB fault \rightarrow C neg components



Example → AG & BC
 at same location



ABC constraints

$$SLG: V_{AG} = R_{AG}$$

$$LC \quad I_{BF} = -I_{CF}$$

$$V_{BG} = V_{CG} + R_C I_{BF}$$

$$\begin{bmatrix} I_0 \\ I_1 \\ I_2 \end{bmatrix} = A_{012}^{-1} \begin{bmatrix} I_{Ae} \\ I_{Bf} \\ I_{Cc} \end{bmatrix}$$

~~I_{Bf}~~

$$I_0 = \frac{1}{3} [I_{Ae} + I_{Bf} - I_{Bf}] = \frac{I_{Ae}}{3}$$

$$I_1 = \frac{1}{3} [I_{Ae} + a I_{Bf} - a^2 I_{Bf}]$$

$$I_2 = \frac{1}{3} [I_{Ae} + a^2 I_{Bf} - a I_{Bf}]$$

$$I_1 + I_2 = \frac{1}{3} \left[2 I_{Af} + B_f \left[a - a^2 + 0^2 - a \right] \right]$$

$$I_1 + I_2 = \frac{2}{3} I_{Af} = 2 I_0$$

$$V_{AG} = R_G I_{Af}$$

$$V_{BG} = V_{CG} + R_{fBC} \cdot I_{Bf}$$

for the moment let $R_G = R_{fBC} = 0$

$$V_{AG} = 0 = V_{A0} + V_{A1} + V_{A2}$$

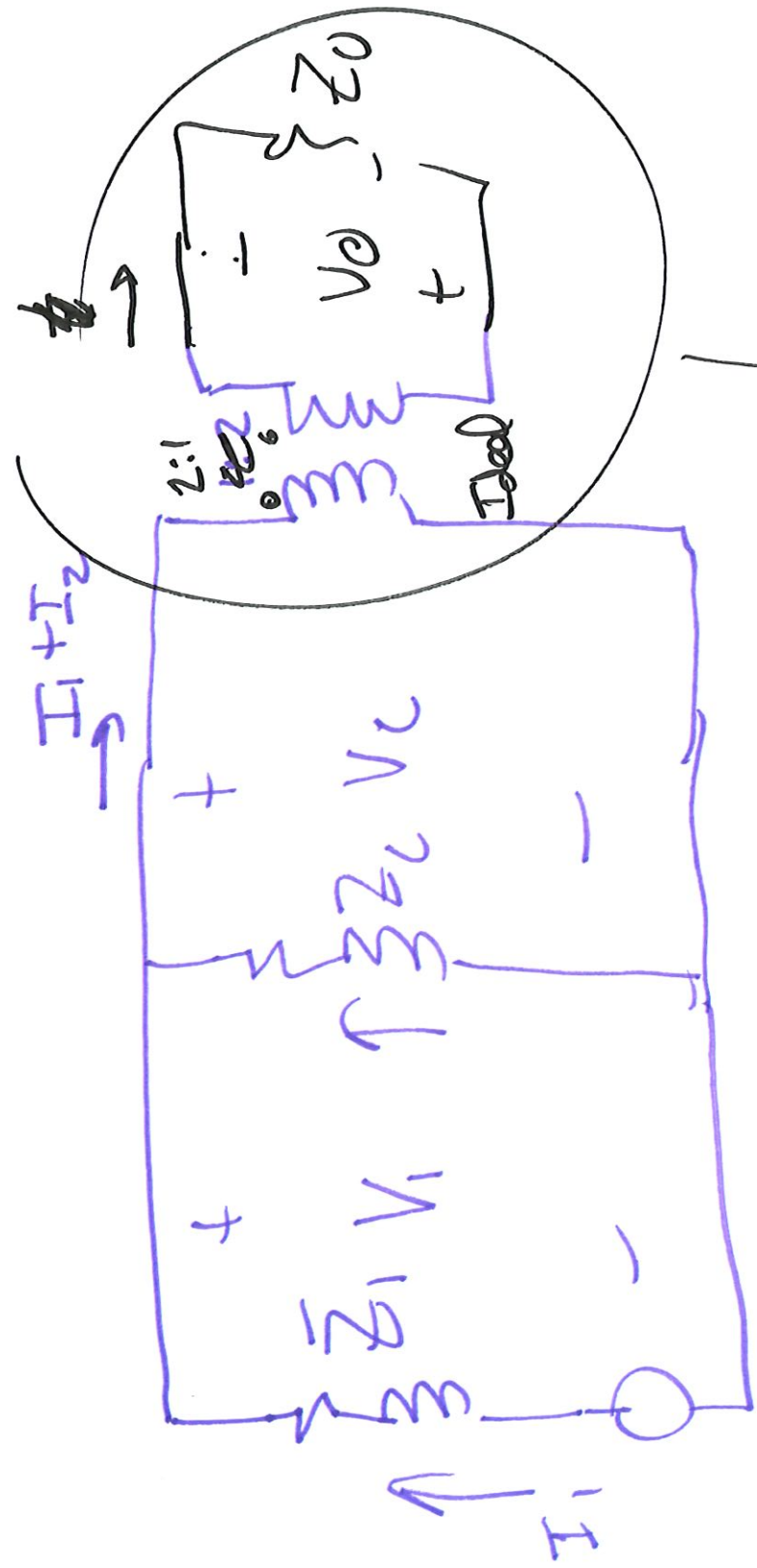
$$V_{BG} = V_{CG} \Rightarrow V_{A1} = V_{A2}$$

