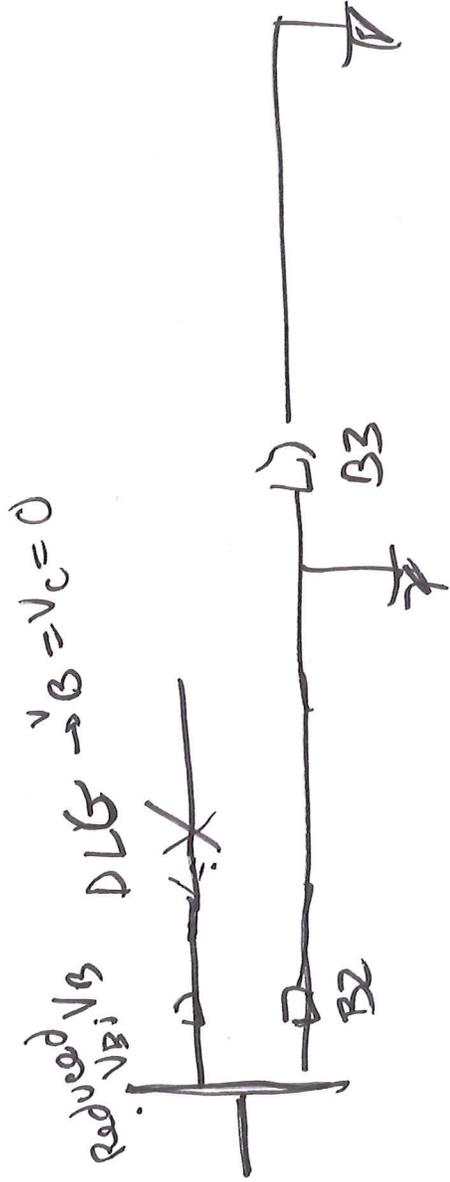


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ECE 525

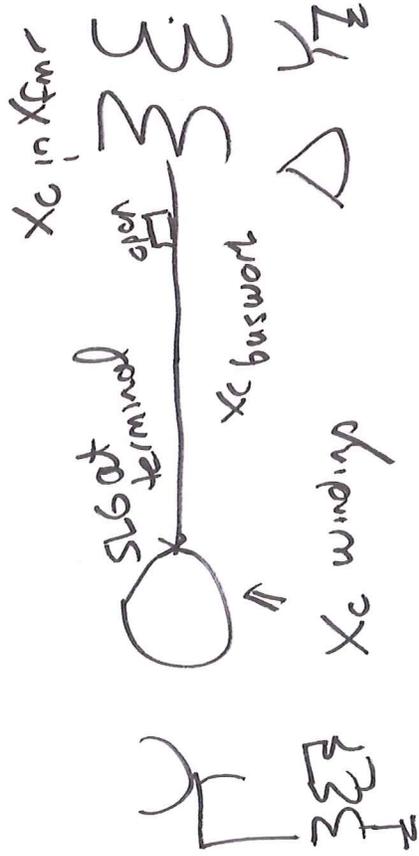
POWER SYSTEM PROTECTION
AND RELAYING

SESSION no. 22



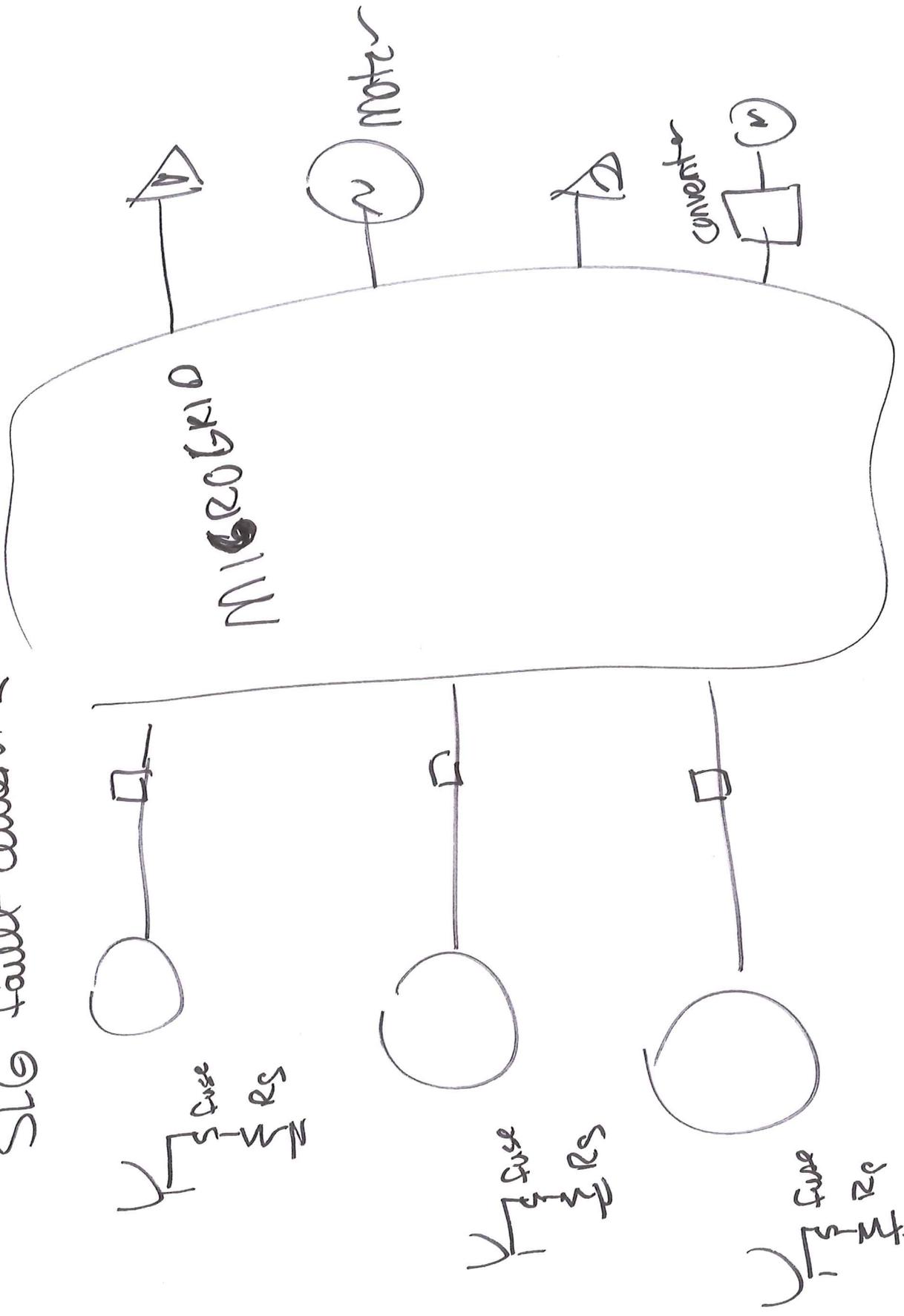
High Resistance Ground (option)

