

## Overhead Line Capacitance Calculations

### A. Start with the same line used for the series impedance calculations

- Conductor radius:

$$\text{dia} := 0.528\text{in} \quad r := \frac{\text{dia}}{2}$$

- Space between phase conductors

$$D_{ab} := 10\text{ft} \quad D_{ac} := 20\text{ft} \quad D_{bc} := 10\text{ft}$$

- Height calculations and distance to image conductors

$$H_{\text{tower}} := 45\text{ft} \quad \text{Sag} := 15\text{ft}$$

$$H_a := H_{\text{tower}} - \frac{2}{3} \cdot \text{Sag} \quad H_a = 35 \cdot \text{ft} \quad H_b := H_a \quad H_c := H_a$$

$$H_{aai} := 2 \cdot H_a \quad H_{aai} = 70 \cdot \text{ft}$$

$$H_{bbi} := 2 \cdot H_b \quad H_{cci} := 2 \cdot H_c$$

$$H_{abi} := \sqrt{(2 \cdot H_a)^2 + D_{ab}^2} \quad H_{abi} = 70.71 \cdot \text{ft}$$

$$H_{aci} := \sqrt{(2 \cdot H_a)^2 + D_{ac}^2} \quad H_{aci} = 72.8 \cdot \text{ft}$$

$$H_{bci} := \sqrt{(2 \cdot H_c)^2 + D_{bc}^2} \quad H_{bci} = 70.71 \cdot \text{ft}$$

$$P := \frac{1}{(2 \cdot \pi \cdot \epsilon_0)} \begin{pmatrix} \ln\left(\frac{H_{aai}}{r}\right) & \ln\left(\frac{H_{abi}}{D_{ab}}\right) & \ln\left(\frac{H_{aci}}{D_{ac}}\right) \\ \ln\left(\frac{H_{abi}}{D_{ab}}\right) & \ln\left(\frac{H_{bbi}}{r}\right) & \ln\left(\frac{H_{bci}}{D_{bc}}\right) \\ \ln\left(\frac{H_{aci}}{D_{ac}}\right) & \ln\left(\frac{H_{bci}}{D_{bc}}\right) & \ln\left(\frac{H_{cci}}{r}\right) \end{pmatrix} \quad P = \begin{pmatrix} 0.14 & 0.04 & 0.02 \\ 0.04 & 0.14 & 0.04 \\ 0.02 & 0.04 & 0.14 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

P is matrix of "Potential Coefficients"

$$C' := P^{-1} \quad C' = \begin{pmatrix} 11.93 & -2.58 & -1.29 \\ -2.58 & 12.35 & -2.58 \\ -1.29 & -2.58 & 11.93 \end{pmatrix} \cdot \frac{\text{nF}}{\text{mi}}$$

$$\text{Length} := 40\text{mi}$$

$$C_{\text{untran}} := C' \cdot \text{Length} \quad C_{\text{untran}} = \begin{pmatrix} 0.48 & -0.1 & -0.05 \\ -0.1 & 0.49 & -0.1 \\ -0.05 & -0.1 & 0.48 \end{pmatrix} \cdot \mu\text{F}$$

Transformation Matrix:

$$a := 1 \cdot e^{j \cdot \frac{2 \cdot \pi}{3}} \quad A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix}$$

$$C_{012} := A_{012}^{-1} \cdot C_{\text{untran}} \cdot A_{012}$$

$$C_{012} = \begin{pmatrix} 0.31 & 0.01 + 0.01i & 0.01 - 0.01i \\ 0.01 - 0.01i & 0.57 & -0.02 - 0.03i \\ 0.01 + 0.01i & -0.02 + 0.03i & 0.57 \end{pmatrix} \cdot \mu\text{F}$$

- Note the complex capacitance values in the off diagonal terms.

$$C_0 := C_{012}_{0,0} \quad C_0 = 310.93 \cdot \text{nF}$$

$$C_1 := C_{012}_{1,1} \quad C_1 = 568.93 \cdot \text{nF} \quad C_{012}_{1,1} - C_{012}_{2,2} = 0 \cdot \text{nF} \quad \text{So } C_2 = C_1$$

- If we use the per phase capacitance formulas:

$$D_m := (D_{ab} \cdot D_{ac} \cdot D_{bc})^{\frac{1}{3}} \quad D_m = 12.6 \cdot \text{ft}$$

$$c_{\text{phase}} := \frac{2 \cdot \pi \cdot \epsilon_0}{\ln\left(\frac{D_m}{r}\right)} \quad c_{\text{phase}} = 8.761 \cdot \frac{\text{pF}}{\text{m}} \quad c_{\text{phase}} \cdot \text{Length} = 563.95 \cdot \text{nF}$$

