

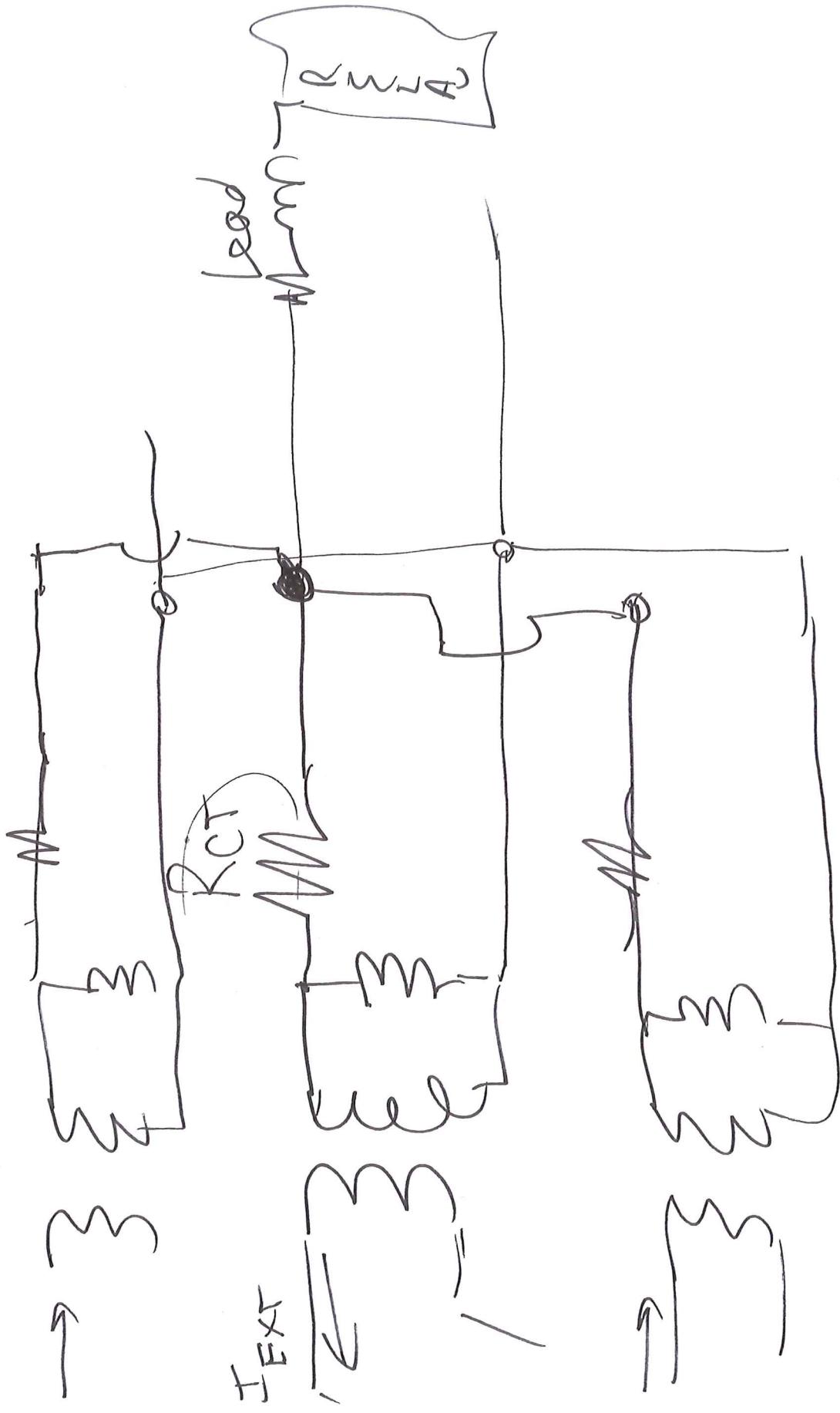
ECE 525

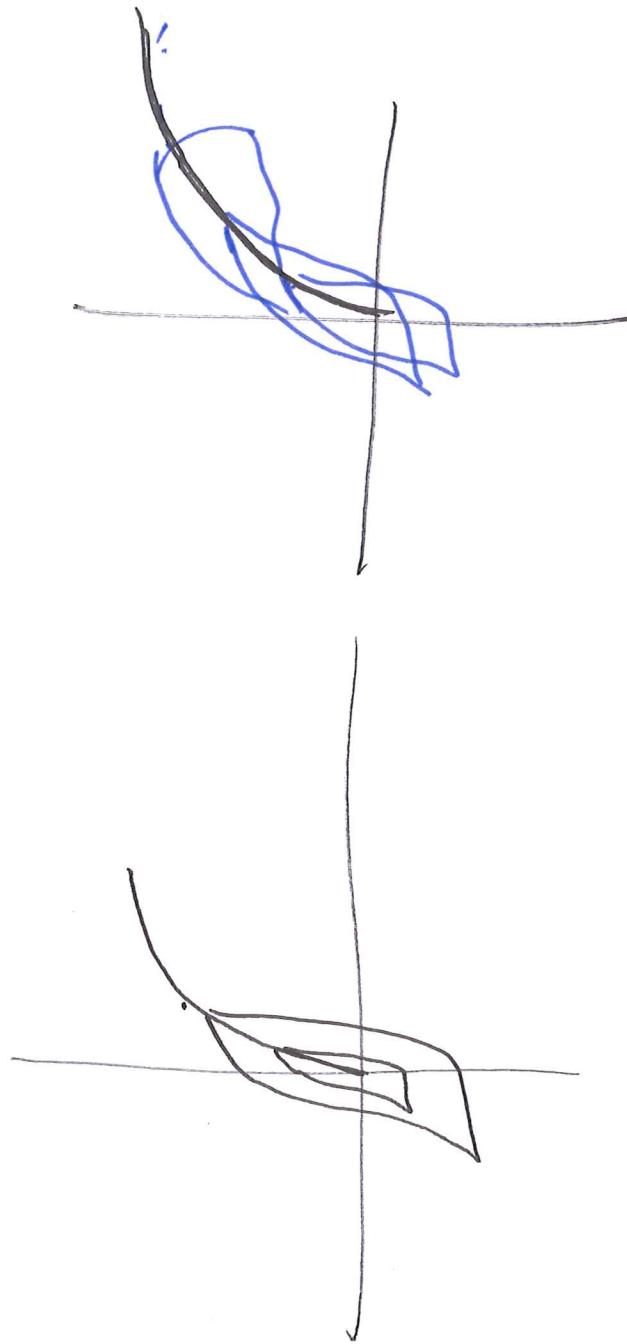
POWER SYSTEM PROTECTION
AND RELAYING

SESSION no. 26

University of Idaho

16 / 14



