

ECE 525

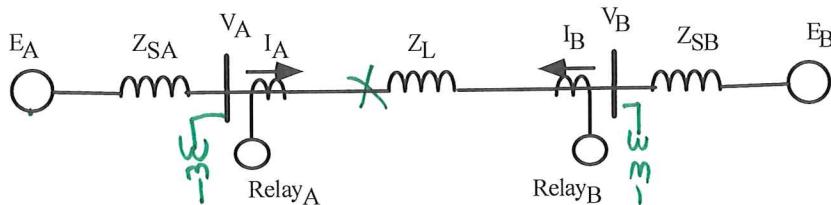
POWER SYSTEM PROTECTION
AND RELAYING

SESSION no. 4

ECE 525: Homework #1

L1 Due Session 6 (Sept. 6)

1. Given the power system below:



Where the following are given as CT and VT secondary quantities::

$$E_{SA} := 70V \cdot e^{j \cdot 0\text{deg}} \quad E_{SB} := 70V \cdot e^{-j \cdot 30\text{deg}}$$

$$Z_{SA1} := 1.5\text{ohm} \cdot e^{j \cdot 87\text{deg}} \quad Z_{SA2} := Z_{SA1} \quad Z_{SA0} := 5\text{ohm} \cdot e^{j \cdot 87\text{deg}}$$

$$Z_{SB1} := 0.8\text{ohm} \cdot e^{j \cdot 83\text{deg}} \quad Z_{SB2} := Z_{SB1} \quad Z_{SB0} := 2.5\text{ohm} \cdot e^{j \cdot 83\text{deg}}$$

$$Z_{L1} := 5\text{ohm} \cdot e^{j \cdot 82\text{deg}} \quad Z_{L0} := 18\text{ohm} \cdot e^{j \cdot 82\text{deg}}$$

The current transformer ratios are: CTR := $\frac{1200}{5}$

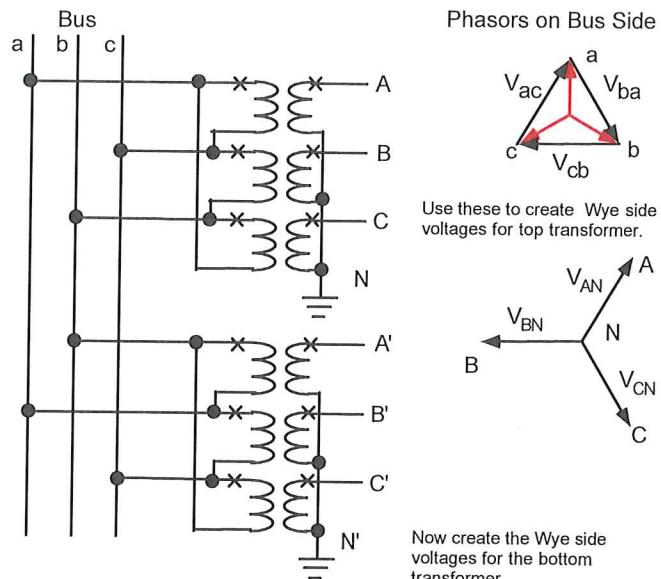
The voltage transformer ratios are: VTR := $\frac{132.8\text{kV}}{70\text{V}}$ Line-to-neutral

- A. Calculate the source voltages, line and source impedances and line current referred to primary values based on the information given above. Also find the line currents in secondary Amps accounting for CT polarity.
 - B. Repeat part A in per unit
 - C. Calculate real and reactive power flow at Bus A and Bus B based on the CT polarity using primary values
 - D. For the conditions of part A, calculate the effective impedance measured by Relay A and Relay B in terms of secondary values. $Z_{AG} = \frac{V_{AG}}{I_A + k_0 3 I_0}$ $Z_{AB} = \frac{V_{AB} - V_{B0}}{I_A - I_B}$
 - E. Suppose a 3 phase fault occurs 30% of the way from Bus A to Bus B, do the following:
 - (1) Calculate the total fault current and the current seen at Relay A and Relay B in primary and secondary quantities.
 - (2) Compare the fault currents to the load currents calculated earlier with load currents
 - (3) Calculate the effective impedances distance elements at Relay A and Relay B would calculate in secondary and primary ohms.
 - (4) What Iop and Irt be for a differential element (assume a charging current of 100 A capacitive divided equally between each end.
 - load condition \rightarrow
 - fault condition
- you can ignore load flow close $E_{SB} = 0$*

