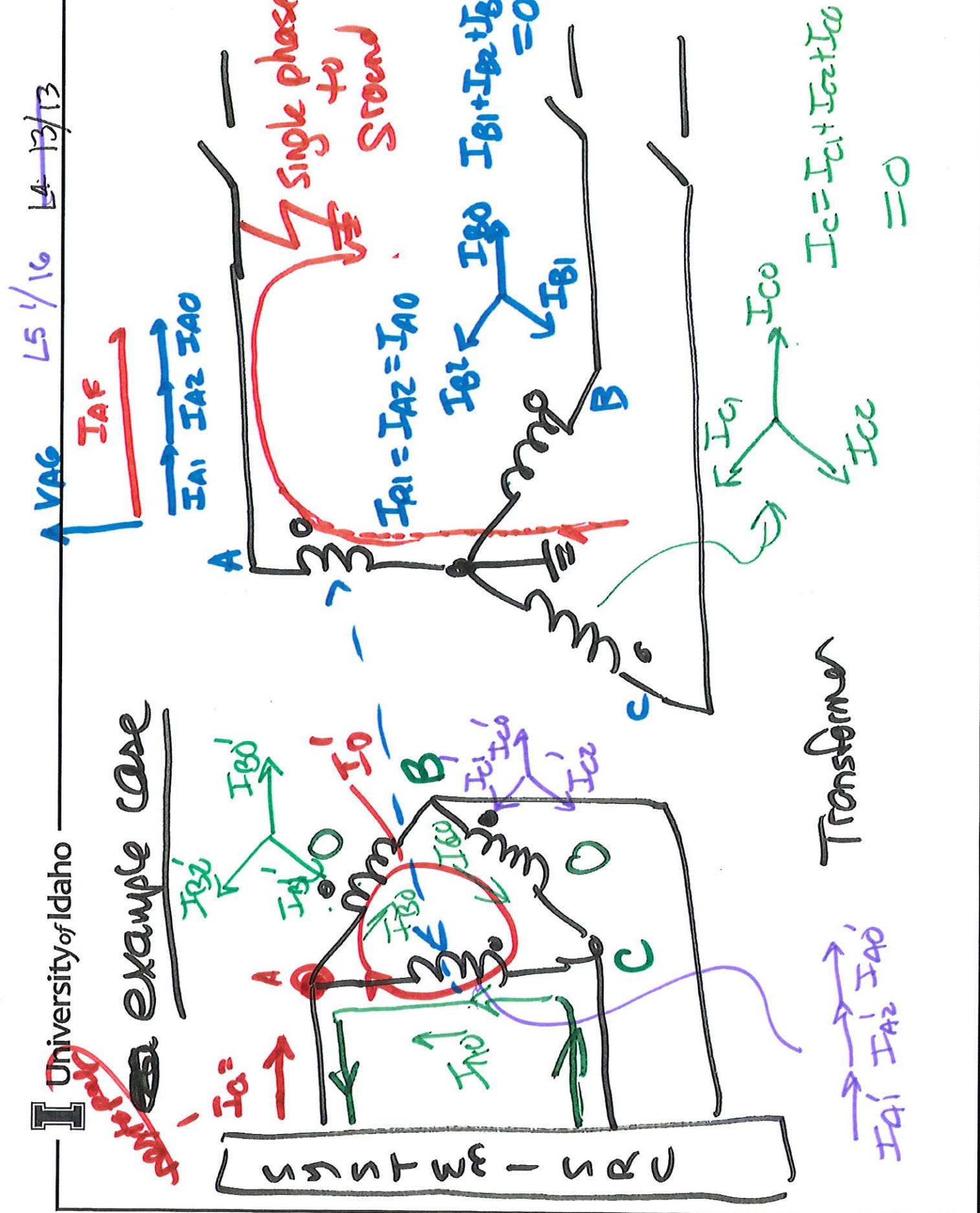


ECE 523
Symmetrical Components
Session 5



$$\bar{I}_a = I_{A0}' + I_{A1}' + I_{A2}'$$
$$I_{ca} = I_{A0}' - I_{A1}' + I_{A2}'$$

$$\bar{I}_a = I_{B1}' - I_{A1}' + I_{B2}' - I_{A2}'$$
$$+ I_{B0}' + I_{A0}'$$
$$+ I_{C0}' + I_{C1}' + I_{C2}'$$
$$= I_{A1}' - I_{C1}' + I_{A2}' - I_{C2}'$$

ECE 523: Lecture 3

- An unbalanced n-phase set of phasors can be represented by n-1 balanced n-phase sets of phasors and a zero phase set of phasors all added together by superposition.