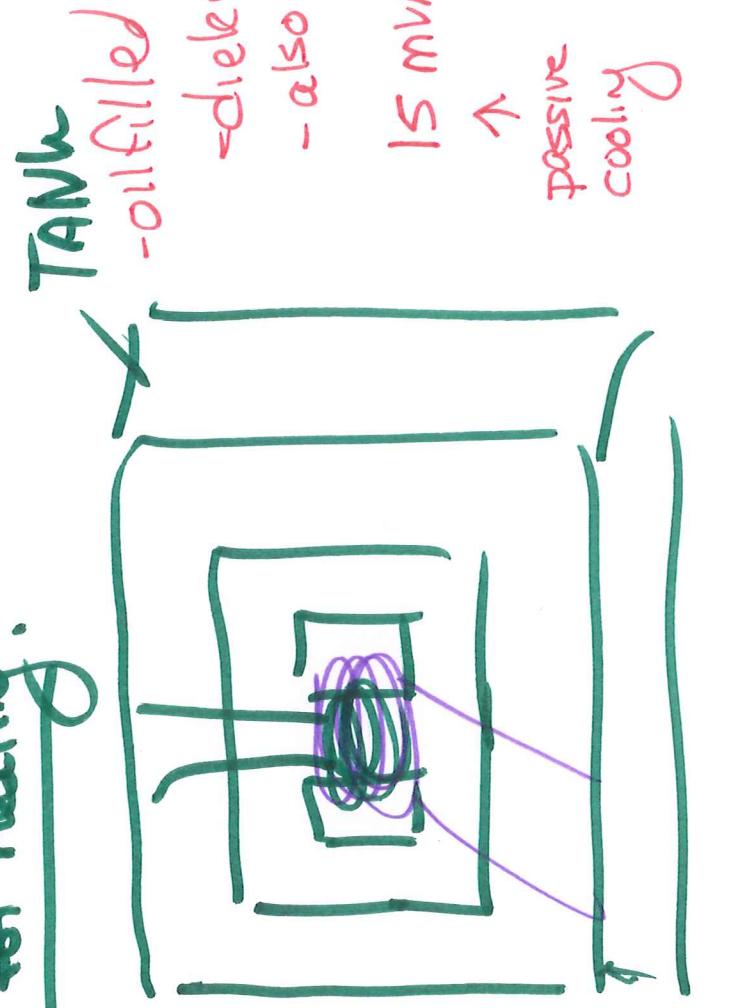


Transformer protection

- Failure of transformer can have long time consequences
 - long replacement time
 - minimize impact of transformer faults