$$3R_G = X_{CO}$$



SLG fault current < 25A

2/3 227



UNgrounded

Fault Detector

SLG: $V_{ng} = 3V_0$

LL, DLG, 3Ø - Overcurrent
+ Directional
determination
as earlier

- Directional Determination
in Ungrounded or high resistance
grounded

→ very small current

→ $3I_0$

↳ ① Determine with
 $I_A + I_B + I_C$

⇒ ① mathematical sum
in relay

CT input



Analog to Digital Converter

- fixed number of bits

→ if we have a 4 bit A/D

1 bit is sign bit

3 bits for the number

2³ combinations

→ 0 to peak

→ 200 A secondary (pk) → 100% CT

111 - 200A

⋮

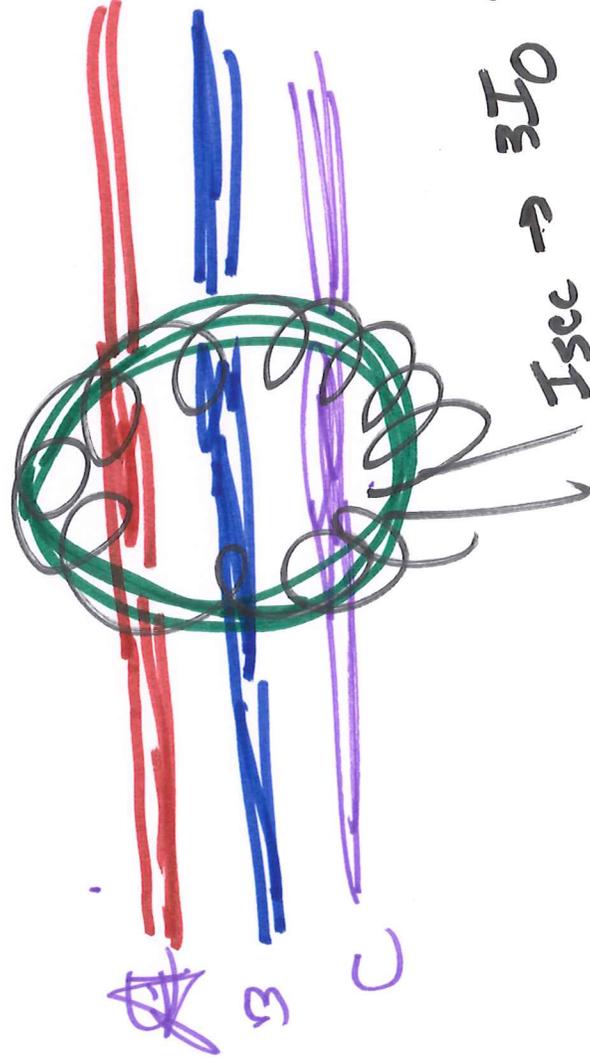
000 → 0A

SLG → 20A primary

$$\downarrow$$

$$\frac{20A}{CTR} = 0.1A \text{ second}$$

—
 $I_A + I_B + I_C \rightarrow$ magnetically



$I_{sec} \rightarrow 3I_o \Rightarrow$ Put this into a scab relay input with small currents

