

Symmetrical Components Example

$$MVA := MW \quad a := 1 \cdot e^{j \cdot 120\text{deg}}$$

$$A_{012} := \begin{pmatrix} 1 & 1 & 1 \\ 1 & a^2 & a \\ 1 & a & a^2 \end{pmatrix} \quad \text{Inv}_- A_{012} = \frac{1}{3} \begin{pmatrix} 1 & 1 & 1 \\ 1 & a & a^2 \\ 1 & a^2 & a \end{pmatrix}$$

$$S_B := 100\text{MVA} \quad V_{BLL} := 230\text{kV} \quad I_B := \frac{S_B}{\sqrt{3} \cdot V_{BLL}} \quad I_B = 251.022\text{A}$$

- Voltages and currents from a single line to ground fault with load flow on weak 230 kV system

$$Z_1 := (3.408 + j \cdot 38.956)\text{ohm} \quad Z_2 := Z_1 \quad Z_2 = (3.408 + 38.956i)\Omega$$

$$Z_0 := 3 \cdot Z_1 \quad Z_0 = (10.224 + 116.868i)\Omega$$

$$V_S := \frac{230\text{kV}}{\sqrt{3}} \cdot e^{j \cdot 0\text{deg}} \quad V_R := \frac{230\text{kV}}{\sqrt{3}} \cdot e^{-j \cdot 16\text{deg}}$$

$$I_{A_prefault} := \frac{(V_S - V_R)}{Z_1} \quad |I_{A_prefault}| = 945.198\text{A} \quad \arg(I_{A_prefault}) = -3\text{-deg}$$

- Prefault current from EMT simulation

$$\text{mag}I_A := 945.1\text{A} \quad \theta_{IA} := -3.03\text{deg}$$

- Fault currents and voltages from EMT simulation

$$I_{ABC} := \begin{pmatrix} 4144\text{A} \cdot e^{-j \cdot 79.74\text{deg}} \\ 945.1\text{A} \cdot e^{-j \cdot 122.9\text{deg}} \\ 945.1\text{A} \cdot e^{j \cdot 117.1\text{deg}} \end{pmatrix} \quad V_{ABC} := \begin{pmatrix} 10^{-5}\text{V} \cdot e^{j \cdot 0\text{deg}} \\ 164.3\text{kV} \cdot e^{-j \cdot 144.0\text{deg}} \\ 164.2\text{kV} \cdot e^{j \cdot 128.2\text{deg}} \end{pmatrix}$$

$$I_{012} := A_{012}^{-1} \cdot I_{ABC} \quad \overrightarrow{|I_{012}|} = \begin{pmatrix} 1345.057 \\ 1643.583 \\ 1345.057 \end{pmatrix} \cdot \text{A} \quad \overrightarrow{\arg(I_{012})} = \begin{pmatrix} -92.923 \\ -57.822 \\ -92.923 \end{pmatrix} \cdot \text{deg}$$

$$V_{012} := A_{012}^{-1} \cdot V_{ABC} \quad \overrightarrow{|V_{012}|} = \begin{pmatrix} 78.9 \\ 105.205 \\ 26.305 \end{pmatrix} \cdot \text{kV} \quad \overrightarrow{\arg(V_{012})} = \begin{pmatrix} 172.117 \\ -7.905 \\ 172.03 \end{pmatrix} \cdot \text{deg}$$

- Comparing our model to the simulation results

$$V_{0f} := 0 - I_{012}_0 \cdot Z_0 \quad |V_{0f}| = 157.795 \cdot \text{kV} \quad \arg(V_{0f}) = 172.077 \cdot \text{deg}$$

$$V_{1f} := \frac{230 \cdot \text{kV}}{\sqrt{3}} - I_{012}_1 \cdot (Z_1) \quad |V_{1f}| = 81.114 \cdot \text{kV} \quad \arg(V_{1f}) = -21.218 \cdot \text{deg}$$

$$V_{2f} := 0 - I_{012}_2 \cdot (Z_2) \quad |V_{2f}| = 52.598 \cdot \text{kV} \quad \arg(V_{2f}) = 172.077 \cdot \text{deg}$$

$$V_{ABCf} := A_{012} \cdot \begin{pmatrix} V_{0f} \\ V_{1f} \\ V_{2f} \end{pmatrix} \quad \overrightarrow{|V_{ABCf}|} = \begin{pmatrix} 132.77 \\ 214.366 \\ 197.876 \end{pmatrix} \cdot \text{kV} \quad \overrightarrow{\arg(V_{ABCf})} = \begin{pmatrix} -179.846 \\ -158.72 \\ 133.554 \end{pmatrix} \cdot \text{deg}$$

Now look at behavior in the time domain.