 - reduce likelihood of external events that impact life of insulation

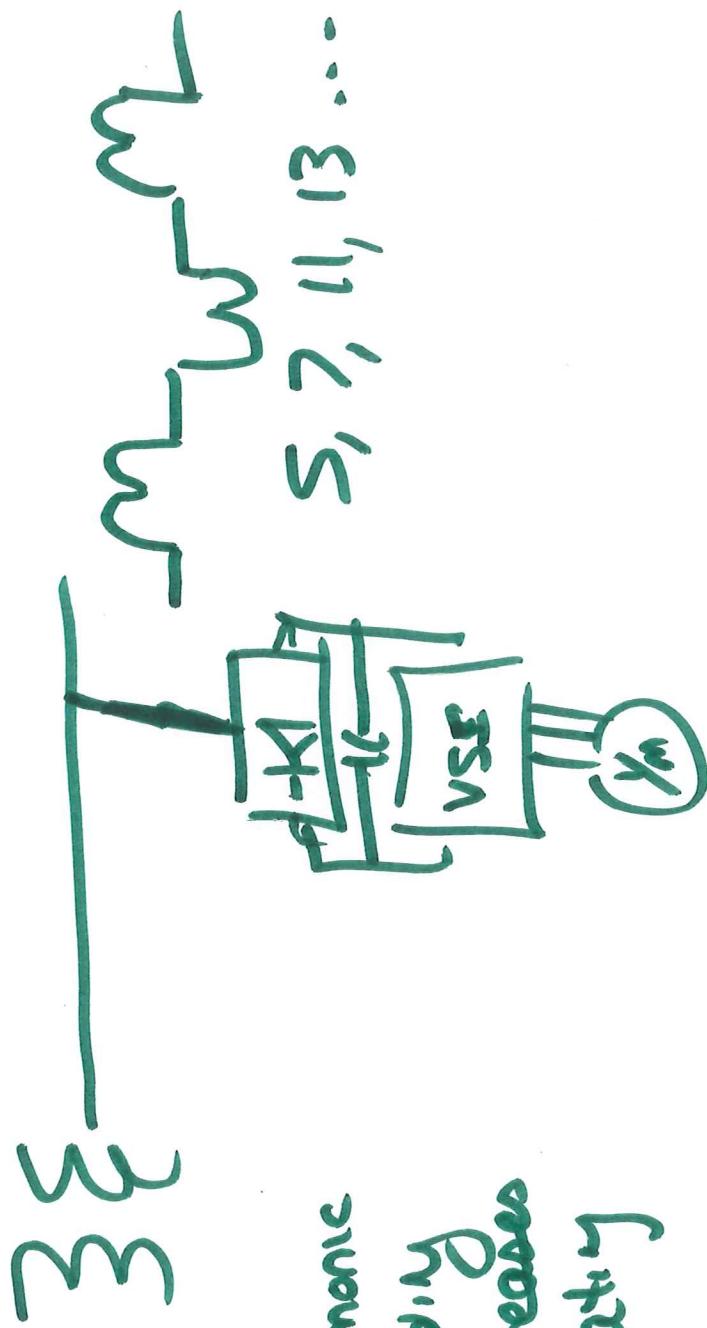
- heating & insulation has big impact on life
- also transient overvoltage

