

ECE 320: Lecture 12

Notes

Voltage Regulation

Compare the secondary voltage at no load with the secondary voltage at full load (one can vary the power factor). This determines the impact of the voltage drop across the series branch.

$$VR = \left[\frac{(V_{s_no_load} - V_{s_full_load})}{V_{s_full_load}} \right] \cdot 100\%$$

- V_s is the secondary voltage (or V_2).
- This is calculated using the voltage magnitudes, not the angle.
- Small numbers are often considered good.
- In some cases, a larger series impedance is preferred, since it will lower fault currents. But it hurts the voltage regulation.
- Alternate form for the equation (where V_p is the primary voltage, or V_1):

$$VR = \left[\frac{\left(V_p \cdot \frac{N_2}{N_1} - V_{s_full_load} \right)}{V_{s_full_load}} \right] \cdot 100\%$$

V_p is the voltage applied to the transformer (and is rated voltage). Assumes very small voltage drop due to magnetizing current at no load.

$V_{s_full_load}$ is the voltage appearing across the load, and V_p (or V_1) is voltage input to the transformer for supply the load at the given V_s value.

Efficiency

What percentage of the power in to the transformer is available at the output.

$$\eta = \frac{P_{out}}{P_{in}} = \frac{P_{out}}{P_{in} + P_{loss}}$$

- Ploss consists of:
1. Copper losses in windings
 2. Eddy current losses in core
 3. Hysteresis losses in the core.

Example: Suppose the transformer tested above is supplying a resistive load of 2.88 Ohm with a voltage of 240V across the load.

Find V_1 , Voltage Regulation, and Efficiency.

From last time:

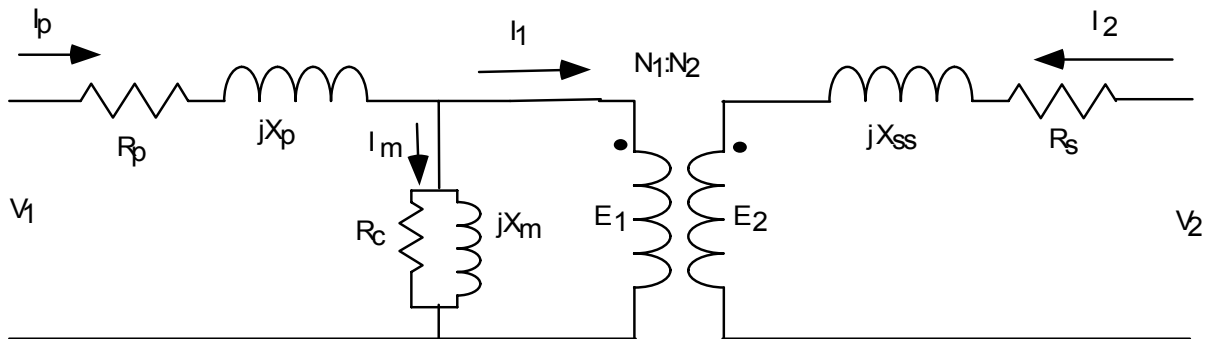
Since we don't know the exact number of turns, set N_1 and N_2 on relative voltage ratings.

$$N_1 := 8000 \quad N_2 := 277$$

$$R_1 := 19.2\text{ohm} \quad X_1 := 95.9\text{ohm} \quad \text{Referred to primary winding}$$

$$R_2 := 0.0173\text{ohm} \quad X_2 := 0.0863\text{ohm} \quad \text{Referred to secondary winding}$$

$$X_m := 38.45\text{k}\Omega \quad R_c := 160\text{k}\Omega \quad \text{Referred to primary winding}$$



Note that any of these quantities can be referred across the ideal transformer. So for example, we could refer X_m and R_c to the secondary winding.

$$X_{ms} := X_m \cdot \left(\frac{N_2}{N_1} \right)^2 \quad X_{ms} = 46.1 \Omega$$

$$R_{cs} := R_c \cdot \left(\frac{N_2}{N_1} \right)^2 \quad R_{cs} = 191.82 \Omega$$

Note that when referring an impedance across the ideal transformer, the impedance will get larger when going from a higher voltage winding to a lower voltage winding, or smaller when going from a lower voltage winding to a higher voltage winding. This is a good way to check your results.