W

2. Sketch the winding connections for a Yg- Δ transformer following the ANSI/IEEE connection standard if (a) the Y-connected winding is the HV winding and (b) if the Δ -connected winding is the HV winding.

W



Note the phase sequence reversal through each transformer.

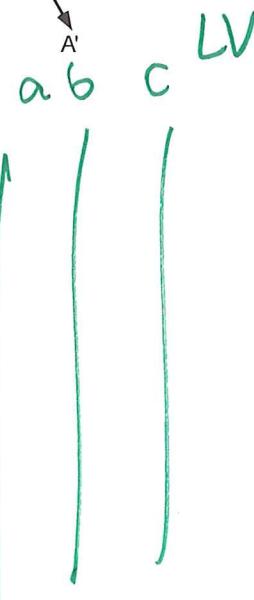
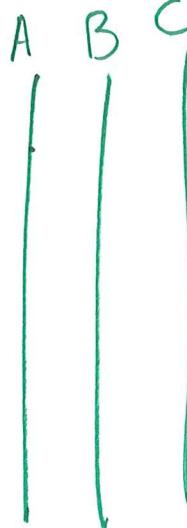
Phase relationships:

$V_{A'N'}$ lags V_{AN} by 120 degrees

$V_{B'N'}$ lags V_{BN} by 120 degrees

$V_{C'N'}$ lags V_{CN} by 120 degrees

HV



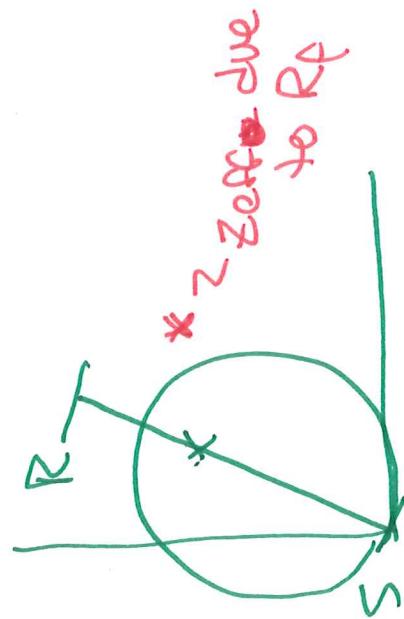
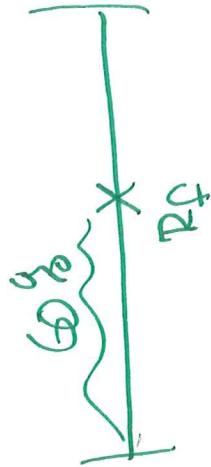
Protection response (and sometimes used in setting)

- Over-reaches
 - we have a response beyond (or more than) the setting
 - Zone 2 elements
 - over reach ~~past~~ end the line
 - In relay response to a fault
 - over reach if the element thinks fault is closer than actual location
-