Causes for heating:



15 MVA / 20 MVA / 25 MVA

- Harmonic current loading due to external loads



- harmonic loading increases heat

- ω factor and transient

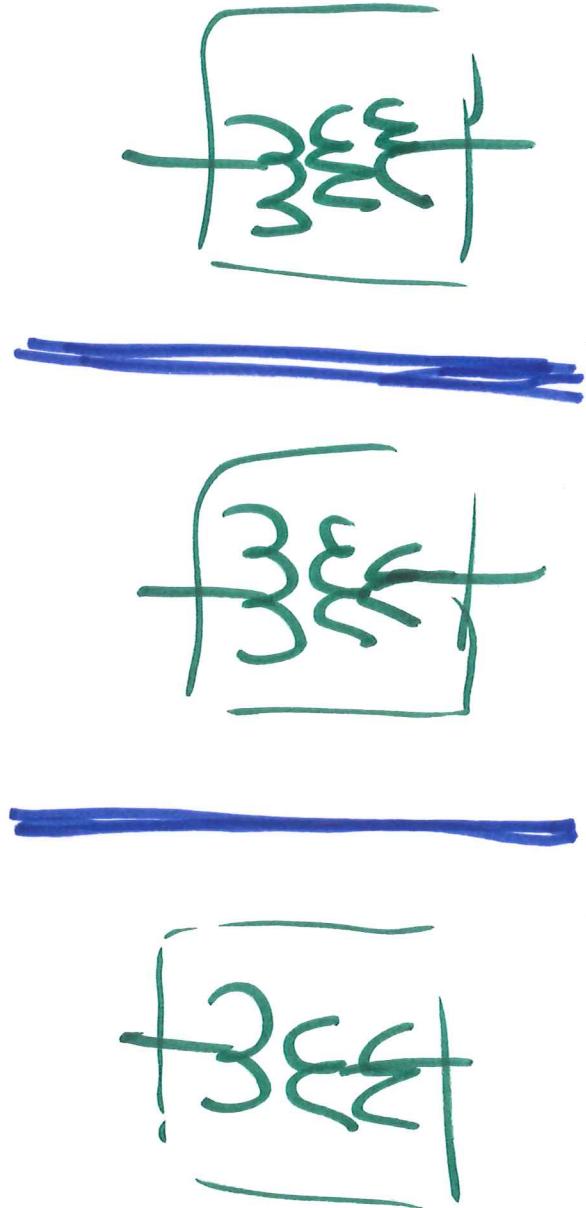
- overexcitation
- steady state overvoltage
 - detect based on harmonics
 - partial saturation
 - odd harmonics \rightarrow $\sin \theta$
- through faults (transformer is carrying current to a fault)
- similar with frequent large motor starts or even short or even overexcitation, or even overvoltage