If a system is high R grounded

→ \mathbb{F}_n could be used in a similar

fashion

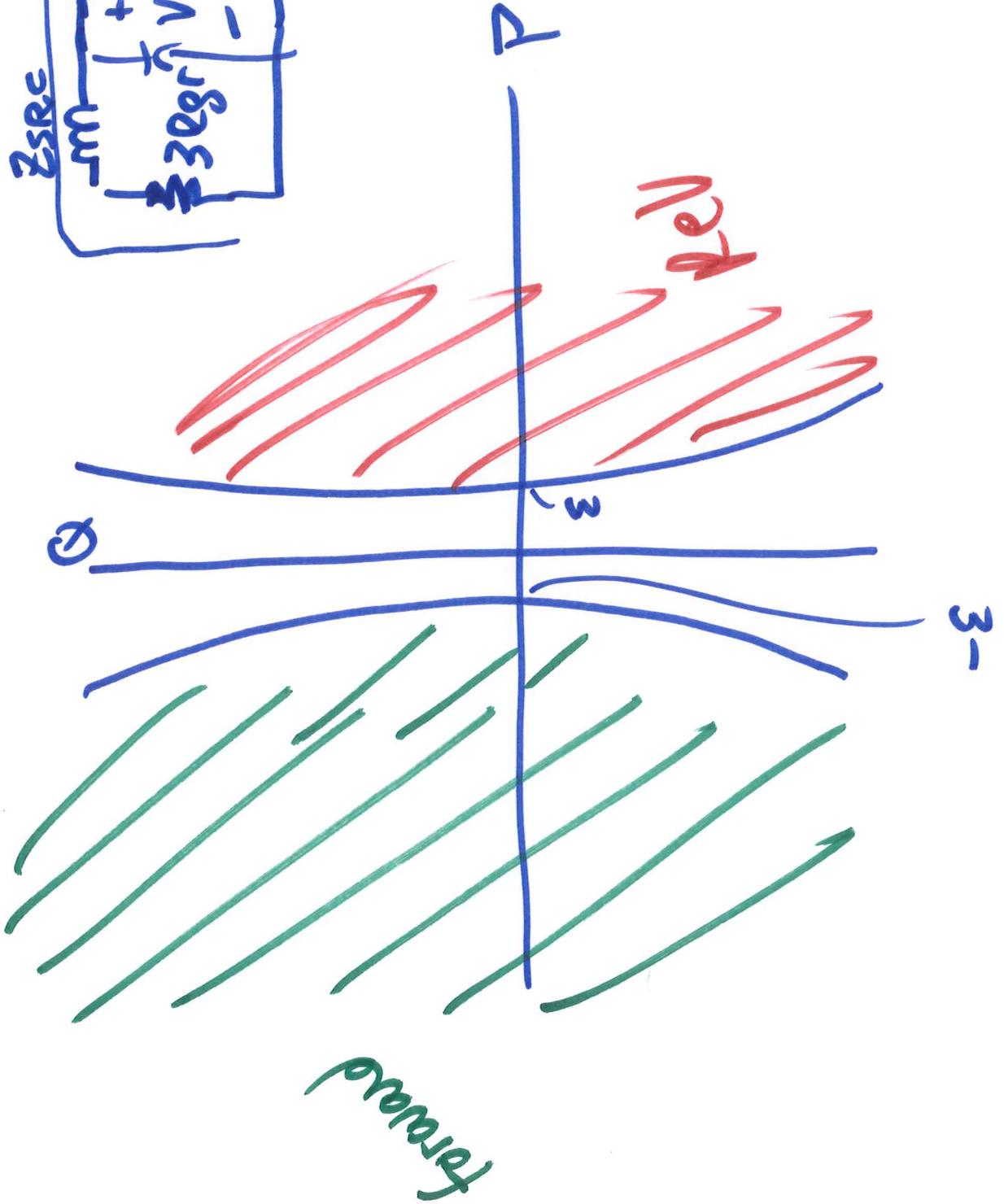
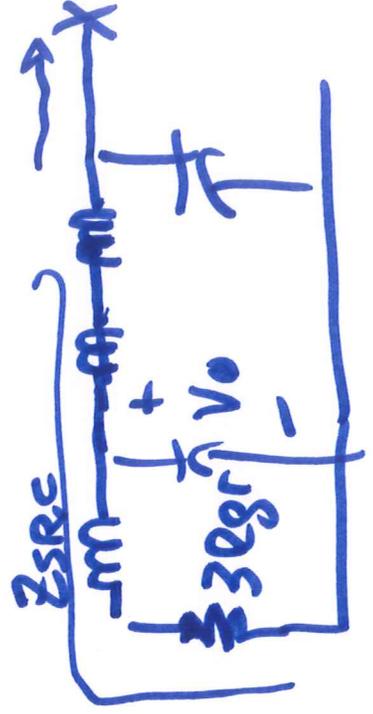
Directional Calculation Options

(1) Wattmetric Method

