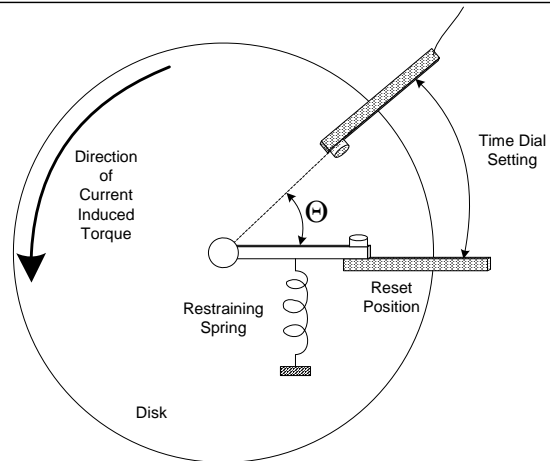


# UI Time Overcurrent Relays

ECE525

Lecture 11

- More or less approximates thermal fuse
  - » Allow coordination with fuses



Time Overcurrent Relays

Fall 2018

# UI Basic equation

ECE525

Lecture 11

Operating torque      Restraining Torque

$$T = \tau_s \left( \left( \frac{I}{I_p} \right)^2 - 1 \right) - K_d \left( \frac{\partial \theta}{\partial t} \right)$$

- $\tau_s$  = restraining spring torque
- $I$  = applied current
- $I_p$  = pick up current
- $K_d$  = disk damping factor
- $\theta$  = angle of disk rotation (proportional to Time Dial Setting (TDS))

Time Overcurrent Relays

Fall 2018

1. Operating torque = Restraining Torque

2. Integrate w.r.t. Time

$$\tau_s \left( \left( \frac{I}{I_p} \right)^2 - 1 \right) = K_d \left( \frac{\partial \theta}{\partial t} \right)$$

$$\theta_2 - \theta_1 = \frac{\tau_s}{K_d} \left( \left( \frac{I}{I_p} \right)^2 - 1 \right) (t_2 - t_1)$$

3. TDS (setting angle),  
where triptime =  $t_2 - t_1$ 

$$TDS = \frac{\tau_s}{K_d} \left( \left( \frac{I}{I_p} \right)^2 - 1 \right) (\text{trip time})$$

4. Finding trip time

$$(\text{trip time}) = TDS \frac{\frac{K_d}{\tau_s}}{\left( \left( \frac{I}{I_p} \right)^2 - 1 \right)} = TDS \frac{A}{(M^2 - 1)}$$

Where:  $M = I/I_p$ 

$$A = K_d/t_s$$

# U I

## Standard Curves -- standard formats

ECE525

Lecture 11

Reset Time ( $M < 1$ )

$$tr = TDS \left( \frac{C}{1 - M^2} \right)$$

Trip time ( $M \geq 1$ )

$$tt = TDS \left( \frac{A}{M^P - 1} + B \right)$$

Some manufacturers include disk inertia in B

Time Overcurrent Relays

Fall 2018

# U I

## US and IEC curve parameters

ECE525

Lecture 11

Curve	A	B	C	P
U.S. Moderately inverse (U1)	0.0104	0.2256	1.08	0.02
U.S. Inverse (U2)	5.95	0.180	5.95	2.00
U.S. Very inverse (U3)	3.88	0.0963	3.88	2.00
U.S. Extremely inverse (U4)	5.67	0.352	5.67	2.00
U.S. Short-time inverse (U5)	0.00342	0.00262	0.323	0.02
I.E.C. Class A - Standard inverse (C1)	0.14	0.0	13.5	0.02
I.E.C. Class B - Very inverse (C2)	13.5	0.0	47.3	2.00
I.E.C. Class C - Extremely inverse (C3)	80.0	0.0	80.0	2.00
I.E.C. Long-time inverse (C4)	120.0	0.0	120.0	2.00
I.E.C. Short-time inverse (C5)	0.05	0.0	4.85	0.04