Then $V_{AG} = 0 = V_{A0} + V_{A1} + V_{A2}$

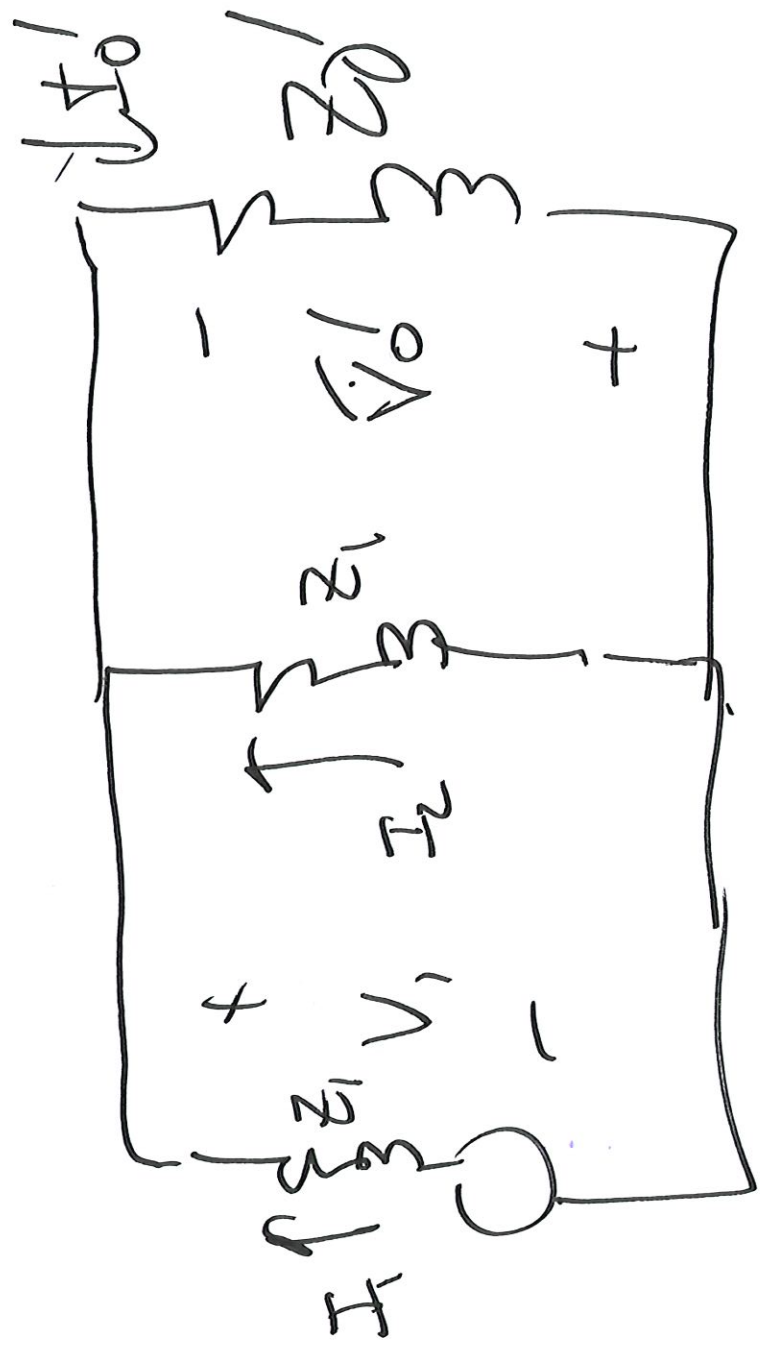
$$0 = V_{A0} + 2V_{A1} = V_{A0} + 2V_{A2}$$