→ high resistance grounded

$$W_0 = \operatorname{Re} [V_0 \cdot I_0^*]$$

$$\text{or } \operatorname{Re} [3V_0 \cdot 3I_0^*]$$



VARMETRIC METHOD

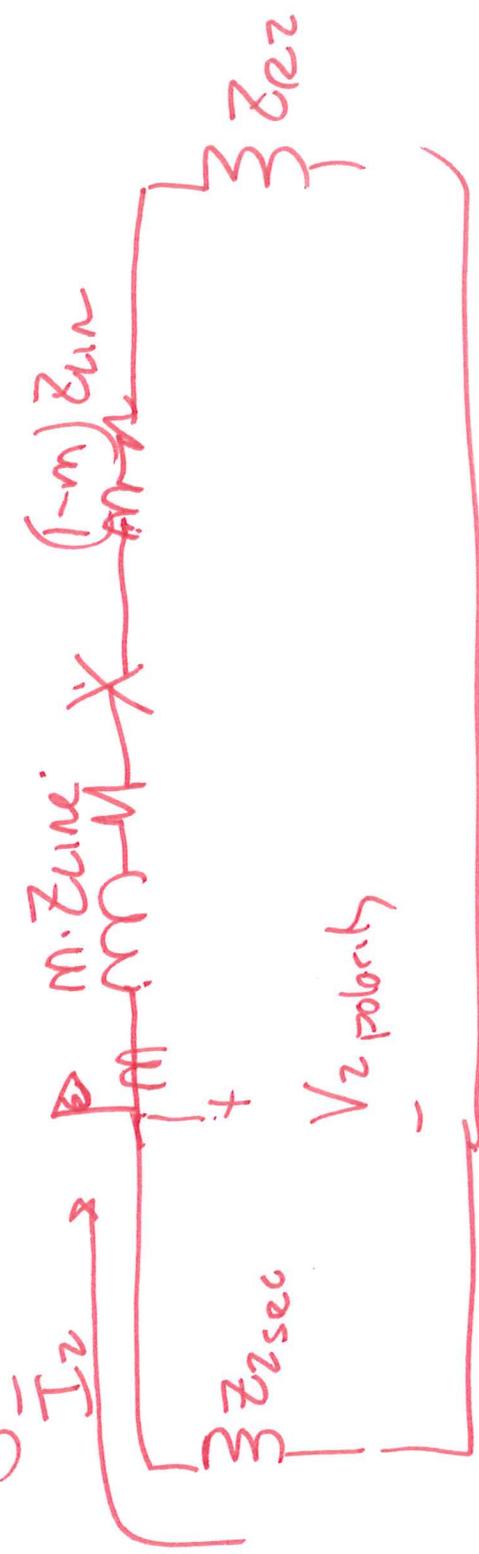
$$Q_0 = I_m \left(-3V_0 \cdot 5I_0^* \right) \uparrow$$