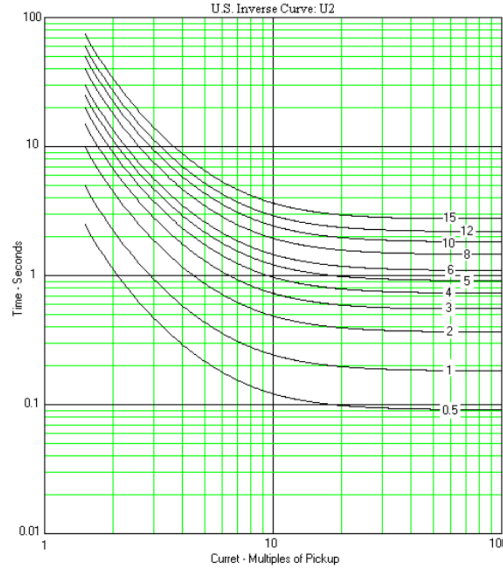
Time Overcurrent Relays

Fall 2018

***U***  
***I***

# US Inverse (U2) Characteristic

*ECE525*  
*Lecture 11*



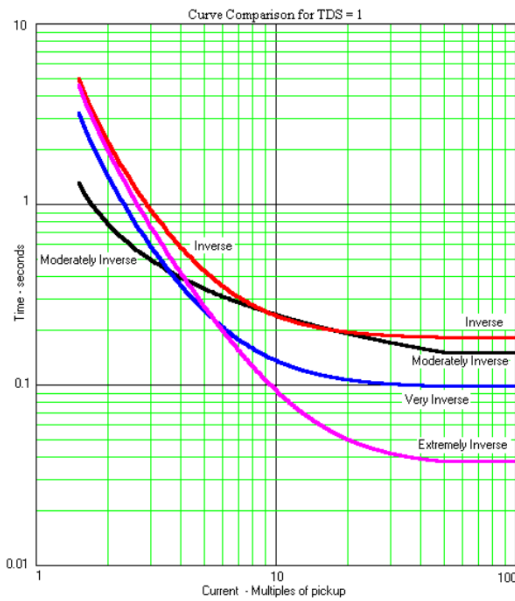
*Time Overcurrent R:*

Fall 2018

***U***  
***I***

# Comparison of curves

*ECE525*  
*Lecture 11*



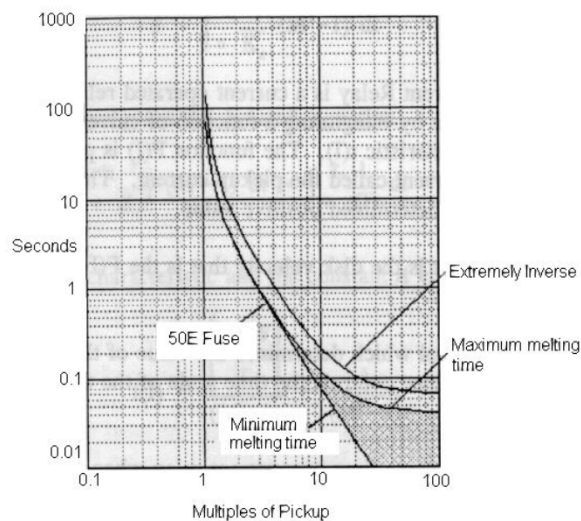
*Time Overcurre*

Fall 2018

# U I Extremely Inverse Curve and 50E fuse

ECE525

Lecture 11



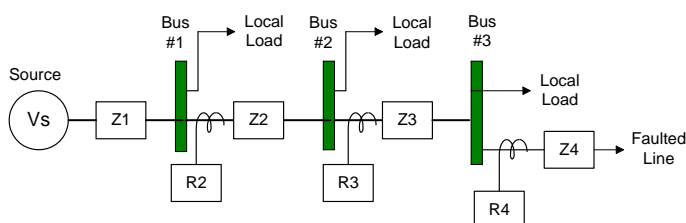
Time Overcurrent Relays

Fall 2018

# U I Example

ECE525

Lecture 11



- Want the relay on the faulted line, R4, to be the only relay to trip
- Max and min fault current (based on ends of faulted line)

$$I_{f3phmax} = \frac{V_s}{Z_1 + Z_2 + Z_3} \quad I_{f3phmin} = \frac{V_s}{Z_1 + Z_2 + Z_3 + Z_4}$$

Time Overcurrent Relays

Fall 2018

**U  
I**

## Example continued

*ECE525*

*Lecture 11*

- The desired coordination can be accomplished by:  
increasing the time dial settings as one proceeds toward  
the source.
  