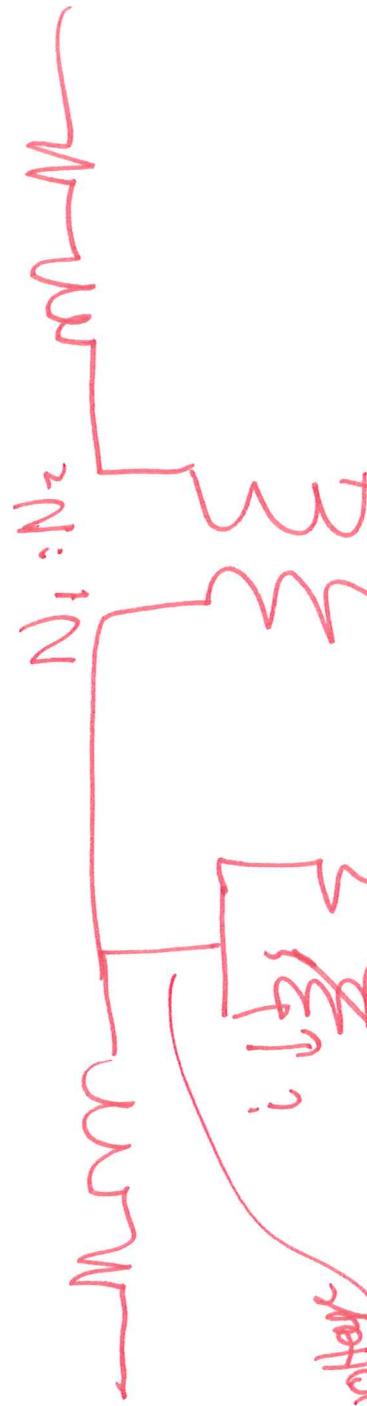
Under reach:

① setting less than length of line

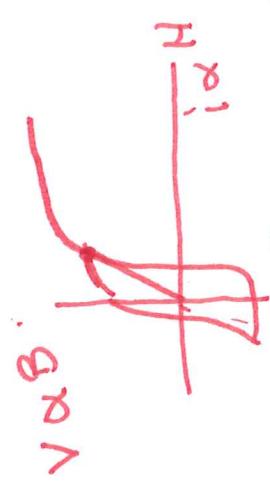
(example, a zone 1 is an underreaching element since set less than line length)



- ② Delay response
- protection element
 - thinks fault farther away than actual.