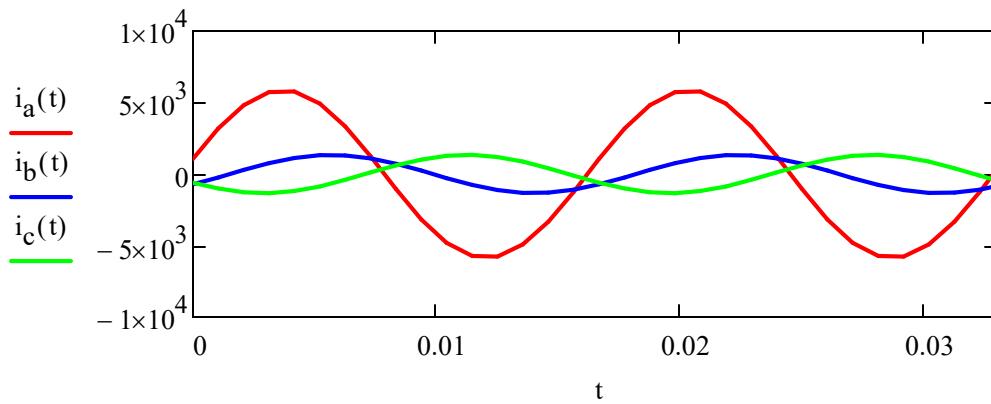
- Set up an array 2 cycles long, with 16 samples per cycle

$$t := 0 \text{ sec}, \frac{1}{16 \cdot 60 \text{ Hz}} .. \frac{2}{60 \text{ Hz}} \quad \omega := 2 \cdot \pi \cdot 60 \text{ Hz}$$

$$i_a(t) := \sqrt{2} \cdot |I_{ABC}_0| \cdot \cos(\omega \cdot t + \arg(I_{ABC}_0))$$

$$i_b(t) := \sqrt{2} \cdot |I_{ABC}_1| \cdot \cos(\omega \cdot t + \arg(I_{ABC}_1))$$

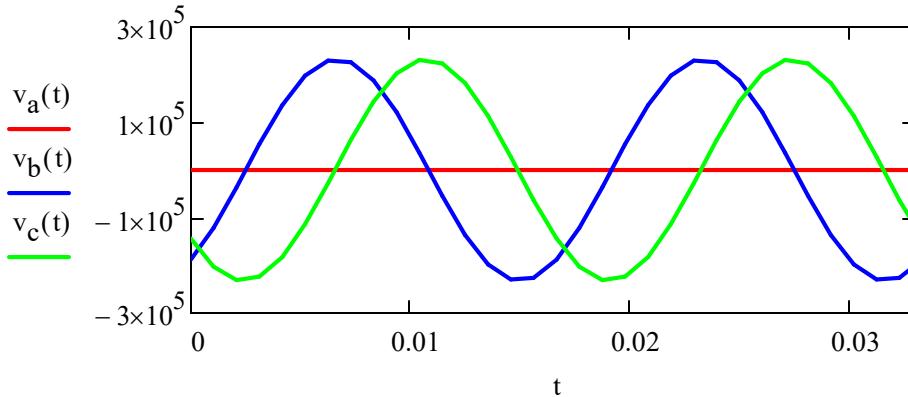
$$i_c(t) := \sqrt{2} \cdot |I_{ABC}_2| \cdot \cos(\omega \cdot t + \arg(I_{ABC}_2))$$



$$v_a(t) := \sqrt{2} \cdot |V_{ABC_0}| \cdot \cos(\omega \cdot t + \arg(V_{ABC_0}))$$

$$v_b(t) := \sqrt{2} \cdot |V_{ABC_1}| \cdot \cos(\omega \cdot t + \arg(V_{ABC_1}))$$

$$v_c(t) := \sqrt{2} \cdot |V_{ABC_2}| \cdot \cos(\omega \cdot t + \arg(V_{ABC_2}))$$



- Convert a and a^2 to units of time

$$T_a := \frac{\arg(a)}{360\text{deg} \cdot 60\text{Hz}} \quad T_a = 5.556 \cdot \text{ms}$$

$$T_{a_sq} := \frac{\arg(a^2) + 360\text{deg}}{360\text{deg} \cdot 60\text{Hz}} \quad T_{a_sq} = 11.111 \cdot \text{ms}$$