- » If relay R2 is expected to provide backup protection for  
relay R4,
  - » Then R4, the relay with the greatest source impedance, would  
be set with the lowest time dial setting

*Time Overcurrent Relays*

Fall 2018

**U  
I**

## Example continued

*ECE525*

*Lecture 11*

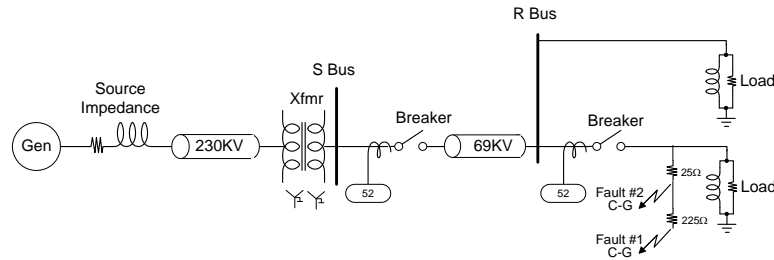
- » If  $I_{MIN}$  is defined as the minimum fault current,
  - » Then the pickup current must be set at or below this current but  
above maximum load current.
  - » Usually with a margin around both
  
- » For relays R2 and R3, the TDS must be set to trip no  
faster than the next downstream device when the fault  
current is maximum for an out of zone fault

*Time Overcurrent Relays*

Fall 2018

# UI EMTP relay simulation

ECE525  
Lecture 11



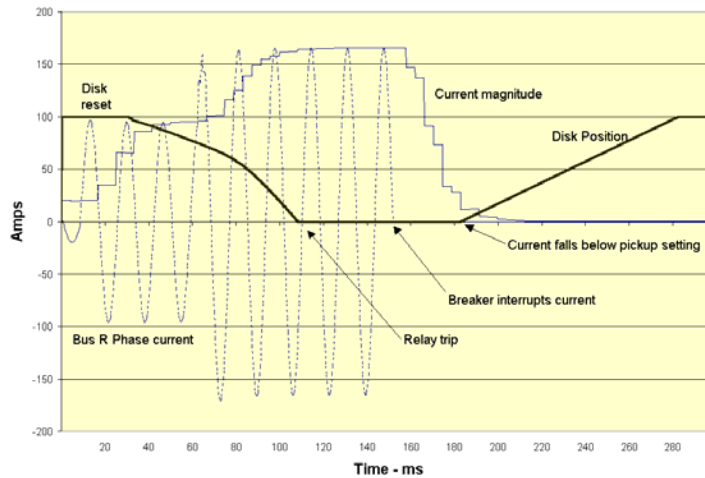
250Ω resistive fault is initiated at 8.3 ms and progresses to a 25Ω fault at 62 ms as can occur by a tree branch coming in contact with the wire.