Note that the per phase capacitance per length doesn't quite match the positive and negative sequence capacitance, as we discussed earlier, this is because the conductor height is left out. Modify the expression:

$$GMH := \left( \frac{H_{abi} \cdot H_{aci} \cdot H_{bci}}{H_{aai} \cdot H_{bbi} \cdot H_{c ci}} \right)^{\frac{1}{3}} \quad GMH = 1.02$$

$$C_{\text{phase\_cor}} := \frac{2 \cdot \pi \cdot \epsilon_0}{\ln\left(\frac{D_m}{r}\right) - \ln(GMH)}$$

$$C_{\text{phase\_cor}} = 8.79 \cdot \frac{\text{pF}}{\text{m}} \quad C_{\text{phase\_cor}} \cdot \text{Length} = 565.71 \cdot \text{nF} \quad C_1 = 568.93 \cdot \text{nF}$$

This is a lot closer, but still off a little bit.

- There are several formulas that can be used for the zero sequence capacitance.

$$H_{abc} := (H_{abi} \cdot H_{aci} \cdot H_{bci})^{\frac{1}{3}}$$

$$H_{aa} := (H_a \cdot H_b \cdot H_c)^{\frac{1}{3}}$$

- From Siemens:

$$C_{\text{zero\_siemens}} := \frac{2 \cdot \pi \cdot \epsilon_0}{\ln\left(\frac{2 \cdot H_{aa} \cdot H_{abc}^2}{r \cdot D_m^2}\right)}$$

$$C_{\text{zero\_siemens}} = 4.82 \cdot \frac{\text{pF}}{\text{m}}$$

$$C0\_S := 40 \text{mi} \cdot C_{\text{zero\_siemens}}$$

$$C0\_S = 310.482 \cdot \text{nF}$$

Or from the Westinghouse T&D manual

$$C_{\text{zero\_west}} := \frac{2 \cdot \pi \cdot \epsilon_0}{\ln\left[\frac{(2 \cdot H_{aa})^3}{r \cdot D_m^2}\right]}$$

$$C_{\text{zero\_west}} = 4.84 \cdot \frac{\text{pF}}{\text{m}}$$

$$C0\_W := 40mi \cdot C\_zero\_west \quad C0\_W = 311.552 \cdot nF \quad C_0 = 310.93 \cdot nF$$

### Transposed Line Examples:

$$R_p := \begin{pmatrix} 0 & 0 & 1 \\ 1 & 0 & 0 \\ 0 & 1 & 0 \end{pmatrix}$$

Transpose Case 1:

$$f1 := 0.2 \quad f2 := 0.3 \quad f3 := 0.5$$

$$C_{net} := f1 \cdot C_{untran} + f2 \cdot R_p^{-1} \cdot C_{untran} \cdot R_p + f3 \cdot R_p \cdot C_{untran} \cdot R_p^{-1}$$

$$C_{net} = \begin{pmatrix} 0.48 & -0.08 & -0.09 \\ -0.08 & 0.48 & -0.09 \\ -0.09 & -0.09 & 0.49 \end{pmatrix} \cdot \mu F$$

$$C_{0121} := A_{012}^{-1} \cdot C_{net} \cdot A_{012}$$

$$C_{0121} = \begin{pmatrix} 0.31 & 5.84 \times 10^{-4} - 0i & 5.84 \times 10^{-4} + 0i \\ 5.84 \times 10^{-4} + 0i & 0.57 & -0 + 0.01i \\ 5.84 \times 10^{-4} - 0i & -0 - 0.01i & 0.57 \end{pmatrix} \cdot \mu F$$

Transposition Case 2:

$$f13 := 0.4 \quad f23 := 0.6 \quad f33 := 0.0$$

$$C_{net3} := f13 \cdot C_{untran} + f23 \cdot R_p^{-1} \cdot C_{untran} \cdot R_p + f33 \cdot R_p \cdot C_{untran} \cdot R_p^{-1}$$

$$C_{net3} = \begin{pmatrix} 0.49 & -0.1 & -0.08 \\ -0.1 & 0.48 & -0.07 \\ -0.08 & -0.07 & 0.48 \end{pmatrix} \cdot \mu F$$

$$C_{0123} := A_{012}^{-1} \cdot C_{net3} \cdot A_{012}$$

$$C_{0123} = \begin{pmatrix} 0.31 & -0 + 0i & -0 - 0i \\ -0 - 0i & 0.57 & 0.02 - 0.01i \\ -0 + 0i & 0.02 + 0.01i & 0.57 \end{pmatrix} \cdot \mu F$$