Note that: $I_1 = \frac{(I_A + a \cdot I_B + a^2 \cdot I_C)}{3}$

- This equation involves rotating I_B and I_C by positive angles, which would mean advancing in time.
- We can only delay measurements, not advance them
- Recall that:

$$a = a^{-2} \quad a - a^{-2} = 0$$

$$a^2 = a^{-1} \quad a^2 - a^{-1} = 0$$

- Instead we will use the following equations for I_1 and I_2 with time delays.

$$I_{1_alt} := \frac{(I_{ABC_0} + a^{-2} \cdot I_{ABC_1} + a^{-1} \cdot I_{ABC_2})}{3} \quad I_{1_alt} = (875.296 - 1391.122i) \text{ A}$$

$$I_{2_alt} := \frac{I_{ABC_0} + a^{-1} \cdot I_{ABC_1} + a^{-2} \cdot I_{ABC_2}}{3}$$

$$I_{2_alt} = (-68.593 - 1343.307i) A$$

As a check

$$I_{1_alt} - I_{012_1} = 0 A$$

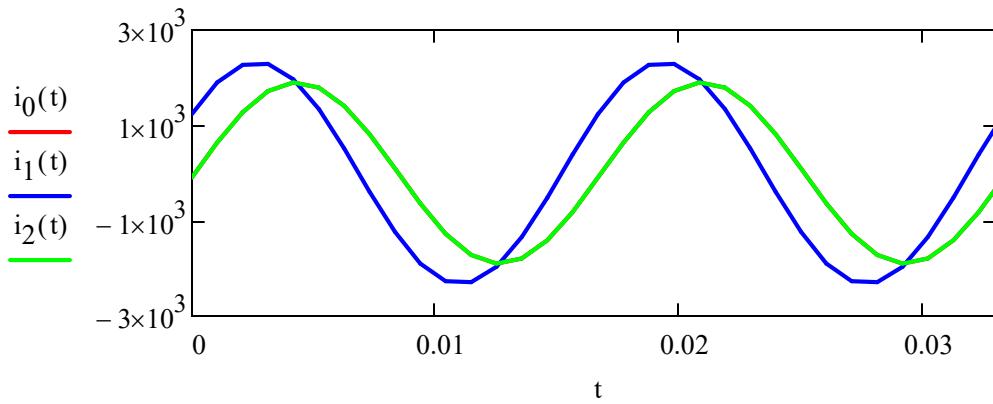
$$I_{1_alt} - I_{012_1} = 0 A$$

- Find sequence current taking angle rotations as time delays

$$i_0(t) := \frac{(i_a(t) + i_b(t) + i_c(t))}{3}$$

$$i_1(t) := \frac{(i_a(t) + i_b(t - T_{a_sq}) + i_c(t - T_a))}{3}$$

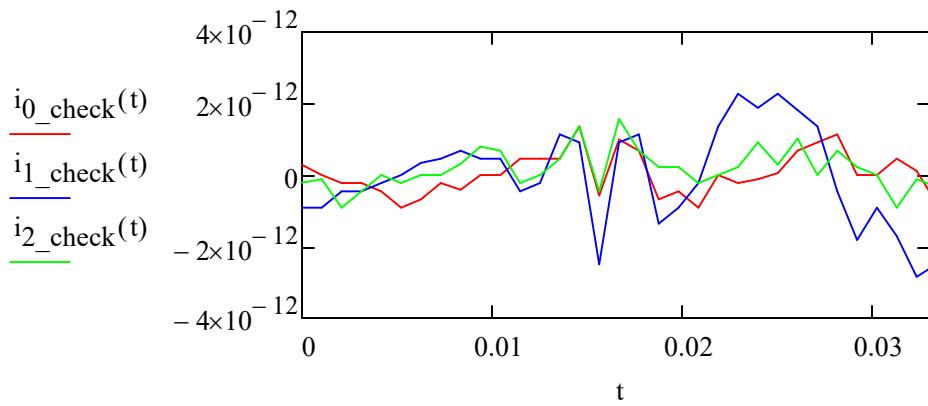
$$i_2(t) := \frac{(i_a(t) + i_b(t + T_a) + i_c(t + T_a))}{3}$$



$$i_{0_check}(t) := i_0(t) - \sqrt{2} \cdot |I_{012_0}| \cdot \cos(\omega \cdot t + \arg(I_{012_0}))$$

$$i_{1_check}(t) := i_1(t) - \sqrt{2} \cdot |I_{012_1}| \cdot \cos(\omega \cdot t + \arg(I_{012_1}))$$