Time Overcurrent Relays

Fall 2018

# UI Example with a trip

ECE525  
Lecture 11



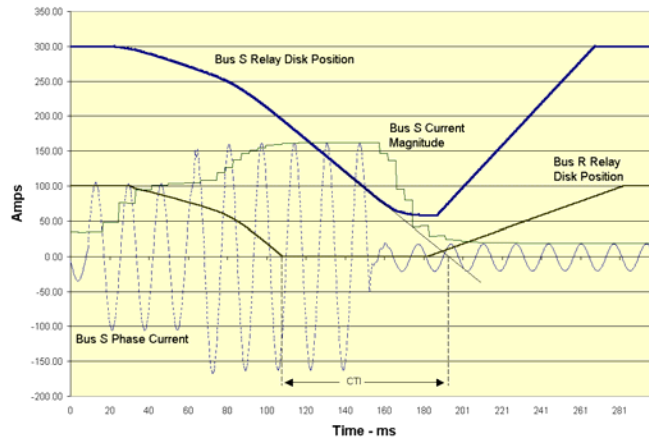
Time Overcurrent Relays

Fall 2018

**U  
I**

# Comparing relay coordination (light load)

ECE525  
Lecture 11



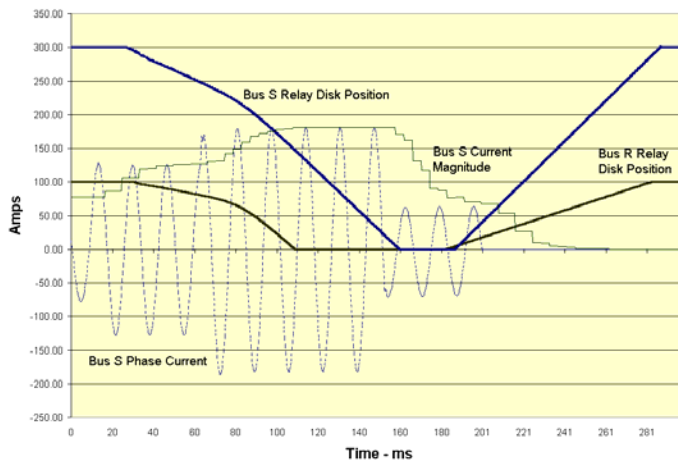
Time Overcurrent Relays

Fall 2018

**U  
I**

# Comparing relay coordination (heavy load)

ECE525  
Lecture 11



Time Overcurrent Relays

Fall 2018

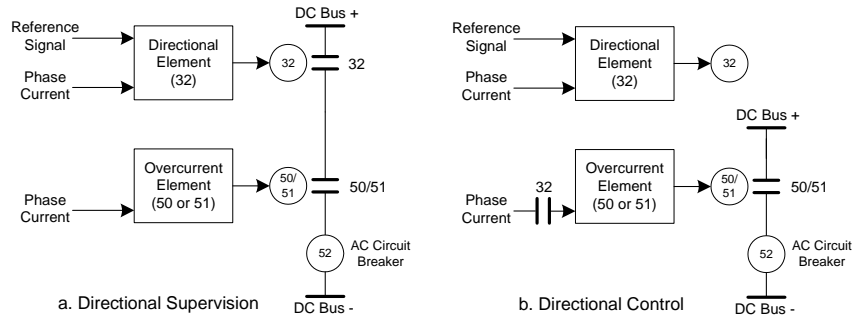


# U I

## Directional Control vs Direction Supervision

ECE525

Lecture 11



Time Overcurrent Relays

Fall 2018

# U I

## Directional Step-Time Overcurrent (ANSI 67)

ECE525

Lecture 11

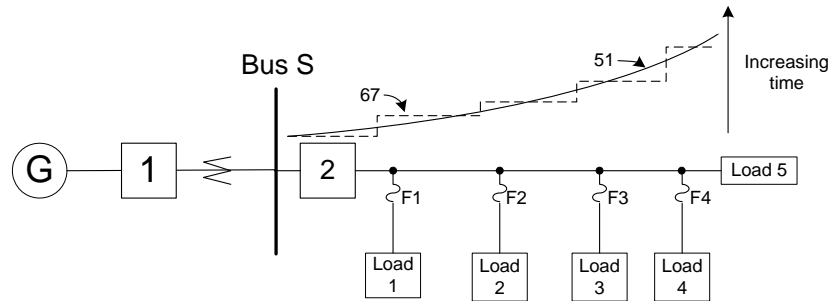
- The directional overcurrent relay can be perceived as a type 50 instantaneous element controlled by a type 32 directional element
- If the type 67 relay element is to provide backup protection, they use definite time delay for downstream coordination
- The 67 element requires more attention to detail for coordination than do type 51 relays
  - » The advantage that the stepped time has over the 51 is that the time steps are independently set.
  - » The disadvantage is that overreach errors have a more pronounced affect that often proves difficult to coordinate

Time Overcurrent Relays

Fall 2018

# UI Directional Step-Time Overcurrent (ANSI 67)

ECE525  
Lecture 11



Time Overcurrent Relays

Fall 2018

# UI Overcurrent Elements in Microprocessor Relays

ECE525  
Lecture 11

- Expect the relay to be able to coordinate with fuses and electromechanical relays
- Implement relay function using the standard curve equations
- Use digital filters to compute RMS magnitude from measured currents
- Add directional supervision
- Take advantage of some calculations difficult to do without microprocessor

Time Overcurrent Relays

Fall 2018