Transposition Case 3:

$$f_{16} := \frac{1}{3} \quad f_{26} := \frac{1}{3} \quad f_{36} := \frac{1}{3}$$

$$C_{net6} := f_{16} \cdot C_{untran} + f_{26} \cdot R_p^{-1} \cdot C_{untran} \cdot R_p + f_{36} \cdot R_p \cdot C_{untran} \cdot R_p^{-1}$$

$$C_{net6} = \begin{pmatrix} 0.48 & -0.09 & -0.09 \\ -0.09 & 0.48 & -0.09 \\ -0.09 & -0.09 & 0.48 \end{pmatrix} \cdot \mu F$$

$$C_{0126} := A_{012}^{-1} \cdot C_{net6} \cdot A_{012}$$

$$C_{0126} = \begin{pmatrix} 0.3109 & 0 & 0 \\ 0 & 0.5689 & 0 \\ 0 & 0 & 0.5689 \end{pmatrix} \cdot \mu F$$

### Line with two conductor bundles

Conductor data from table:

$$dia2 := 1.108in \quad rad2 := \frac{dia2}{2} \quad rad2 = 0.05 \cdot ft$$

Spacing:

Within the bundle:

$$Da1a2 := 1.5ft \quad Db1b2 := 1.5ft \quad Dc1c2 := 1.5ft$$

Between Phases

$$Da1b1 := 24ft \quad Da1b2 := Da1b1 + Db1b2 \quad Da1b2 = 25.5 \cdot ft$$

$$Da2b1 := Da1b1 - Da1a2 \quad Da2b1 = 22.5 \cdot ft \quad Da2b2 := 24ft$$

$$Da1c1 := 48\text{ft}$$

$$Da1c2 := Da1c1 + Dc1c2$$

$$Da1c2 = 49.5\cdot\text{ft}$$

$$Da2c1 := Da1c1 - Da1a2$$

$$Da2c1 = 46.5\cdot\text{ft}$$

$$Da2c2 := 48\text{ft}$$

$$Db1c1 := 24\text{ft}$$

$$Db1c2 := Db1c1 + Dc1c2$$

$$Db1c2 = 25.5\cdot\text{ft}$$

$$Db2c1 := Db1c1 - Db1b2$$

$$Db2c1 = 22.5\cdot\text{ft}$$

$$Db2c2 := 24\text{ft}$$

Height Calculations (assume same height as above). Use symmetry, so don't compute all permutations.