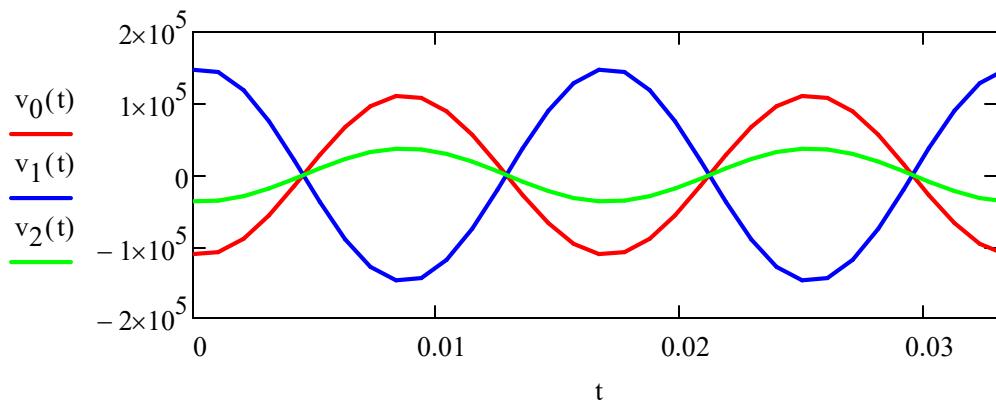
$$i_{2_check}(t) := i_2(t) - \sqrt{2} \cdot |I_{012_2}| \cdot \cos(\omega \cdot t + \arg(I_{012_2}))$$



$$v_0(t) := \frac{(v_a(t) + v_b(t) + v_c(t))}{3}$$

$$v_1(t) := \frac{(v_a(t) + v_b(t + T_a) + v_c(t + T_{a_sq}))}{3}$$

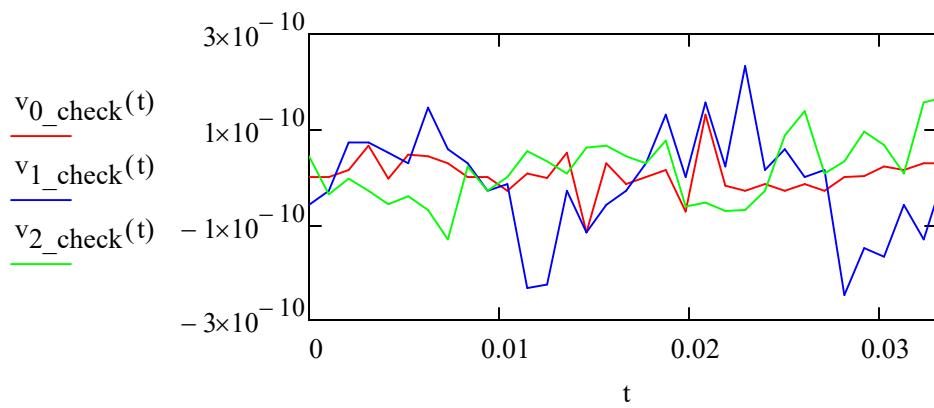
$$v_2(t) := \frac{(v_a(t) + v_b(t + T_{a_sq}) + v_c(t + T_a))}{3}$$



$$v_{0_check}(t) := v_0(t) - \sqrt{2} \cdot |V_{012_0}| \cdot \cos(\omega \cdot t + \arg(V_{012_0}))$$

$$v_{1_check}(t) := v_1(t) - \sqrt{2} \cdot |V_{012_1}| \cdot \cos(\omega \cdot t + \arg(V_{012_1}))$$

$$v_{2_check}(t) := v_2(t) - \sqrt{2} \cdot |V_{012_2}| \cdot \cos(\omega \cdot t + \arg(V_{012_2}))$$



- Implemented same scheme in ATP.

$$I_0 := 1345A \cdot e^{-j \cdot 93.02 \deg}$$

$$I_1 := 1644A \cdot e^{-j \cdot 57.94 \deg}$$

$$I_2 := 1345A \cdot e^{-j \cdot 93 \deg}$$

- Above we calculated

$$\overrightarrow{|I_{012}|} = \begin{pmatrix} 1345.057 \\ 1643.583 \\ 1345.057 \end{pmatrix} A$$

$$\overrightarrow{\arg(I_{012})} = \begin{pmatrix} -92.923 \\ -57.822 \\ -92.923 \end{pmatrix} \cdot \deg$$