$$V_a = V_{a1} + V_{a2} + V_{a3} \dots V_{an}$$

$$V_b = V_{b1} + V_{b2} + V_{b3} \dots V_{bn} \sim V_{b0}$$

etc.

$$V_n = V_{n1} + V_{n2} + V_{n3} \dots V_{n,n} \sim V_{n0}$$

- Define a generalized phase angle shift term "a":

$$a = e^{j \frac{2\pi}{n}}$$

Note for a three phase system: $a := e^{j \frac{2\pi}{3}}$

$$\nearrow \wedge = 3$$

$$\arg(a) = 120^\circ$$

- Now make a into a function that depends on n. Leave n as a variable we can define. For now set a value

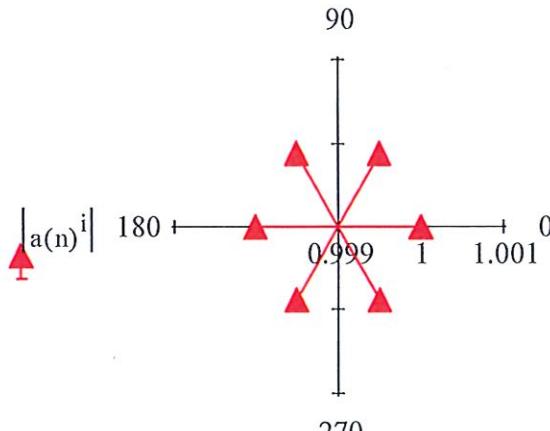
$$n := 6$$

$$a(n) := 1e^{j \frac{2\pi}{n}}$$

We can also define an array index, and have terms that vary as this increments.

$$i := 0, 1 \dots (n - 1)$$

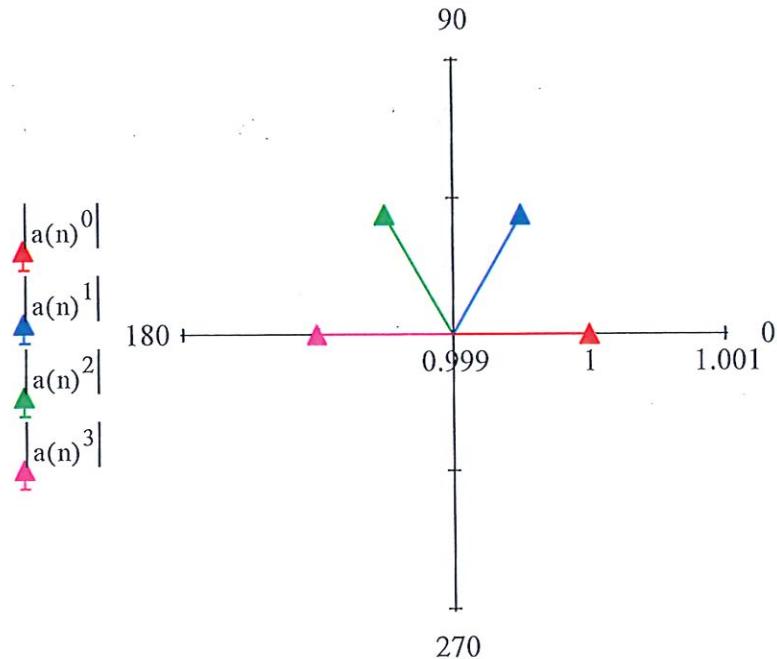
- Polar plot, with magnitude and angle as "i" increments
- Set line type to "stem" in the properties
- Note that we can't tell which way it rotates as "i" increments



$$\arg(a(n)^i)$$

4/16
L5

This time we will actually
show the powers of "a"



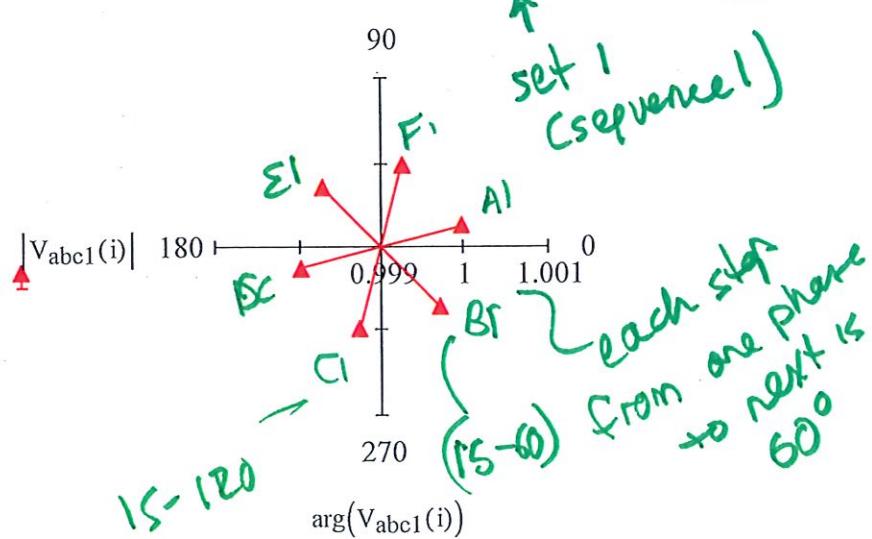
$$\arg(a(n)^0), \arg(a(n)^1), \arg(a(n)^2), \arg(a(n)^3)$$