$$Ha1a1i := 2\cdot Ha$$

$$Hb1b1i := 2\cdot Hb$$

$$Hc1c1i := 2\cdot Hc$$

$$Ha2a2i := 2\cdot Ha$$

$$Hb2b2i := 2\cdot Hb$$

$$Hc2c2i := 2\cdot Hc$$

$$Ha1a2i := \sqrt{(2\cdot Ha)^2 + Da1a2^2}$$

$$Hb1b2i := \sqrt{(2\cdot Hb)^2 + Db1b2^2}$$

$$Ha1b1i := \sqrt{(2\cdot Ha)^2 + Da1b1^2}$$

$$Ha1b2i := \sqrt{(2\cdot Ha)^2 + Da1b2^2}$$

$$Ha1c1i := \sqrt{(2\cdot Ha)^2 + Da1c1^2}$$

$$Ha1c2i := \sqrt{(2\cdot Ha)^2 + Da1c2^2}$$

$$Hb1c1i := \sqrt{(2\cdot Hb)^2 + Db1c1^2}$$

$$Hb1c2i := \sqrt{(2\cdot Hb)^2 + Db1c2^2}$$

$$Hc1c2i := \sqrt{(2\cdot Hc)^2 + Dc1c2^2}$$

$$Ha2b2i := \sqrt{(2\cdot Ha)^2 + Da2b2^2}$$

$$Ha2b1i := \sqrt{(2\cdot Ha)^2 + Da2b1^2}$$

$$Ha2c2i := \sqrt{(2\cdot Ha)^2 + Da2c2^2}$$

$$Ha2c1i := \sqrt{(2\cdot Ha)^2 + Da2c1^2}$$

$$Hb2c1i := \sqrt{(2\cdot Hb)^2 + Db2c1^2}$$

$$Hb2c2i := \sqrt{(2\cdot Hb)^2 + Db2c2^2}$$

$$P_u := \frac{1}{2 \cdot \pi \cdot \epsilon_0} \begin{bmatrix} \ln\left[\frac{(Ha1a1i)}{\text{rad}2}\right] & \ln\left(\frac{Ha1b1i}{Da1b1}\right) & \ln\left(\frac{Ha1c1i}{Da1c1}\right) & \ln\left(\frac{Ha1a2i}{Da1a2}\right) & \ln\left(\frac{Ha1b2i}{Da1b2}\right) & \ln\left(\frac{Ha1c2i}{Da1c2}\right) \\ \ln\left(\frac{Ha1b1i}{Da1b1}\right) & \ln\left[\frac{(Hb1b1i)}{\text{rad}2}\right] & \ln\left(\frac{Hb1c1i}{Db1c1}\right) & \ln\left(\frac{Ha2b1i}{Da2b1}\right) & \ln\left(\frac{Hb1b2i}{Db1b2}\right) & \ln\left(\frac{Hb1c2i}{Db1c2}\right) \\ \ln\left(\frac{Ha1c1i}{Da1c1}\right) & \ln\left(\frac{Hb1c1i}{Db1c1}\right) & \ln\left[\frac{(Hc1c1i)}{\text{rad}2}\right] & \ln\left(\frac{Ha2c1i}{Da2c1}\right) & \ln\left(\frac{Hb2c1i}{Db2c1}\right) & \ln\left(\frac{Hc1c2i}{Dc1c2}\right) \\ \ln\left(\frac{Ha1a2i}{Da1a2}\right) & \ln\left(\frac{Ha2b1i}{Da2b1}\right) & \ln\left(\frac{Ha2c1i}{Da2c1}\right) & \ln\left[\frac{(Ha2a2i)}{\text{rad}2}\right] & \ln\left(\frac{Ha2b2i}{Da2b2}\right) & \ln\left(\frac{Ha2c2i}{Da2c2}\right) \\ \ln\left(\frac{Ha1b2i}{Da1b2}\right) & \ln\left(\frac{Hb1b2i}{Db1b2}\right) & \ln\left(\frac{Hb2c1i}{Db2c1}\right) & \ln\left(\frac{Ha2b2i}{Da2b2}\right) & \ln\left[\frac{(Hb2b2i)}{\text{rad}2}\right] & \ln\left(\frac{Hb2c2i}{Db2c2}\right) \\ \ln\left(\frac{Ha1c2i}{Da1c2}\right) & \ln\left(\frac{Hb1c2i}{Db1c2}\right) & \ln\left(\frac{Hc1c2i}{Dc1c2}\right) & \ln\left(\frac{Ha2c2i}{Da2c2}\right) & \ln\left(\frac{Hb2c2i}{Db2c2}\right) & \ln\left[\frac{(Hc2c2i)}{\text{rad}2}\right] \end{bmatrix}$$

$$P_u = \begin{pmatrix} 0.13 & 0.02 & 0.01 & 0.07 & 0.02 & 0.01 \\ 0.02 & 0.13 & 0.02 & 0.02 & 0.07 & 0.02 \\ 0.01 & 0.02 & 0.13 & 0.01 & 0.02 & 0.07 \\ 0.07 & 0.02 & 0.01 & 0.13 & 0.02 & 0.01 \\ 0.02 & 0.07 & 0.02 & 0.02 & 0.13 & 0.02 \\ 0.01 & 0.02 & 0.07 & 0.01 & 0.02 & 0.13 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$C_{\text{bund}} := P_u^{-1} = \begin{pmatrix} 10.58 & -0.49 & -0.17 & -5.38 & -0.41 & -0.15 \\ -0.49 & 10.68 & -0.48 & -0.58 & -5.3 & -0.41 \\ -0.17 & -0.48 & 10.62 & -0.18 & -0.58 & -5.38 \\ -5.38 & -0.58 & -0.18 & 10.62 & -0.48 & -0.17 \\ -0.41 & -5.3 & -0.58 & -0.48 & 10.68 & -0.49 \\ -0.15 & -0.41 & -5.38 & -0.17 & -0.49 & 10.58 \end{pmatrix} \cdot \frac{\text{pF}}{\text{m}}$$