Dated voltage
2-350 or 1000

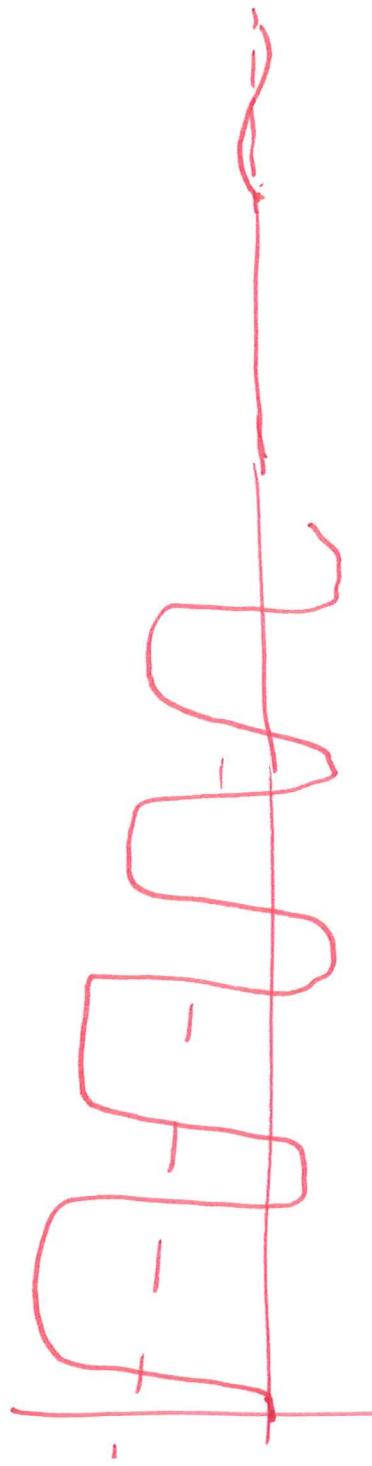


Hysteresis

Core loss

$$V = N \frac{d\Phi}{dt}$$

inrush current $\sim 5\text{-}10 \mu\text{s}$ worst case



harmonic spectrum