- Now look at the balanced n-phase sets:

- Define an initial magnitude and angle reference:
- Phase relationship for phase sequence 1:

$$V_{1\text{ref}} := 1.0e^{j \cdot 15\text{deg}}$$

$$V_{abc1(i)} := a(n)^{n-i} \cdot V_{1\text{ref}}$$



- Phase relationship for phase sequence 2:

$$V_{2\text{ref}} := 1.1e^{j \cdot 5\text{deg}}$$

$$V_{abc2}(i) := a(n)^{2(n-i)} \cdot V_{2\text{ref}}$$

- Relationship for phase sequence "n"

$$V_{n\text{ref}} := 0.5e^{j \cdot 45\text{deg}}$$

$$V_{abcn}(i) := a(n)^{n(n-i)} \cdot V_{n\text{ref}}$$

- Try entering different values of n

Sums of columns

- First the zero column:

$$\text{Col_0} := \sum_{i=1}^n V_{abcn}(i) \quad |\text{Col_0}| = 3 \quad \arg(\text{Col_0}) = 45 \cdot \text{deg}$$

$$\frac{|\text{Col_0}|}{n} = 0.5$$

$$\left(\frac{|\text{Col_0}|}{n} \right) - |V_{n\text{ref}}| = 0$$

- Now the "1" column (multiply terms by a^i):

$$\text{Col_1} := \sum_{i=1}^n \left(a(n)^i \cdot V_{abc1}(i) \right) \quad |\text{Col_1}| = 6 \quad \arg(\text{Col_1}) = 15 \cdot \text{deg}$$