If length = 40 miles:

$$C_{\text{line\_bu}} := C_{\text{bund}} \cdot 40 \text{mi}$$

$$C_{\text{line\_bu}} = \begin{pmatrix} 0.68 & -0.03 & -0.01 & -0.35 & -0.03 & -0.01 \\ -0.03 & 0.69 & -0.03 & -0.04 & -0.34 & -0.03 \\ -0.01 & -0.03 & 0.68 & -0.01 & -0.04 & -0.35 \\ -0.35 & -0.04 & -0.01 & 0.68 & -0.03 & -0.01 \\ -0.03 & -0.34 & -0.04 & -0.03 & 0.69 & -0.03 \\ -0.01 & -0.03 & -0.35 & -0.01 & -0.03 & 0.68 \end{pmatrix} \cdot \mu\text{F}$$

Matrix Reduction (note this is done to the P matrix:

$$P_a := \text{submatrix}(P_u, 0, 2, 0, 2)$$

$$P_a = \begin{pmatrix} 0.13 & 0.02 & 0.01 \\ 0.02 & 0.13 & 0.02 \\ 0.01 & 0.02 & 0.13 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$P_b := \text{submatrix}(P_u, 0, 2, 3, 5)$$

$$P_b = \begin{pmatrix} 0.07 & 0.02 & 0.01 \\ 0.02 & 0.07 & 0.02 \\ 0.01 & 0.02 & 0.07 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$P_c := \text{submatrix}(P_u, 3, 5, 0, 2)$$

$$P_c = \begin{pmatrix} 0.07 & 0.02 & 0.01 \\ 0.02 & 0.07 & 0.02 \\ 0.01 & 0.02 & 0.07 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$P_d := \text{submatrix}(P_u, 3, 5, 3, 5)$$

$$P_d = \begin{pmatrix} 0.13 & 0.02 & 0.01 \\ 0.02 & 0.13 & 0.02 \\ 0.01 & 0.02 & 0.13 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

Modify matrix by performing:  $Q_a'b'c' - Q_{abc}$  and  $V_{abc} + V_a'b'c'$  similar to what was done for series  $Z_{abc}$

$$P_{b\text{new}} := P_b - P_a \quad P_{c\text{new}} := P_c - P_a \quad P_{d\text{new}} := P_a - P_b - P_c + P_d$$

Reduce to equivalent 3x3 matrix

$$P_{\text{equiv}} := P_a - P_{b\text{new}} \cdot P_{d\text{new}}^{-1} \cdot P_{c\text{new}}$$



$$P_{\text{equiv}} = \begin{pmatrix} 0.1 & 0.02 & 0.01 \\ 0.02 & 0.1 & 0.02 \\ 0.01 & 0.02 & 0.1 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}} \quad C_{\text{equiv}} := P_{\text{equiv}}^{-1}$$

$$C_{\text{equiv}} = \begin{pmatrix} 10.43 & -1.97 & -0.67 \\ -1.97 & 10.76 & -1.97 \\ -0.67 & -1.97 & 10.43 \end{pmatrix} \cdot \frac{\text{pF}}{\text{m}} \quad C_{\text{equiv\_len}} := C_{\text{equiv}} \cdot \text{Length}$$

$$C_{0128} := A_{012}^{-1} \cdot C_{\text{equiv\_len}} \cdot A_{012}$$

$$C_{0128} = \begin{pmatrix} 0.48 & 0.01 + 0.02i & 0.01 - 0.02i \\ 0.01 - 0.02i & 0.78 & -0.03 - 0.05i \\ 0.01 + 0.02i & -0.03 + 0.05i & 0.78 \end{pmatrix} \cdot \mu\text{F}$$

Note that the original C012 was:

$$C_{012} = \begin{pmatrix} 0.31 & 0.01 + 0.01i & 0.01 - 0.01i \\ 0.01 - 0.01i & 0.57 & -0.02 - 0.03i \\ 0.01 + 0.01i & -0.02 + 0.03i & 0.57 \end{pmatrix} \cdot \mu\text{F}$$