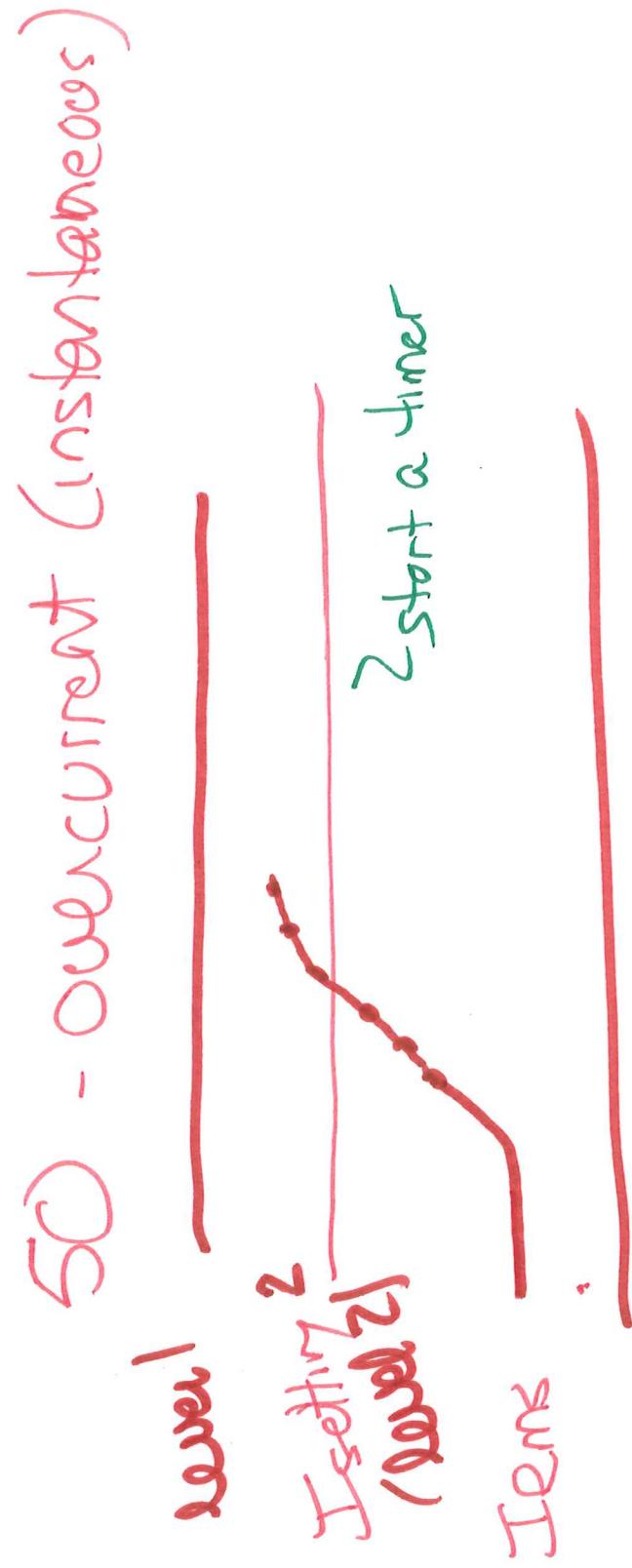
$-2\pi f_0$ ~~is~~ S_n harmonic

\hookrightarrow harmonic blocker

Line changing current



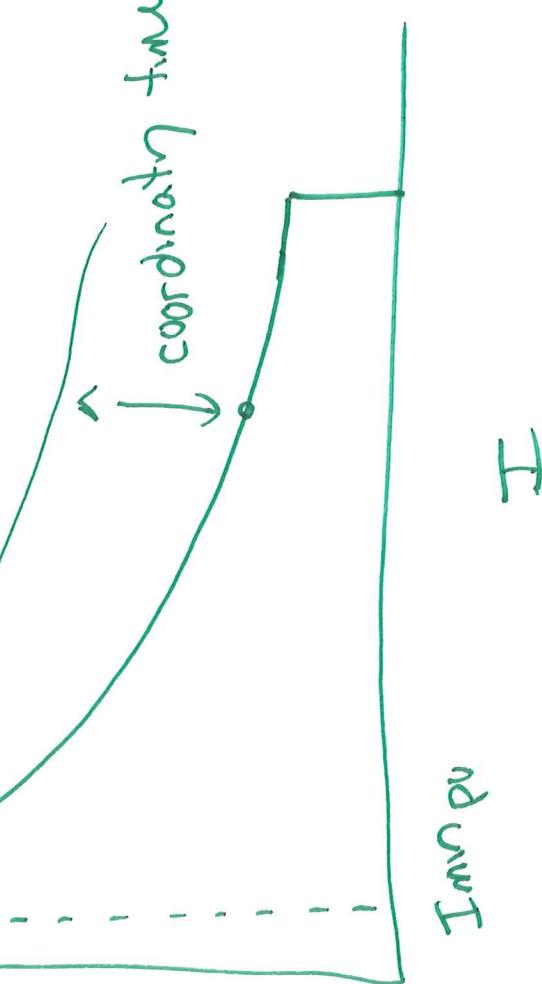
- Overcurrent on overvoltage (under voltage)
(Threshold comparison)