We are given the voltage across the load:

$$V_2 := 240\text{V}$$

$$R_{\text{load}} := 2.88\text{ohm}$$

$$I_{\text{out}} := \frac{V_2}{R_{\text{load}}} \quad I_{\text{out}} = 83.33\text{ A}$$

$$P_{\text{out}} := \text{Re}(V_2 \cdot \overline{I_{\text{out}}}) \quad P_{\text{out}} = 20\text{kW} \quad \text{Loaded to rated load, with unity power factor}$$

Transformer secondary current:

$$I_2 := -I_{\text{out}} \quad \text{Note that } I_{\text{out}} \text{ and } I_2 \text{ have opposite polarities.}$$

$$E_2 := V_2 - I_2 \cdot (R_2 + j \cdot X_2) \quad |E_2| = 241.55\text{ V} \quad \arg(E_2) = 1.71\text{ deg}$$

$$E_1 := E_2 \cdot \frac{N_1}{N_2} \quad |E_1| = 6976.14\text{ V}$$

$$I_{\text{shunt}} := \frac{E_1}{R_c} + \frac{E_1}{j \cdot X_m} \quad I_{\text{shunt}} = 0.05 - 0.18i\text{ A} \quad |I_{\text{shunt}}| = 0.19\text{ A}$$

$$\arg(I_{\text{shunt}}) = -74.78\text{ deg}$$

$$I_1 := -I_2 \cdot \frac{N_2}{N_1} \quad I_1 = 2.89\text{ A}$$

$$I_p := I_1 + I_{\text{shunt}} \quad I_p = 2.93 - 0.18i\text{ A}$$

$$|I_p| = 2.94\text{ A} \quad \arg(I_p) = -3.51\text{ deg}$$

$$V_1 := E_1 + I_p \cdot (R_1 + j \cdot X_1) \quad |V_1| = 7063.37\text{ V}$$

$$\arg(V_1) = 3.94\text{ deg}$$

$$P_{\text{in}} := \text{Re}(V_1 \cdot \overline{I_p}) \quad P_{\text{in}} = 20.59\text{kW}$$

$$VR := \frac{\left(|V1| \cdot \frac{N2}{N1} - |V2| \right)}{|V2|} \quad VR = 1.9\%$$

$$\eta := \frac{P_{out}}{P_{in}} \quad \eta = 97.13\%$$

$$P_{loss} := P_{in} - P_{out} \quad P_{loss} = 590.25 \text{ W}$$

$$\text{Core losses:} \quad P_{core} := \frac{(|E1|)^2}{R_c} \quad P_{core} = 304.17 \text{ W}$$

$$\text{Copper losses:} \quad P_{loss} - P_{core} = 286.09 \text{ W}$$

$$\text{or we could do:} \quad (|I_p|)^2 \cdot R_1 + (|I_2|)^2 \cdot R_2 = 286.09 \text{ W}$$

Terminology

- X_m is often referred to as the magnetizing reactance, or a the excitation reactance.
- The parallel combination of R_c and X_m can be called the "shunt branch" or the "exciting branch".
- As mentioned above, the secondary winding terms, R_s , X_s , V_s , E_s , and I_s , are the same as the primary terms with a "2" (R_2 , X_2 , V_2 , E_2 , and I_2).
- Similar comments can also be made with the primary winding, as: V_p , I_p , R_p , X_p , and E_p or those with a "1" (R_1 , X_1 , V_1 , E_1 , and I_1). However, be careful since some people label I_1 as the current into the ideal transformer, and I_p as the terminal current ($I_p + I_{shunt}$).