Compare what the bundling has done to the sequence capacitances

Now if we had instead used the approximations of using the GMR of the bundle

$$R_{\text{bundle}} := \sqrt{\text{rad}^2 \cdot D_{a1a2}}$$

$$P_{\text{equivbund}} := \frac{1}{2 \cdot \pi \cdot \epsilon_0} \cdot \begin{pmatrix} \ln\left(\frac{H_{aai}}{R_{\text{bundle}}}\right) & \ln\left(\frac{H_{abi}}{D_{a1b1}}\right) & \ln\left(\frac{H_{aci}}{D_{a1c1}}\right) \\ \ln\left(\frac{H_{abi}}{D_{a1b1}}\right) & \ln\left(\frac{H_{bbi}}{R_{\text{bundle}}}\right) & \ln\left(\frac{H_{bci}}{D_{b1c1}}\right) \\ \ln\left(\frac{H_{aci}}{D_{a1c1}}\right) & \ln\left(\frac{H_{bci}}{D_{b1c1}}\right) & \ln\left(\frac{H_{cc1}}{R_{\text{bundle}}}\right) \end{pmatrix}$$

$$C_{\text{equivbund}} := P_{\text{equivbund}}^{-1} \cdot \text{Length}$$

$$C_{equivbund} = \begin{pmatrix} 667.35 & -124.16 & -25.76 \\ -124.16 & 689.46 & -124.16 \\ -25.76 & -124.16 & 667.35 \end{pmatrix} \cdot nF$$

Error between these methods:

$$Error := C_{equiv\_len} - C_{equivbund} \quad Error = \begin{pmatrix} 4.098 & -2.685 & -17.278 \\ -2.685 & 3.243 & -2.685 \\ -17.278 & -2.685 & 4.098 \end{pmatrix} \cdot nF$$

Or calculating the sequence capacitance

$$C_{0128e} := A_{012}^{-1} \cdot C_{equivbund} \cdot A_{012}$$

$$C_{0128e} = \begin{pmatrix} 492 & 12.72 + 22.03i & 12.72 - 22.03i \\ 12.72 - 22.03i & 766.08 & -36.49 - 63.2i \\ 12.72 + 22.03i & -36.49 + 63.2i & 766.08 \end{pmatrix} \cdot nF$$

$$Err := C_{0128} - C_{0128e}$$

$$Err = \begin{pmatrix} -11.285 & -2.29 - 3.966i & -2.29 + 3.966i \\ -2.29 + 3.966i & 11.362 & 5.007 + 8.672i \\ -2.29 - 3.966i & 5.007 - 8.672i & 11.362 \end{pmatrix} \cdot nF$$

This is comparable to what we saw for the impedance

**Now consider a static wire case:**

- Consider two GW options

$$\text{dia}_{\text{gw}_375\text{in}} := 0.385\text{in} \quad \text{dia}_{\text{gw}1\text{F}} := 0.346\text{in}$$

$$\text{Dagw} := \sqrt{(10\text{ft})^2 + (15\text{ft})^2} \quad \text{Dcgw} := \text{Dagw} \quad \text{Dbgw} := 15\text{ft}$$

$$\text{Hgw}_{\text{tower}} := 60\text{ft} \quad \text{Sag}_{\text{gw}} := 15\text{ft} \quad \bullet \text{ Note that sag for ground wire is often different than for phase conductors. This will impact distance between phase conductors and ground wire}$$

$$\text{Hgw} := \text{Hgw}_{\text{tower}} - \frac{2}{3} \cdot \text{Sag}_{\text{gw}} \quad \text{Hgw} = 50 \cdot \text{ft} \quad \text{Hgw}_{\text{gwi}} := 2 \cdot \text{Hgw}$$

$$\text{Hagwi} := \sqrt{(2 \cdot \text{Ha} + \text{Dbgw})^2 + \text{Dab}^2} \quad \text{Hagwi} = 85.59 \cdot \text{ft}$$

$$\text{Hcgwi} := \sqrt{(2 \cdot \text{Hc} + \text{Dbgw})^2 + \text{Dbc}^2} \quad \text{Hcgwi} = 85.59 \cdot \text{ft}$$

$$\text{Hbgwi} := 2 \cdot \text{Hb} + \text{Dbgw} \quad \text{Hbgwi} = 85 \cdot \text{ft}$$