Track sources of heating &
predict life span loss

C 37. Q1

Protection of internal faults

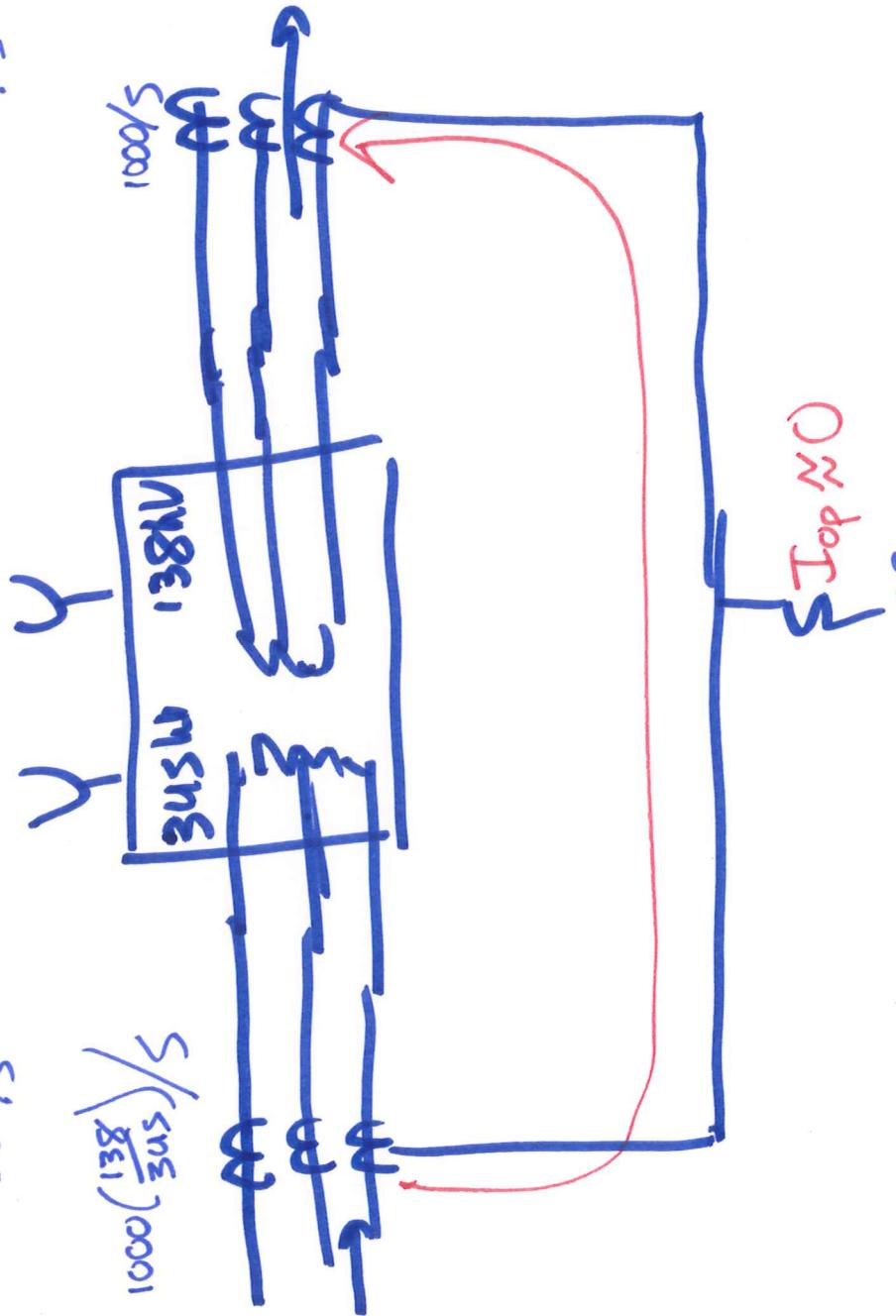
- a fault that evolves to a point where there is a time can log repair time