$$V_{A1} = V_{A2} = -\frac{V_{A0}}{2}$$

Since same location we can use a single port equivalent



refer across transformer



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$$Y_{Bus0}(M) := \begin{bmatrix} \frac{1}{Z_{S0}} & 0 & 0 & 0 & 0 \\ 0 & \frac{1}{Z_{T10}} + \frac{1}{M \cdot Z_{L0}} & 0 & 0 & \frac{-1}{M \cdot Z_{L0}} \\ 0 & 0 & \frac{1}{(1-M) \cdot Z_{L0}} + \frac{1}{Z_{T20}} & 0 & \frac{-1}{(1-M) \cdot Z_{L0}} \\ 0 & 0 & 0 & \frac{1}{Z_{R0}} & 0 \\ 0 & \frac{-1}{M \cdot Z_{L0}} & \frac{-1}{(1-M) \cdot Z_{L0}} & 0 & \frac{1}{M \cdot Z_{L0}} + \frac{1}{(1-M) \cdot Z_{L0}} \end{bmatrix}$$

$$Z_{Bus1}(M) := Y_{Bus1}(M)^{-1}$$

$$Z_{Bus2}(M) := Y_{Bus2}(M)^{-1}$$

$$Z_{Bus0}(M) := Y_{Bus0}(M)^{-1}$$

Simultaneous AG and BC faults 30% of the way from Bus 1 to Bus 2

$$I_1 + I_2 = 2 \cdot I_0$$

$$V_1 = V_2 = \frac{-1}{2} \cdot V_0$$

$$V_f := 1.0 \text{ pu} \quad \text{No load}$$

$$M := 0.3$$

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$$I_1 := \frac{V_f}{Z_{Bus1}(M)_{4,4} + \left[\frac{1}{Z_{Bus2}(M)_{4,4}} + \frac{1}{(Z_{Bus0}(M)_{4,4}) \cdot \frac{1}{4}} \right]^{-1}}$$

$|I_1| = 2.055 \text{ pu} \quad \arg(I_1) = -86.871 \text{ deg}$

$$I_2 := -I_1 \cdot \left[\frac{(Z_{Bus0}(M)_{4,4})}{4} + \frac{(Z_{Bus2}(M)_{4,4})}{4} \right]$$

$|I_2| = 0.55 \text{ pu} \quad \arg(I_2) = 91.613 \text{ deg}$

$$I_0 := \frac{I_1}{2} \cdot \left[\frac{Z_{Bus2}(M)_{4,4}}{Z_{Bus2}(M)_{4,4} + \frac{(Z_{Bus0}(M)_{4,4})}{4}} + \frac{Z_{Bus2}(M)_{4,4}}{(Z_{Bus0}(M)_{4,4}) \cdot \frac{1}{4}} \right]$$

$|I_0| = 0.752 \text{ pu} \quad \arg(I_0) = -86.316 \text{ deg}$

Handwritten notes:
 → correct for my current constraints
 $(I_1 + I_2) - 2 \cdot I_0 = 0$

$$V_1 := V_f - I_1 \cdot Z_{Bus1}(M)_{4,4} \quad |V_1| = 0.211 \text{ pu} \quad \arg(V_1) = -1.196 \text{ deg}$$

$$V_2 := -I_2 \cdot Z_{Bus2}(M)_{4,4} \quad |V_2| = 0.211 \text{ pu} \quad \arg(V_2) = -1.196 \text{ deg}$$

$$V_0 := -I_0 \cdot Z_{Bus0}(M)_{4,4} \quad |V_0| = 0.423 \text{ pu} \quad \arg(V_0) = 178.804 \text{ deg}$$