First Ground Wire Case: 3/8" copperweld

$$\text{P}_{\text{gw}1} := \frac{1}{2\pi \cdot \epsilon_0} \cdot \begin{pmatrix} \ln\left(\frac{\text{Haai}}{r}\right) & \ln\left(\frac{\text{Habi}}{\text{Dab}}\right) & \ln\left(\frac{\text{Haci}}{\text{Dac}}\right) & \ln\left(\frac{\text{Hagwi}}{\text{Dagw}}\right) \\ \ln\left(\frac{\text{Habi}}{\text{Dab}}\right) & \ln\left(\frac{\text{Hbbi}}{r}\right) & \ln\left(\frac{\text{Hbci}}{\text{Dbc}}\right) & \ln\left(\frac{\text{Hbgwi}}{\text{Dbgw}}\right) \\ \ln\left(\frac{\text{Haci}}{\text{Dac}}\right) & \ln\left(\frac{\text{Hbci}}{\text{Dbc}}\right) & \ln\left(\frac{\text{Hcci}}{r}\right) & \ln\left(\frac{\text{Hcgwi}}{\text{Dcgw}}\right) \\ \ln\left(\frac{\text{Hagwi}}{\text{Dagw}}\right) & \ln\left(\frac{\text{Hbgwi}}{\text{Dbgw}}\right) & \ln\left(\frac{\text{Hcgwi}}{\text{Dcgw}}\right) & \ln\left(\frac{\text{Hgw}_{\text{gwi}}}{\frac{\text{dia}_{\text{gw}_375\text{in}}}{2}}\right) \end{pmatrix}$$

$$\text{P}_{\text{gw}1} = \begin{pmatrix} 0.14 & 0.04 & 0.02 & 0.03 \\ 0.04 & 0.14 & 0.04 & 0.03 \\ 0.02 & 0.04 & 0.14 & 0.03 \\ 0.03 & 0.03 & 0.03 & 0.16 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

Matrix Reduction (note this is done to the P matrix:

$$\text{Pagw1} := \text{submatrix}(\text{Pgw1}, 0, 2, 0, 2) \quad \text{Pagw1} = \begin{pmatrix} 0.14 & 0.04 & 0.02 \\ 0.04 & 0.14 & 0.04 \\ 0.02 & 0.04 & 0.14 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Pbgw1} := \text{submatrix}(\text{Pgw1}, 0, 2, 3, 3) \quad \text{Pbgw1} = \begin{pmatrix} 0.03 \\ 0.03 \\ 0.03 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Pcgw1} := \text{submatrix}(\text{Pgw1}, 3, 3, 0, 2) \quad \text{Pcgw1} = (0.03 \ 0.03 \ 0.03) \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Pdgw1} := \text{submatrix}(\text{Pgw1}, 3, 3, 3, 3) \quad \text{Pdgw1} = (0.16) \cdot \frac{\text{m}}{\text{pF}}$$

Reduce to equivalent 3x3 matrix

$$\text{Pequivgw1} := \text{Pagw1} - \text{Pbgw1} \cdot \text{Pdgw1}^{-1} \cdot \text{Pcgw1} \quad \text{Pequivgw1} = \begin{pmatrix} 0.14 & 0.03 & 0.02 \\ 0.03 & 0.14 & 0.03 \\ 0.02 & 0.03 & 0.14 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Cequivgw1} := \text{Pequivgw1}^{-1} \cdot \text{Length} \quad \text{Cequivgw1} = \begin{pmatrix} 0.49 & -0.09 & -0.04 \\ -0.09 & 0.5 & -0.09 \\ -0.04 & -0.09 & 0.49 \end{pmatrix} \cdot \mu\text{F}$$

$$\text{C}_{012\text{gw1}} := \text{A}_{012}^{-1} \cdot \text{Cequivgw1} \cdot \text{A}_{012}$$

$$\text{C}_{012\text{gw1}} = \begin{pmatrix} 337.06 & 5.4 + 9.35i & 5.4 - 9.35i \\ 5.4 - 9.35i & 568.96 & -20.11 - 34.83i \\ 5.4 + 9.35i & -20.11 + 34.83i & 568.96 \end{pmatrix} \cdot \text{nF}$$

Note that the original C012 was:

$$C_{012} = \begin{pmatrix} 310.93 & 5.84 + 10.12i & 5.84 - 10.12i \\ 5.84 - 10.12i & 568.93 & -20.1 - 34.81i \\ 5.84 + 10.12i & -20.1 + 34.81i & 568.93 \end{pmatrix} \cdot \text{nF}$$

All of the change is basically in the zero sequence component.