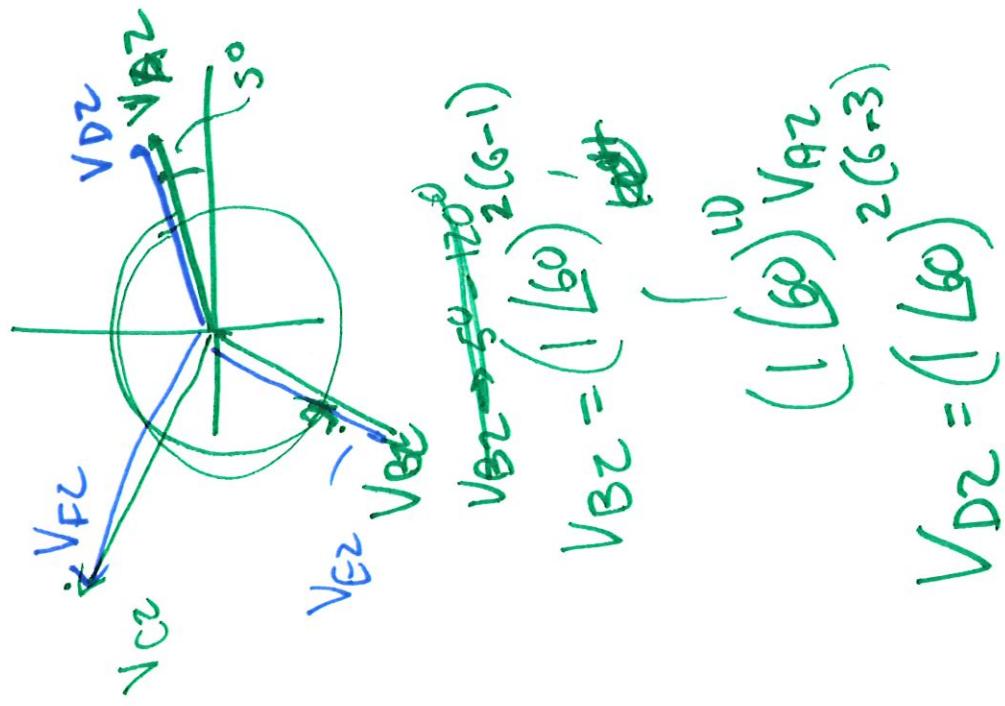
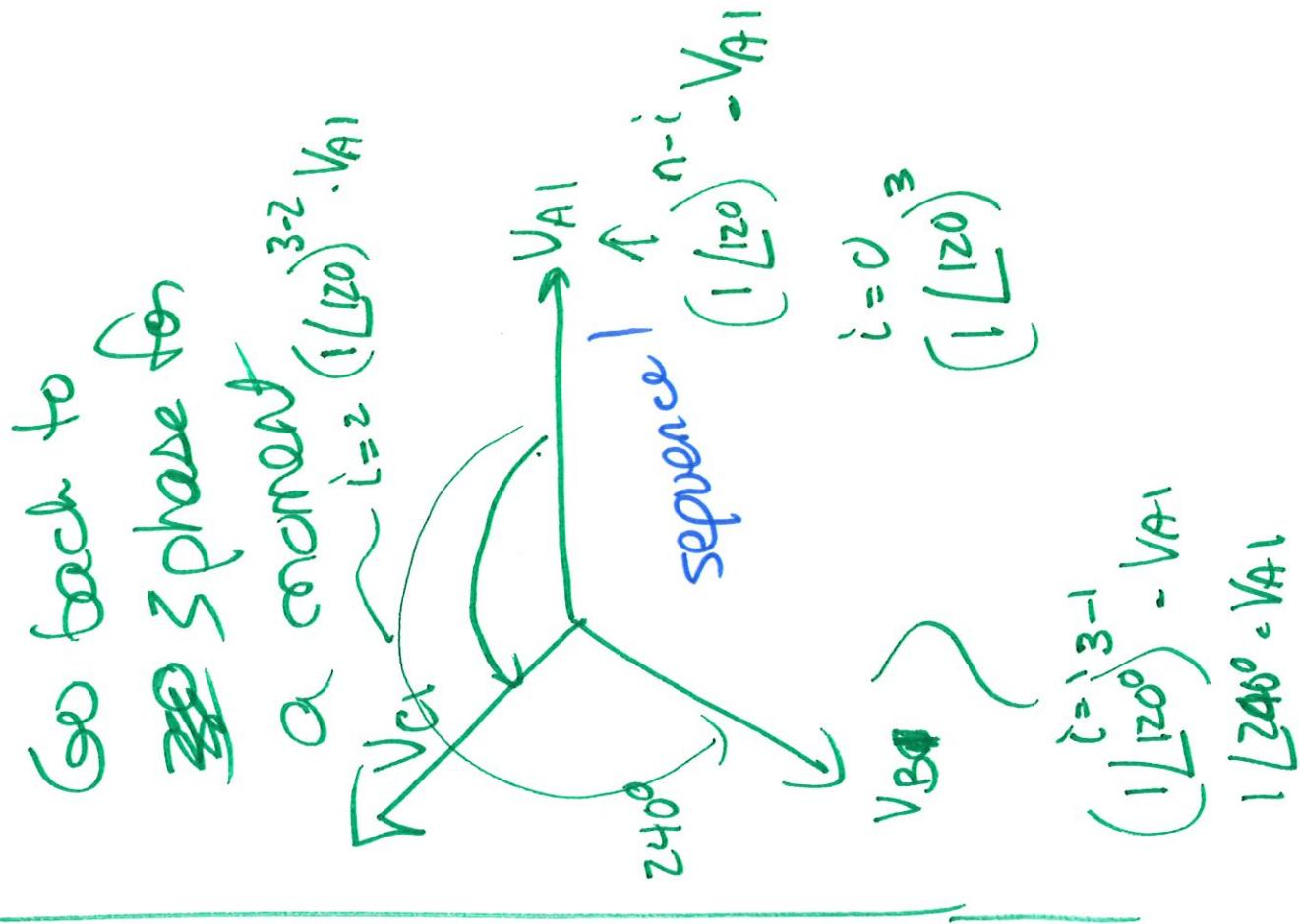
$$\frac{|\text{Col_1}|}{n} = 1$$