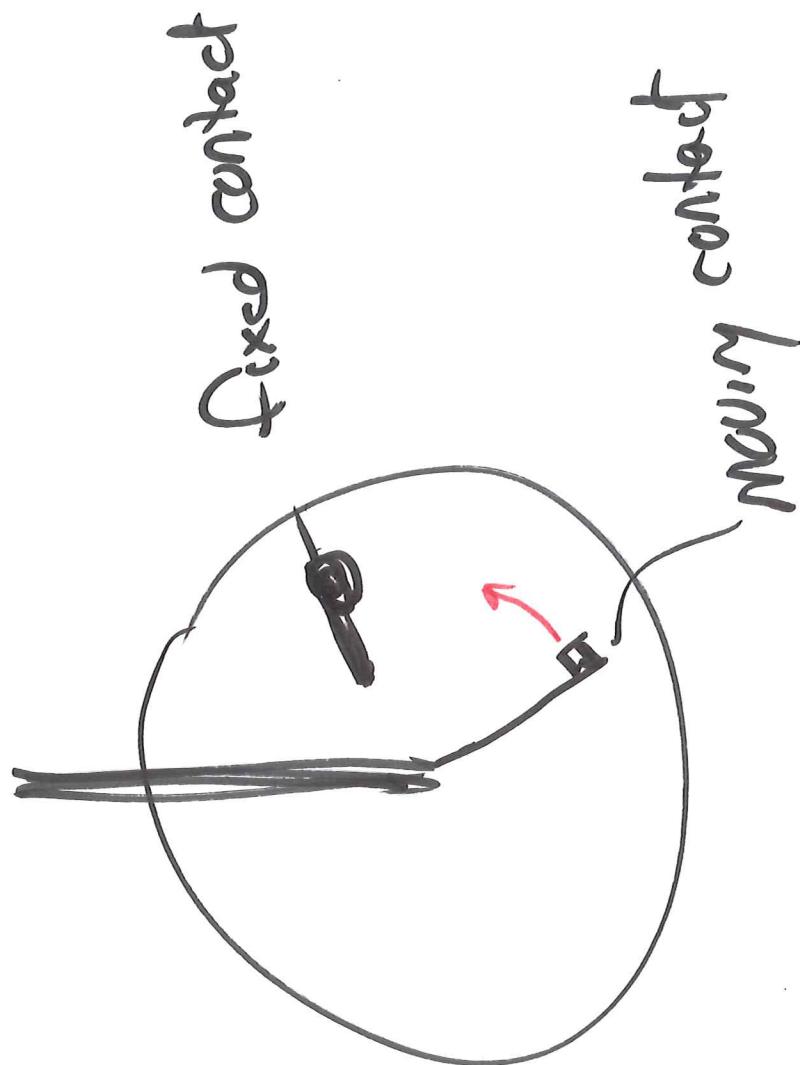


5 | - inverse time overcurrent

- very common in
distribution systems