→ inductive grounded
- ~~un~~ ungrounded

Susceptance

$$B_0 = I_m \left(I_0 / V_0 \right)$$

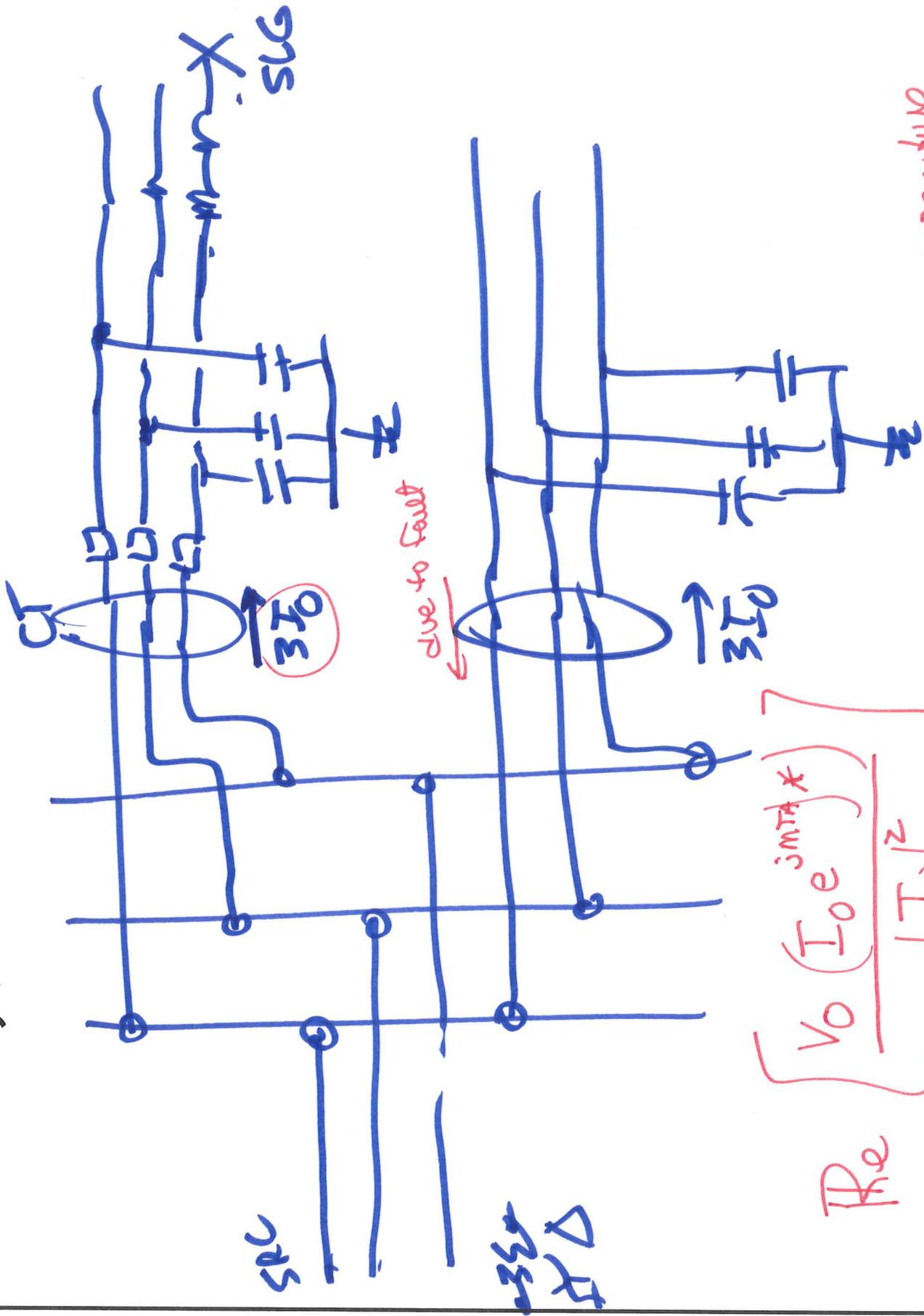
Negative sequence directional element