Repeat same multiplier on column 2 and column 0

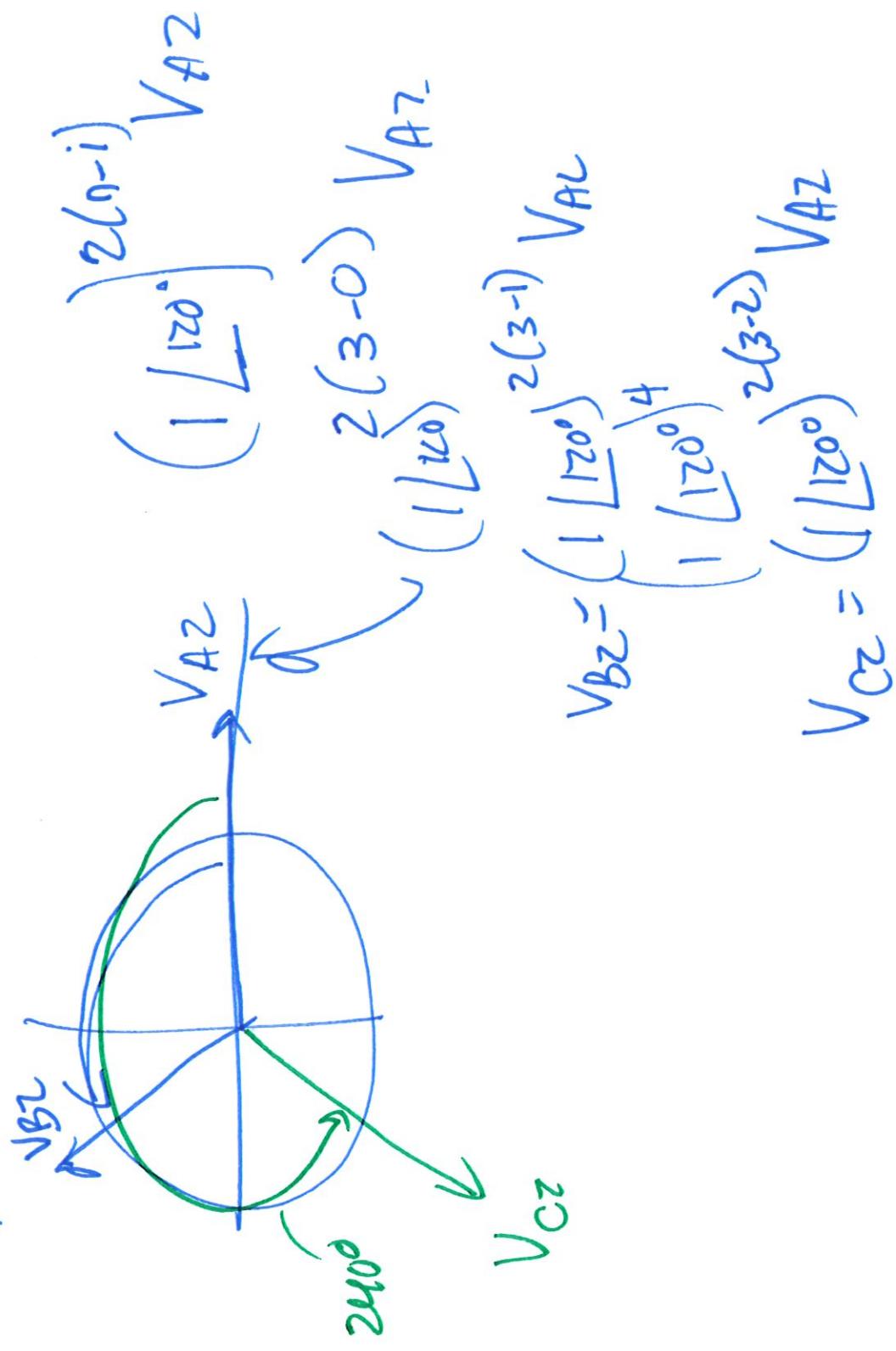
$$\text{Col_21} := \sum_{i=1}^n \left(a(n)^i \cdot V_{abc2}(i) \right) \quad |\text{Col_21}| = 0$$

sequence I had a 1 here

each rotation front are phase to next is 120° (2. 60°)



Sequence Z in 3Ø Det



$$\text{Col_01} := \sum_{i=1}^n \left(a(n)^i \cdot V_{abcn}(i) \right) \quad |\text{Col_01}| = 0$$

- Now the "2" column (multiply terms by a^{2i}):

$$\begin{aligned} \text{Col_2} := \sum_{i=1}^n & \left(a(n)^{2 \cdot i} \cdot V_{abc2}(i) \right) \quad |\text{Col_2}| = 6.6 \quad \arg(\text{Col_2}) = 5 \cdot \deg \\ & \left(\frac{|\text{Col_2}|}{n} \right) - |V_{2\text{ref}}| = 0 \end{aligned}$$

Repeat same multiplier on column 1 and column 0

$$\text{Col_12} := \sum_{i=1}^n \left(a(n)^{2 \cdot i} \cdot V_{abc1}(i) \right) \quad |\text{Col_12}| = 0$$

$$\text{Col_02} := \sum_{i=1}^n \left(a(n)^{2 \cdot i} \cdot V_{abcn}(i) \right) \quad |\text{Col_02}| = 0$$