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$$\frac{-V_0}{2} - V_1 = 0$$

$$V_{ABC} := A_{012} \cdot \begin{pmatrix} V_0 \\ V_1 \\ V_2 \end{pmatrix} \quad \vec{V}_{ABC} = \begin{pmatrix} 0 \\ 0.634 \\ 0.634 \end{pmatrix}$$

$$\arg(V_{ABC_1}) = 178.804 \cdot \text{deg}$$

$$\arg(V_{ABC_2}) = 178.804 \cdot \text{deg}$$

Very close to ATP

$$I_{ABC} := A_{012} \cdot \begin{pmatrix} I_0 \\ I_1 \\ I_2 \end{pmatrix} \quad \vec{I}_{ABC} = \begin{pmatrix} 2.257 \\ 2.256 \\ 2.256 \end{pmatrix}$$

$$\vec{\arg(I_{ABC})} = \begin{pmatrix} -86.316 \\ -177.191 \\ 2.809 \end{pmatrix} \cdot \text{deg}$$

SLG or LL alone (without simultaneous):

- SLG

$$I_{0slg} := \frac{V_f}{(Z_{Bus1(M)}{}_{4,4} + Z_{Bus2(M)}{}_{4,4} + Z_{Bus0(M)}{}_{4,4})}$$