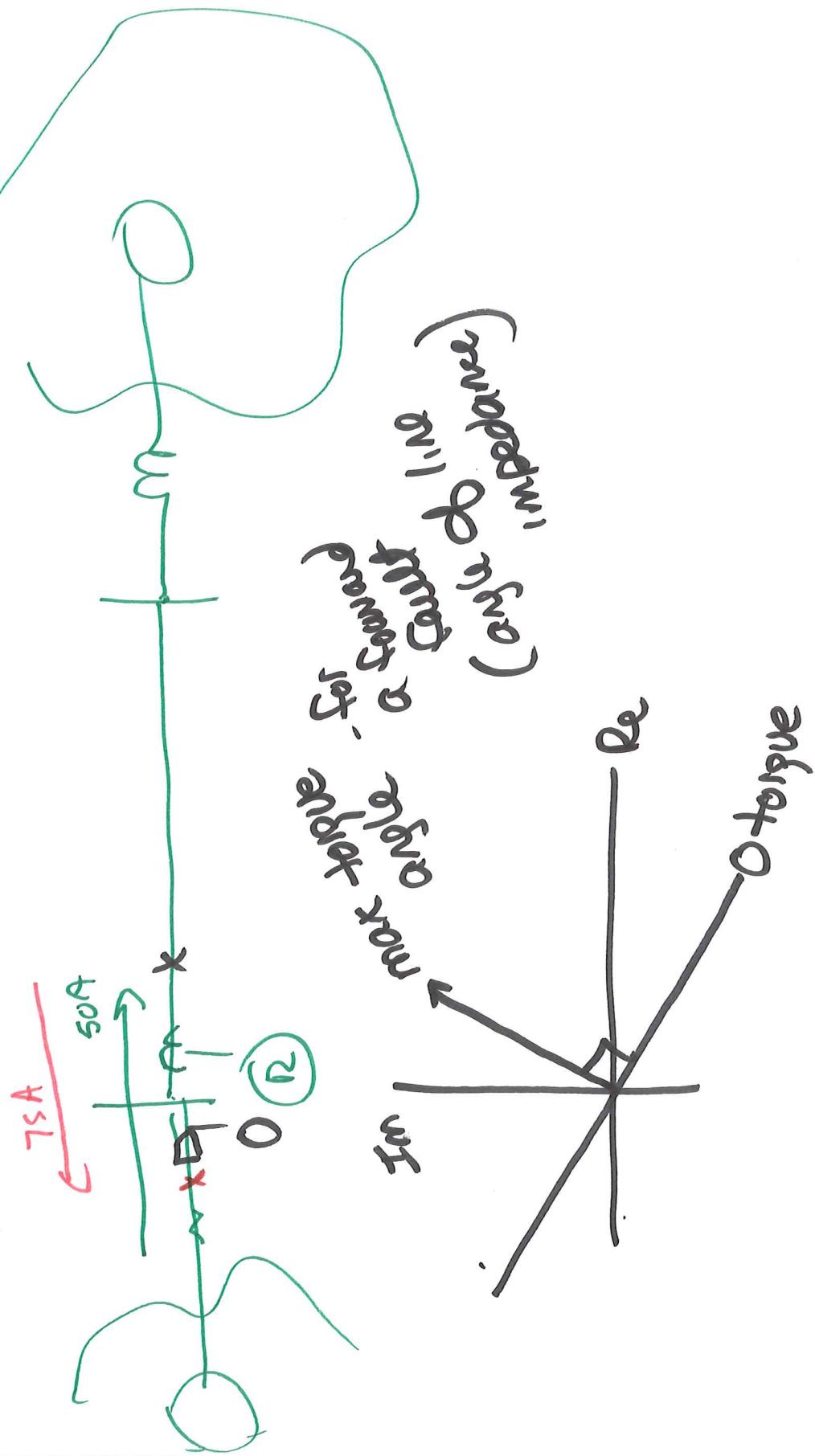
t

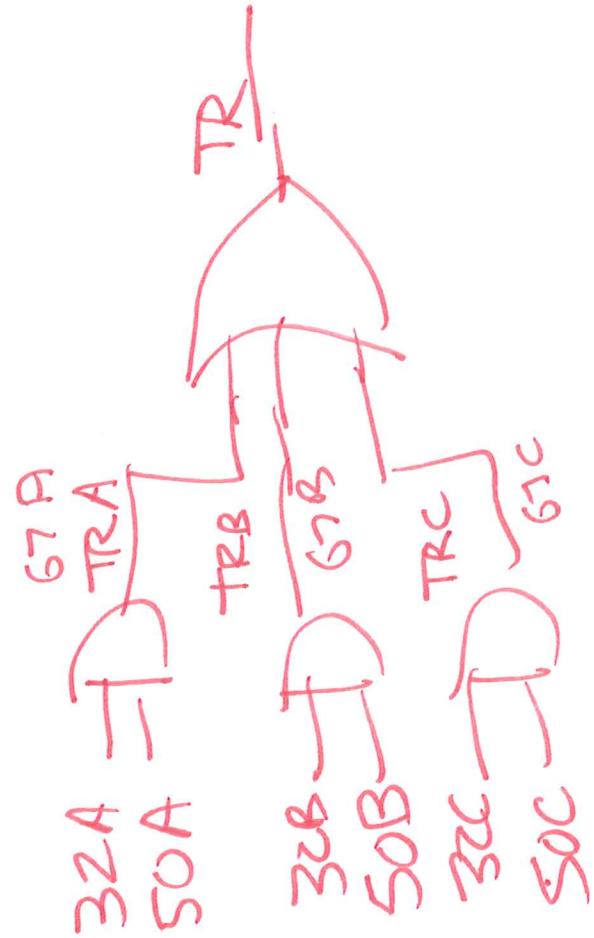
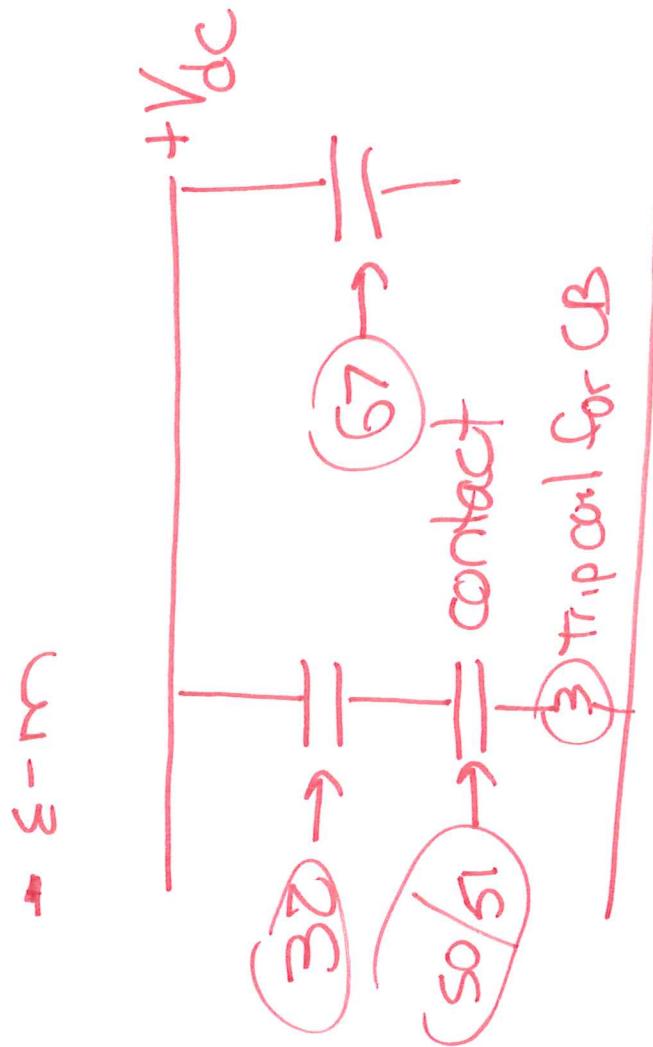