Matrix relation (for n = 6)

$$C_{012345} := \frac{1}{6} \cdot \begin{pmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a(6) & a(6)^2 & a(6)^3 & a(6)^4 & a(6)^5 \\ 1 & a(6)^2 & a(6)^4 & a(6)^6 & a(6)^8 & a(6)^{10} \\ 1 & a(6)^3 & a(6)^6 & a(6)^9 & a(6)^{12} & a(6)^{15} \\ 1 & a(6)^4 & a(6)^8 & a(6)^{12} & a(6)^{16} & a(6)^{20} \\ 1 & a(6)^5 & a(6)^{10} & a(6)^{15} & a(6)^{20} & a(6)^{25} \end{pmatrix}$$

inverse transform

from ABCD... to 0,1,2,3,4,5

6/6
L5

$$6C_{012345} = \begin{pmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 0.5 + 0.87i & -0.5 + 0.87i & -1 & -0.5 - 0.87i & 0.5 - 0.87i \\ 1 & -0.5 + 0.87i & -0.5 - 0.87i & 1 & -0.5 + 0.87i & -0.5 - 0.87i \\ 1 & -1 & 1 & -1 & 1 & -1 \\ 1 & -0.5 - 0.87i & -0.5 + 0.87i & 1 & -0.5 - 0.87i & -0.5 + 0.87i \\ 1 & 0.5 - 0.87i & -0.5 - 0.87i & -1 & -0.5 + 0.87i & 0.5 + 0.87i \end{pmatrix}$$

$$C_{012345}^{-1} = \begin{pmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & 0.5 - 0.87i & -0.5 - 0.87i & -1 & -0.5 + 0.87i & 0.5 + 0.87i \\ 1 & -0.5 - 0.87i & -0.5 + 0.87i & 1 & -0.5 - 0.87i & -0.5 + 0.87i \\ 1 & -1 & 1 & -1 & 1 & -1 \\ 1 & -0.5 + 0.87i & -0.5 - 0.87i & 1 & -0.5 + 0.87i & -0.5 - 0.87i \\ 1 & 0.5 + 0.87i & -0.5 + 0.87i & -1 & -0.5 - 0.87i & 0.5 - 0.87i \end{pmatrix}$$

Note that: $a(6) = 0.5 + 0.87i$ $a(6)^4 = -0.5 - 0.87i$

$$a(6)^2 = -0.5 + 0.87i$$
 $a(6)^5 = 0.5 - 0.87i$

$$a(6)^3 = -1$$
 $a(6)^6 = 1$

and so on.....

- Compare matrix inverse with 6 times the complex conjugate (element by element)

$$C_{012345}^{-1} - 6 \cdot \overline{C_{012345}} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

complex conjugate

- Set tolerance value.....

Result Format

Number Format Display Options Unit Display Tolerance

Complex threshold (10)

10

Zero threshold (15)

10

Replace the $1/n$ term with $\text{SQRT}(n)/n = 1/\text{SQRT}(n)$ to give a power invariant transform:

$$C_{\text{alt}} := \frac{1}{\sqrt{6}} \cdot \begin{pmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a(6) & a(6)^2 & a(6)^3 & a(6)^4 & a(6)^5 \\ 1 & a(6)^2 & a(6)^4 & a(6)^6 & a(6)^8 & a(6)^{10} \\ 1 & a(6)^3 & a(6)^6 & a(6)^9 & a(6)^{12} & a(6)^{15} \\ 1 & a(6)^4 & a(6)^8 & a(6)^{12} & a(6)^{16} & a(6)^{20} \\ 1 & a(6)^5 & a(6)^{10} & a(6)^{15} & a(6)^{20} & a(6)^{25} \end{pmatrix}$$

$$C_{\text{alt}}^{-1} - \overline{C_{\text{alt}}} = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 \end{pmatrix}$$

Finally, we can derive the reverse transformation:

We know that: $V_{b1} = a^{-1} \cdot V_{a1}$ This time we are trying to shift V_{a1} to V_{b1}

Note that:

$$a^n = 1 \quad \text{and} \quad a^n \cdot a^{-1} = a^{n-1} \quad \text{Effectively added 360 degrees}$$

$$\text{Therefore: } a^{-1} = a^{n-1}$$

- This repeats for integer multiples of n

Check with actual values:

$$a(n)^{-1} - a(n)^{n-1} = 0 \quad a(n)^{-2} - a(n)^{n-2} = 0$$

11/16

L5

"1" term:

$$V_{b1} = a^{n-1} \cdot V_{a1}$$

$$V_{c1} = a^{n-2} \cdot V_{a1}$$

$$V_{d1} = a^{n-3} \cdot V_{a1}$$

etc.

"2" term:

$$V_{b2} = a^{n-2} \cdot V_{a2}$$

$$V_{c2} = a^{n-4} \cdot V_{a2}$$

$$V_{d2} = a^{n-6} \cdot V_{a2}$$

etc.