$$V_2 = I_2 Z_{sec} \angle \theta_{Z_{sec}}$$

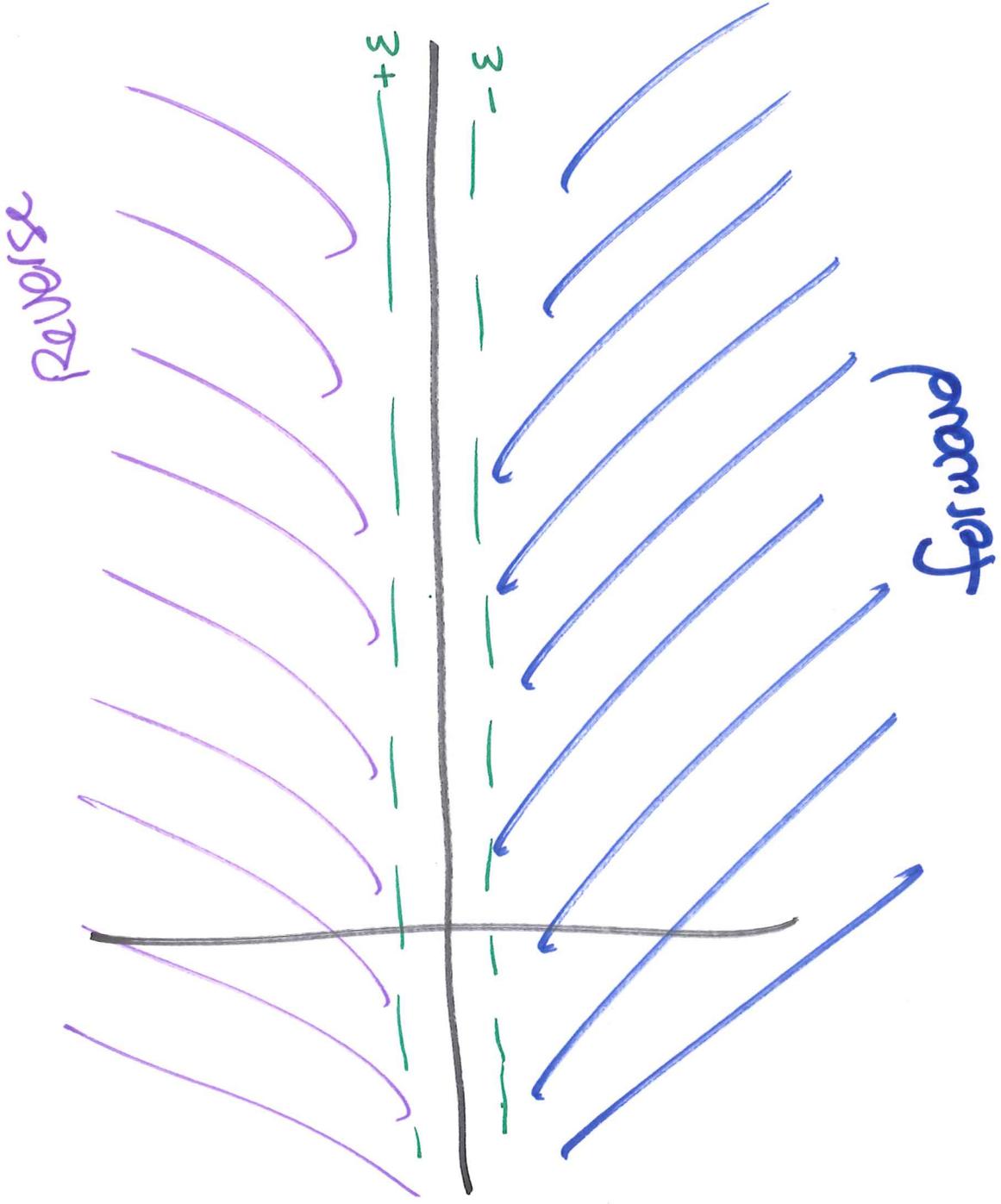
$$\text{Re} \left[\frac{V_c (I_2 e^{j\theta_{I_2}})}{|I_2|^2} \right] = -|Z_{sec}|$$