Jawwalls

→ First line: Different protection

soot: 2500W
CT_{local}/s



— 195 : 2500 : 2501 — 25 : 2 — 25 : 7 — 195,

2. Permutation and Combination

1. CT ratios may not cancel the Power Transfer ratio

3: Magnetizing Current

- Transformer always draws
- 2-4% of rated current in steady-state

→ magnetizing inrush current



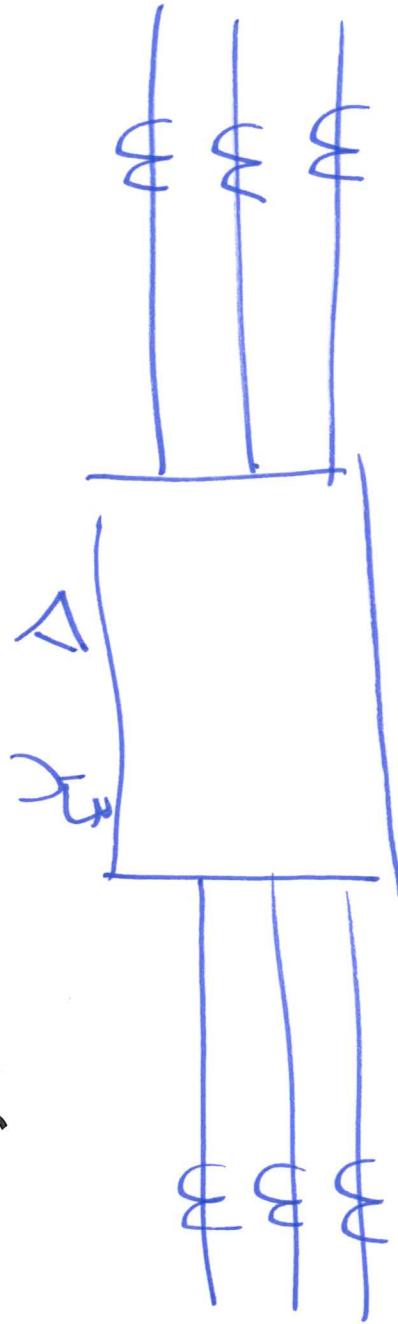
Transformer Phase Shift

$\Delta Y, (\gamma\Delta)$ \Rightarrow ANSI/IEEE Standard

$\Rightarrow V_{LN}$ on HV side leads view on LV side by 30°

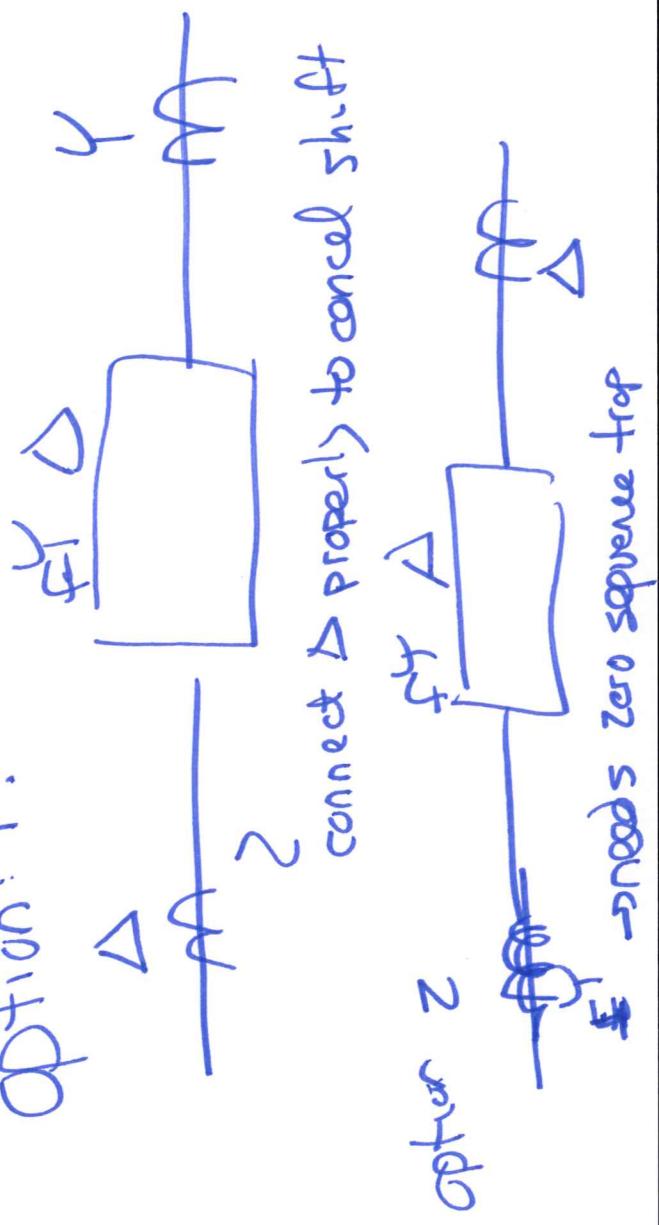
$\rightarrow \Delta Y / \rightarrow$ impact turns ratios