"n-1" term:

$$V_{b_{nm1}} = a \cdot V_{a_{nm1}}$$

$$V_{c_{nm1}} = a^2 \cdot V_{a_{nm1}}$$

$$V_{d_{nm1}} = a^3 \cdot V_{a_{nm1}}$$

etc.

$$n := 6$$

$$A_{012345} = \begin{bmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a^{-1} & a^{-2} & a^{-3} & a^{-4} & a^{-(n-1)} \\ 1 & a^{-2} & a^{-4} & a^{-6} & a^{-8} & a^{-2(n-1)} \\ 1 & a^{-3} & a^{-6} & a^{-9} & a^{-12} & a^{-3(n-1)} \\ 1 & a^{-4} & a^{-8} & a^{-12} & a^{-16} & a^{-4(n-1)} \\ 1 & a^{-(n-1)} & a^{-2(n-1)} & a^{-3(n-1)} & a^{-4(n-1)} & a^{-5(n-1)} \end{bmatrix}$$

This what we call Symmetric components transfer for a 30 Det

- Lets rewrite this a bit, realizing that $n=6$

$$A_{012345} = \begin{pmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a^{n-1} & a^{n-2} & a^{n-3} & a^{n-4} & a^{n-5} \\ 1 & a^{n-2} & a^{n-4} & a^{2n-6} & a^{2n-8} & a^{2n-10} \\ 1 & a^{n-3} & a^{2n-6} & a^{2n-9} & a^{2n-12} & a^{3n-15} \\ 1 & a^{n-4} & a^{2n-8} & a^{2n-12} & a^{3n-16} & a^{4n-20} \\ 1 & a^{n-5} & a^{2n-10} & a^{3n-15} & a^{4n-20} & a^{4n-25} \end{pmatrix} = \begin{pmatrix} 1 & 1 & 1 & 1 & 1 & 1 \\ 1 & a^5 & a^4 & a^3 & a^2 & a \\ 1 & a^4 & a^2 & a^0 & a^4 & a^2 \\ 1 & a^3 & a^0 & a^3 & a^0 & a^3 \\ 1 & a^2 & a^4 & a^0 & a^2 & a^4 \\ 1 & a & a^2 & a^3 & a^4 & a^5 \end{pmatrix}$$

$$a^6 \quad a^6 = 0^0$$

$$\text{30 set } n=1$$

$$\begin{bmatrix} a^3 & a^3 & a^3 \\ a^3 & a^2 & a^1 \\ 0^3 & a^1 & a^0 \end{bmatrix}_{3-2} = a^3 \begin{bmatrix} 1 & 1 & 1 \\ 1 & a^2 & a^2 \\ 1 & a & a^2 \end{bmatrix}$$

$$\begin{bmatrix} V_{A0} \\ V_{A1} \\ V_{A2} \end{bmatrix} = \begin{pmatrix} -1 & \sqrt{AG} \\ 0 & V_{BG} \\ 0 & V_{CG} \end{pmatrix} \begin{bmatrix} V_{A0} \\ V_{A1} \\ V_{A2} \end{bmatrix}$$

Normal, positive sequence
operator

$$\begin{bmatrix} V_0 \\ V_A \\ V_B \\ V_C \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha & \alpha^2 \\ 1 & \alpha^2 & \alpha \end{bmatrix} \begin{bmatrix} V_0 \\ V_A \\ V_B \\ V_C \end{bmatrix} = \frac{\left(\frac{V_0}{3}\right)}{\left(\frac{V_A}{3}\right)} = \frac{\left(\frac{V_0}{3}\right)}{\left(\frac{V_B}{3}\right)} = \frac{\left(\frac{V_0}{3}\right)}{\left(\frac{V_C}{3}\right)}$$

$$\begin{aligned} V_A &= \frac{1}{3} V_0 \\ V_B &= \frac{1}{3} (-120) \\ V_C &= \frac{1}{3} (+120) \\ V_A &= \frac{1}{3} \left(\frac{V_0}{\alpha^2} \right) \end{aligned}$$

$$3\phi \text{ per } A_{012} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha^4 \\ 1 & \alpha^4 & \alpha^2 \end{bmatrix}$$

$\alpha^6 = 1$

$$\begin{bmatrix} V_{A0} \\ V_{B0} \\ V_{C0} \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \alpha^2 & \alpha^4 \\ 1 & \alpha^4 & \alpha^2 \end{bmatrix} \begin{bmatrix} V_{A1} \\ V_{B1} \\ V_{C1} \end{bmatrix}$$