Second Ground Wire Case: 1F copperweld

$$P_{gw2} := \frac{1}{2\pi \cdot \epsilon_0} \cdot \begin{pmatrix} \ln\left(\frac{H_{aai}}{r}\right) & \ln\left(\frac{H_{abi}}{D_{ab}}\right) & \ln\left(\frac{H_{aci}}{D_{ac}}\right) & \ln\left(\frac{H_{agwi}}{D_{agw}}\right) \\ \ln\left(\frac{H_{abi}}{D_{ab}}\right) & \ln\left(\frac{H_{bbi}}{r}\right) & \ln\left(\frac{H_{bci}}{D_{bc}}\right) & \ln\left(\frac{H_{bgwi}}{D_{bgw}}\right) \\ \ln\left(\frac{H_{aci}}{D_{ac}}\right) & \ln\left(\frac{H_{bci}}{D_{bc}}\right) & \ln\left(\frac{H_{cci}}{r}\right) & \ln\left(\frac{H_{cgwi}}{D_{cgw}}\right) \\ \ln\left(\frac{H_{agwi}}{D_{agw}}\right) & \ln\left(\frac{H_{bgwi}}{D_{bgw}}\right) & \ln\left(\frac{H_{cgwi}}{D_{cgw}}\right) & \ln\left(\frac{H_{gwgwi}}{\frac{\text{diag}_{gw1F}}{2}}\right) \end{pmatrix}$$

$$P_{gw2} = \begin{pmatrix} 0.14 & 0.04 & 0.02 & 0.03 \\ 0.04 & 0.14 & 0.04 & 0.03 \\ 0.02 & 0.04 & 0.14 & 0.03 \\ 0.03 & 0.03 & 0.03 & 0.16 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

Matrix Reduction (note this is done to the P matrix:

$$P_{agw2} := \text{submatrix}(P_{gw2}, 0, 2, 0, 2) \quad P_{agw2} = \begin{pmatrix} 0.14 & 0.04 & 0.02 \\ 0.04 & 0.14 & 0.04 \\ 0.02 & 0.04 & 0.14 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Pbgw2} := \text{submatrix}(\text{Pgw2}, 0, 2, 3, 3) \quad \text{Pbgw2} = \begin{pmatrix} 0.03 \\ 0.03 \\ 0.03 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Pcgw2} := \text{submatrix}(\text{Pgw2}, 3, 3, 0, 2) \quad \text{Pcgw2} = (0.03 \ 0.03 \ 0.03) \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Pdgw2} := \text{submatrix}(\text{Pgw2}, 3, 3, 3, 3) \quad \text{Pdgw2} = (0.16) \cdot \frac{\text{m}}{\text{pF}}$$

Reduce to equivalent 3x3 matrix

$$\text{Pequivgw2} := \text{Pagw2} - \text{Pbgw2} \cdot \text{Pdgw2}^{-1} \cdot \text{Pcgw2} \quad \text{Pequivgw2} = \begin{pmatrix} 0.14 & 0.03 & 0.02 \\ 0.03 & 0.14 & 0.03 \\ 0.02 & 0.03 & 0.14 \end{pmatrix} \cdot \frac{\text{m}}{\text{pF}}$$

$$\text{Cequivgw2} := \text{Pequivgw2}^{-1} \cdot \text{Length} \quad \text{Cequivgw2} = \begin{pmatrix} 0.49 & -0.09 & -0.04 \\ -0.09 & 0.5 & -0.09 \\ -0.04 & -0.09 & 0.49 \end{pmatrix} \cdot \mu\text{F}$$

$$\text{C012}_{\text{gw2}} := \text{A}_{012}^{-1} \cdot \text{Cequivgw2} \cdot \text{A}_{012}$$

$$\text{C012}_{\text{gw2}} = \begin{pmatrix} 336.71 & 5.41 + 9.36i & 5.41 - 9.36i \\ 5.41 - 9.36i & 568.96 & -20.11 - 34.83i \\ 5.41 + 9.36i & -20.11 + 34.83i & 568.96 \end{pmatrix} \cdot \text{nF}$$

Compare to first GW

$$\text{C012}_{\text{gw1}} = \begin{pmatrix} 337.06 & 5.4 + 9.35i & 5.4 - 9.35i \\ 5.4 - 9.35i & 568.96 & -20.11 - 34.83i \\ 5.4 + 9.35i & -20.11 + 34.83i & 568.96 \end{pmatrix} \cdot \text{nF}$$

$$\text{diff\_gw} := \text{submatrix}(\text{C012}_{\text{gw1}}, 0, 0, 0, 0) - \text{submatrix}(\text{C012}_{\text{gw2}}, 0, 0, 0, 0)$$

$$\text{diff\_gw} = (0.34) \cdot \text{nF} \quad \text{Due to different conductor size}$$