$\rightarrow \Delta Y$ we will not have I_0

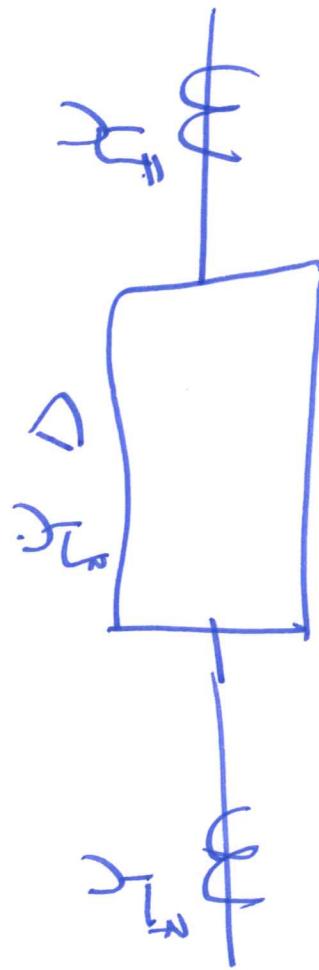


E-m relays

option 1:



microprocessor relay



→ relay perform math
to compensate for
Shift
— And remove To
matrix multiplication

Compensation matrices for transformer differential protection

- Apply one for each winding of the transformer
- Typical usage is:

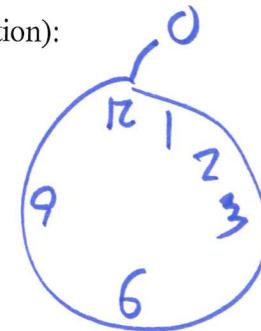
$$\begin{pmatrix} I_{A.sec_cor} \\ I_{B.sec_cor} \\ I_{C.sec_cor} \end{pmatrix} = \underline{\text{MAT}_{\text{correction}}} \cdot \frac{1}{\text{Tap}_{\text{HV}} \cdot \text{CTR}_{\text{HV}}} \cdot \begin{pmatrix} I_{A_Primary} \\ I_{B_Primary} \\ I_{C_Primary} \end{pmatrix}$$

Power Transformer Primary

- Matrices for commonly used transformer connections in the North America
 - Standard Y Connected winding (Y_0 using IEC clock position notation):

V_A
↑

$$\text{MAT}_0 := \begin{pmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$



- Δ connected winding, D_{AB} (D_1 using IEC clock position notation):

Δ_{AB}

$$\text{MAT}_1 := \frac{1}{\sqrt{3}} \cdot \begin{pmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ -1 & 0 & 1 \end{pmatrix}$$

- Δ connected winding, D_{AC} (D_{11} using IEC clock position notation):

$$\text{MAT}_{11} := \frac{1}{\sqrt{3}} \cdot \begin{pmatrix} 1 & 0 & -1 \\ -1 & 1 & 0 \\ 0 & -1 & 1 \end{pmatrix}$$

- Zero sequence removal matrix:

$$\text{MAT}_{12} := \frac{1}{3} \cdot \begin{pmatrix} 2 & -1 & -1 \\ -1 & 2 & -1 \\ -1 & -1 & 2 \end{pmatrix}$$