Phase A Sequence Components

ABC line to ground voltages

Phase A, B and C Reference: Transformations and Inverse Transformations

$$a := 1 \cdot e^{j \cdot 120^\circ}$$

Phase A symmetrical components transform

$$A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix}$$

Phase B symmetrical components transform

$$B_{012} := \begin{pmatrix} 1 & a & a^2 \\ 1 & 1 & 1 \\ 1 & a^2 & a \end{pmatrix}$$

Phase C symmetrical components transform

$$C_{012} := \begin{pmatrix} 1 & a^2 & a \\ 1 & a & a^2 \\ 1 & 1 & 1 \end{pmatrix}$$

From the n phase set

$$\text{Inverse } A_{012} := \frac{1}{3} \begin{pmatrix} 1 & 1 & 1 \\ 1 & a & a^2 \\ 1 & a^2 & a \end{pmatrix}$$

$$\text{Inverse } A_{012} - A_{012}^{-1} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\text{Inverse } B_{012} := \frac{1}{3} \begin{pmatrix} 1 & 1 & 1 \\ a^2 & 1 & a \\ a & 1 & a^2 \end{pmatrix}$$

$$\text{Inverse } B_{012} - B_{012}^{-1} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\text{Inverse } C_{012} := \frac{1}{3} \begin{pmatrix} 1 & 1 & 1 \\ a & a^2 & 1 \\ a^2 & a & 1 \end{pmatrix}$$

$$\text{Inverse } C_{012} - C_{012}^{-1} = \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

Symmetrical Components Transformations

European versus North American Notation

$$a := e^{j \cdot 120\text{deg}} = \text{cis } 120^\circ$$

$$h := e^{j \cdot 120\text{deg}}$$

Phase A symmetrical components transform (A)

$$A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix}$$

0 1 2

Phase R symmetrical components transform (H)

$$H_{PNZ} := \begin{pmatrix} 1 & 1 & 1 \\ h^2 & h & 1 \\ h & h^2 & 1 \end{pmatrix}$$

P N Z

$$Z_{aa} := (14.9 + j \cdot 58.4) \Omega$$

$$Z_{ab} := (4 + j \cdot 27.3) \Omega$$

$$Z_{bb} := (14.9 + j \cdot 58.4) \Omega$$

$$Z_{ac} := (4 + j \cdot 27.3) \Omega$$

$$Z_{cc} := (14.9 + j \cdot 58.4) \Omega$$

$$Z_{bc} := (4 + j \cdot 27.3) \Omega$$

$$Z_{ABC} := \begin{pmatrix} Z_{aa} & Z_{ab} & Z_{ac} \\ Z_{ab} & Z_{bb} & Z_{bc} \\ Z_{ac} & Z_{bc} & Z_{cc} \end{pmatrix}$$

$$Z_{012} := A_{012}^{-1} \cdot Z_{ABC} \cdot A_{012}$$

$$Z_{012} = \begin{pmatrix} 22.9 + 113i & 0 & 0 \\ 0 & 10.9 + 31.1i & 0 \\ 0 & 0 & 10.9 + 31.1i \end{pmatrix} \Omega$$

Z

Diagonal \Rightarrow perfect decoupling between pos, neg, & zero sequence

$$Z_{PNZ} := H_{PNZ}^{-1} \cdot Z_{ABC} \cdot H_{PNZ}$$

$$Z_{PNZ} = \begin{pmatrix} 10.9 + 31.1i & 0 & 0 \\ 0 & 10.9 + 31.1i & 0 \\ 0 & 0 & 22.9 + 113i \end{pmatrix} \Omega$$

Z

$$I_a := 100A \cdot e^{j \cdot 0\text{deg}}$$

$$I_b := 2000A \cdot e^{j \cdot 30\text{deg}}$$

$$I_c := 1900A \cdot e^{j \cdot 210\text{deg}}$$

$$I_{012} := A_{012}^{-1} \cdot \begin{pmatrix} I_a \\ I_b \\ I_c \end{pmatrix} \quad \overrightarrow{|I_{012}|} = \begin{pmatrix} 64.4 \\ 1109.23 \\ 1142.56 \end{pmatrix} \text{A} \quad \overrightarrow{\arg(I_{012})} = \begin{pmatrix} 15 \\ 119.37 \\ -59.39 \end{pmatrix} \cdot \text{deg}$$

O
P
N
Z Z

$$I_{PNZ} := H_{PNZ}^{-1} \cdot \begin{pmatrix} I_a \\ I_b \\ I_c \end{pmatrix} \quad \overrightarrow{|I_{PNZ}|} = \begin{pmatrix} 1109.23 \\ 1142.56 \\ 64.4 \end{pmatrix} \text{A} \quad \overrightarrow{\arg(I_{PNZ})} = \begin{pmatrix} 119.37 \\ -59.39 \\ 15 \end{pmatrix} \cdot \text{deg}$$

P
N
Z