for forward fault



$$\text{Re} \left[\frac{V_o (I_{oe}^{jMTA})}{|I_o|^2} \right]$$

$MTA = -90^\circ \rightarrow$ capacitive fault current

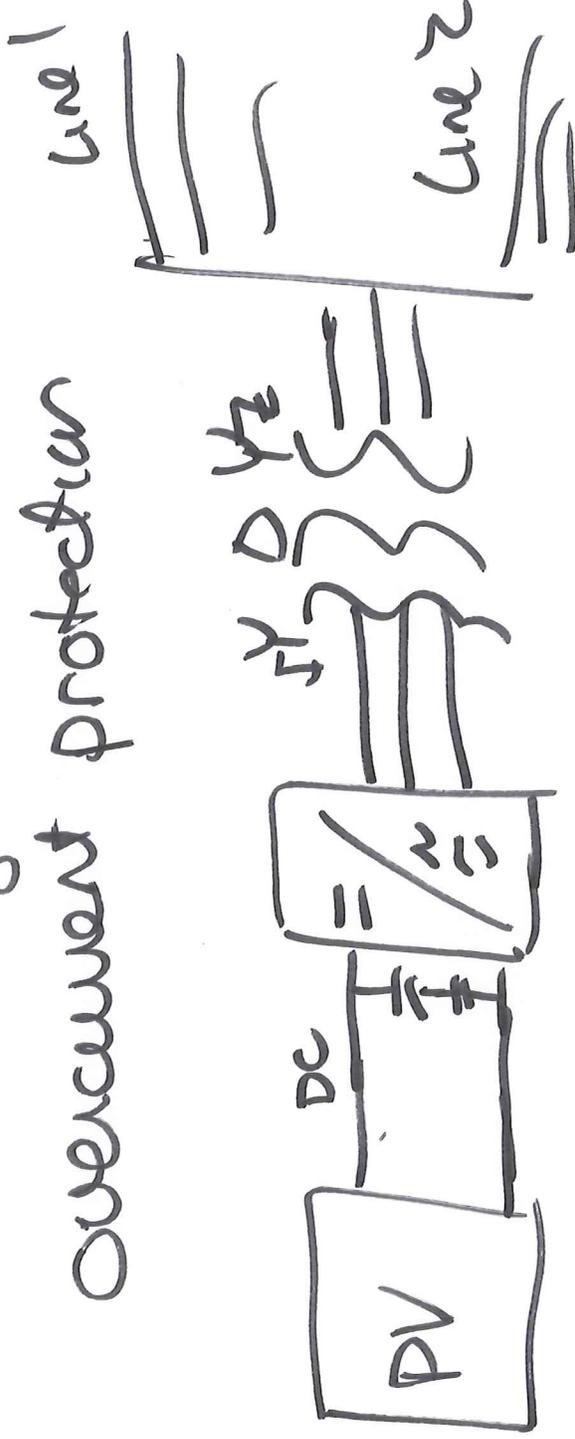


- If system is high resistance grounded - -

MTA \rightarrow angle of fault current

with $3R_E$ in parallel with X_C0

Challenges of voltage source
 converter generation for
 overcurrent protection



fast
 current

regulator \rightarrow limits $|I|$ to 1.2-1.5 pu

Regulator's $Pf \Rightarrow$ unity capacitor - some also regulate $I_2 = 0$

- some also have to boost current voltage $I_0 = 0$