Directional Elements

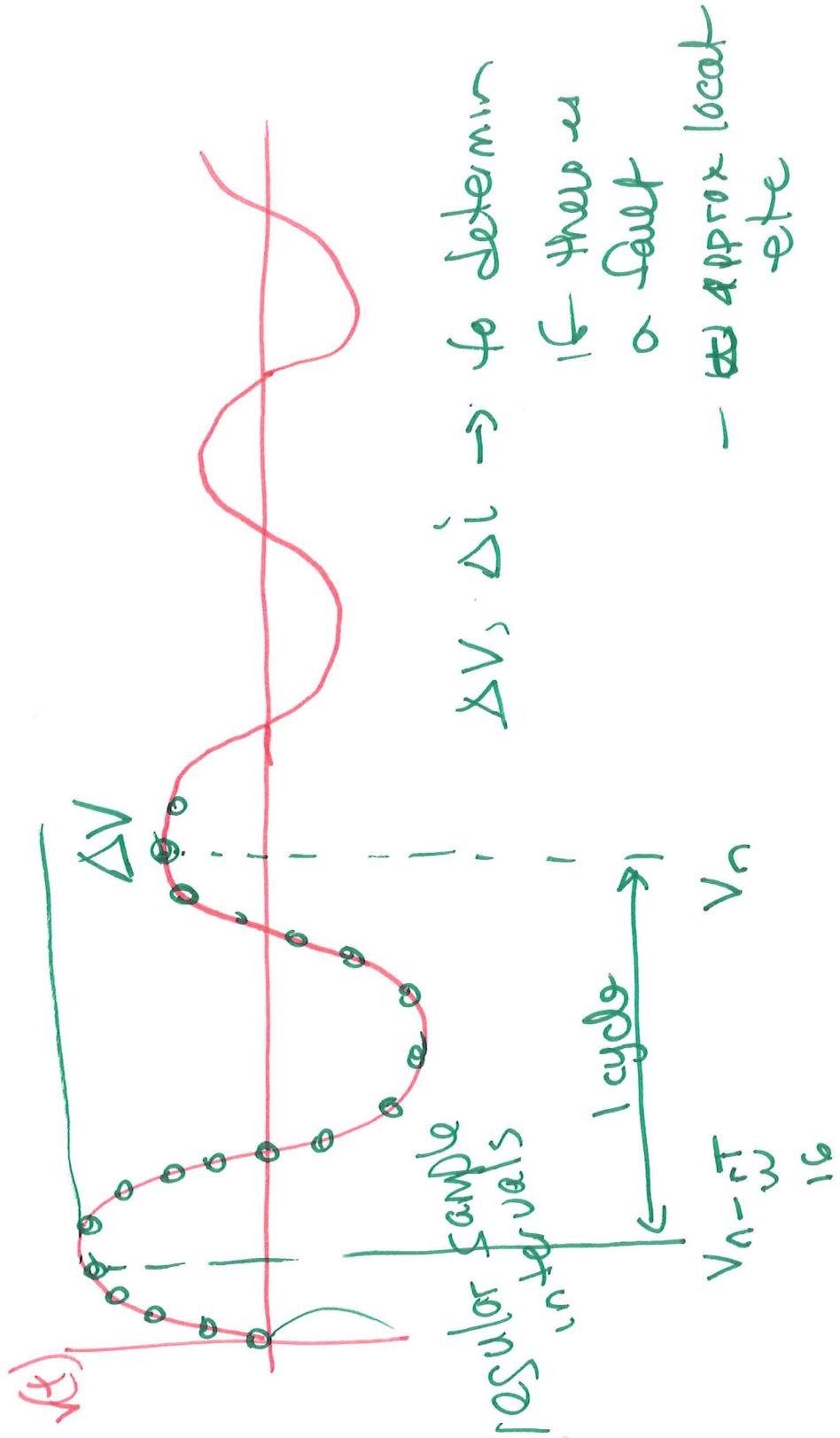
- supervision elements





TRANSIENT ELEMENTS

• Delta Quantiles (Superimposed quantiles)



Traveling waves