$$|I_{0slg}| = 0.752$$

$$\arg(I_{0slg}) = -86.316 \cdot \text{deg}$$

$$I_{A_slg} := 3 \cdot I_{0slg}$$

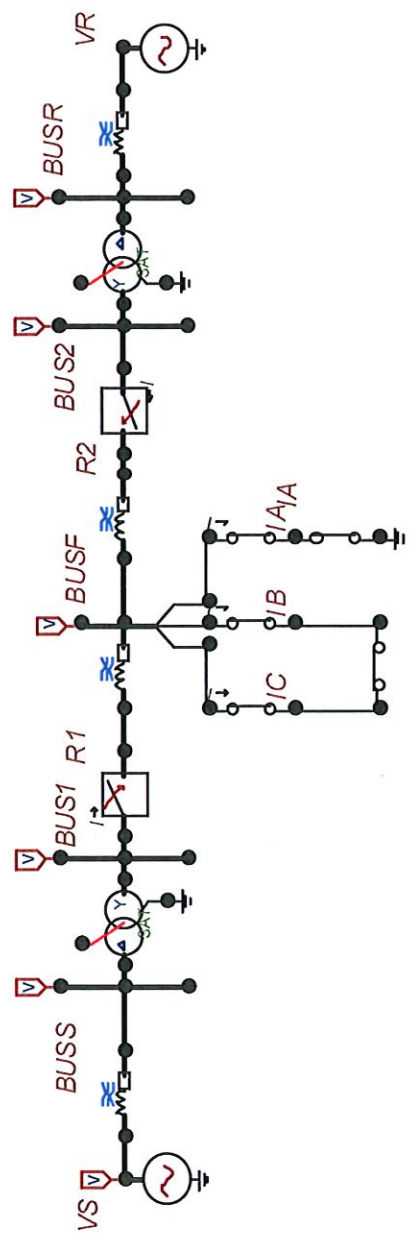
$$|I_{A_slg}| = 2.257 \cdot \text{pu}$$

$$\arg(I_{A_slg}) = -86.316 \cdot \text{deg}$$

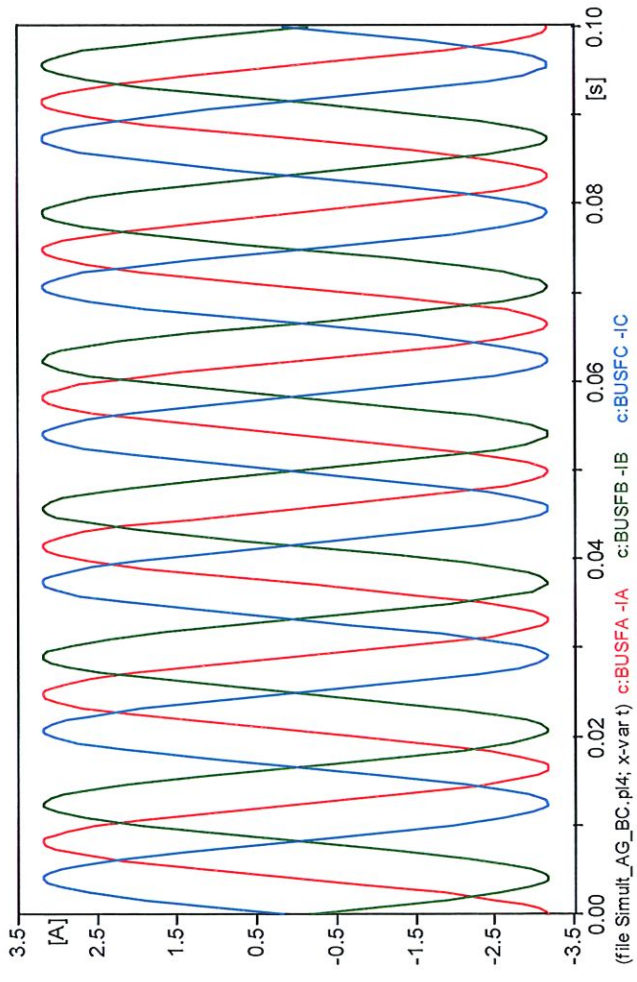
- Same as for simultaneous

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• ATP System Model



• Fault Currents (versus time):



• Note that: $I_C = -I_B$

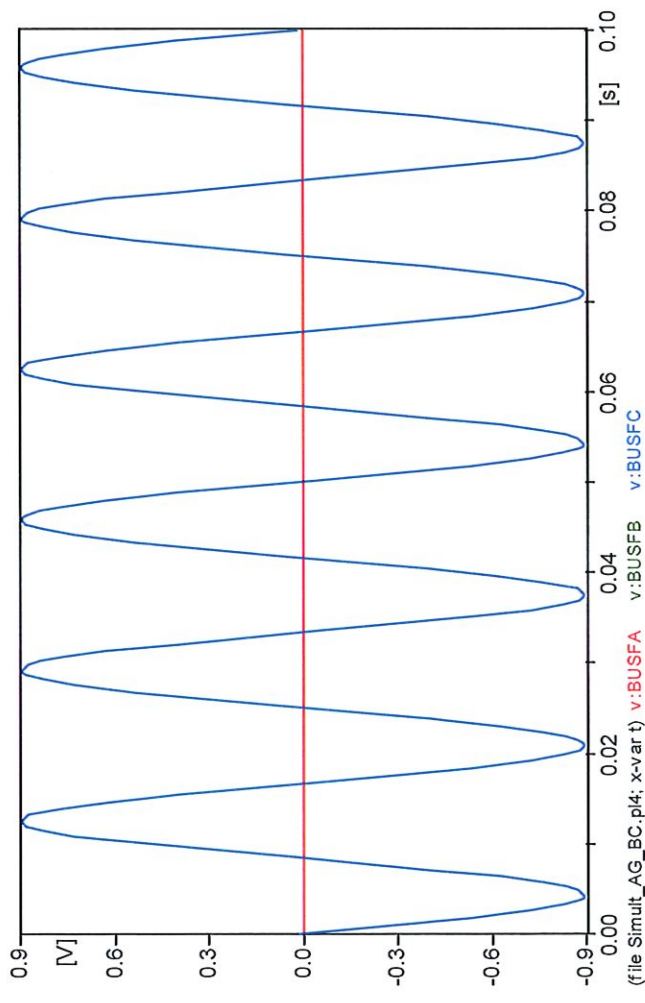
$|I_A| = 2.257A$ $\theta_A := -86.24deg$

$|I_B| = 2.257A$ $\theta_A := -177.1deg$

$|I_C| = 2.257A$ $\theta_A := 2.88deg$

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- Voltages at the fault point:



$$|V_{AG}| = 0V$$

$$|V_{BG}| = 0.6339V \quad \theta_{VB} := 178.9\text{deg}$$

$$|V_{CG}| = 0.6339V \quad \theta_{VC} := 178.9\text{deg}$$

If the faults ~~to~~ not at
same location

