

Sample Exam Solution

1. (20 pts) Either circle the correct answer or write in a short answer for each of the following.

A (T or F) the real power loss in an ideal capacitor is 0.

True. $P = 0$, but Q is not 0.

B What does total harmonic current distortion represent? What is considered to be a good number?

Total harmonic distortion, or THD, is a measure of how much harmonic distortion is present, relative to the magnitude of the fundamental component of the current.

$$\text{THD} = 100 \cdot \sqrt{\frac{(I_2)^2 + (I_3)^2 + \dots}{I_1^2}}$$

The lower the value of THD the better, ideally it is zero. Harmonic standards such as IEEE 519 upper limits for THD.

C You are given an iron core with a N -turn winding excited by an AC voltage source with a constant voltage magnitude. The peak flux density will (increase or decrease) when the frequency the voltage is increased.

It will decrease.

$$e(t) = E_m \cdot \cos(\omega \cdot t)$$

$$\phi(t) = \frac{1}{N} \cdot \int E_m \cdot \cos(\omega \cdot t) dt = \frac{-1}{N \cdot \omega} \cdot E \cdot \sin(\omega \cdot t)$$

Flux is divided by frequency, so a given voltage corresponds to a smaller flux as frequency increases. Then:

$$B = \frac{\phi(t)}{A} \quad \text{So if flux decreases with frequency, then flux density decreases.}$$

D Suppose a coil of wire is wrapped around a magnetic core. Will the inductance increase or decrease as the mean path length increases.

$$L = \frac{N^2 \cdot \mu_r \cdot \mu_0 \cdot A}{\text{length}}$$

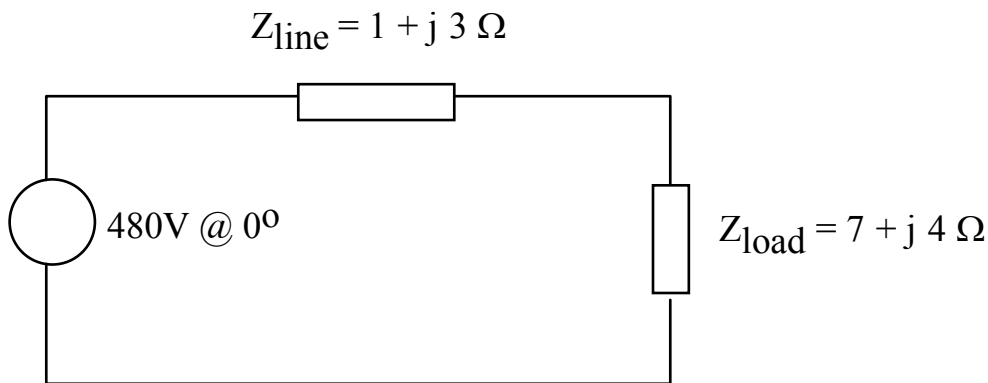
So if the length increases, L will decrease

E. Why does the open circuit test only show excitation losses (losses within the core) and not winding ($I^2 R$) losses?

The rated terminal voltage is applied to the transformer, but the load current is zero. Application of rated terminal voltage results in normal excitation and therefore normal excitation losses. However, with zero load current, the current through the windings is very small (only the small excitation current), so the i^2R losses are very small relative to the excitation losses.

2. (30 pts) Do the following given the 60 Hz circuit shown below:

A Calculate instantaneous power delivered by the source



$$V_S := 480V$$

$$Z_{\text{line}} := 1\text{ohm} + j\cdot 3\text{ohm}$$

$$Z_{\text{load}} := 7\text{ohm} + j\cdot 4\text{ohm}$$

$$I_S := \frac{V_S}{Z_{\text{line}} + Z_{\text{load}}}$$

$$I_S = 33.982 - 29.735i \text{ A}$$

$$|I_S| = 45.155 \text{ A}$$

$$\arg(I_S) = -41.186 \text{ deg}$$

$$v(t) := \sqrt{2} \cdot V_S \cdot \cos(2 \cdot \pi \cdot 60 \text{Hz} \cdot t) \quad \sqrt{2} \cdot V_S = 678.823 \text{ V}$$

$$i(t) := \sqrt{2} \cdot I_S \cdot \cos(2 \cdot \pi \cdot 60 \text{Hz} \cdot t - 41.186 \text{deg}) \quad \sqrt{2} \cdot |I_S| = 63.858 \text{ A}$$

$$2 \cdot |V_S| \cdot |I_S| = 43.348 \text{ kW}$$

$$p(t) = v(t) \cdot i(t) = \frac{43.48}{2} \text{ kW} \cdot [\cos[0 - (-41.186 \text{deg})] - \cos(4 \cdot \pi \cdot 60 \text{Hz} \cdot t - 41.186 \text{deg})]$$

$$P_{\text{AVE}} := \frac{2 \cdot |V_S| \cdot |I_S|}{2} \cos(41.186 \text{deg}) \quad P_{\text{AVE}} = 16.311 \text{ kW}$$

As a check, solve with phasors

$$\text{Re}(V_S \cdot \overline{I_S}) = 16.312 \text{ kW}$$

B Compute the power factor of the load

$$\text{PFangle} := \arg(Z_{\text{load}}) \quad \text{PFangle} = 29.745 \text{ deg}$$

$$\text{PF} := \cos(\text{PFangle}) \quad \text{PF} = 0.868 \quad \text{lagging}$$

C Determine the per phase capacitance needed to make the effective power factor of the load capacitor bank unity.

First find V_{load}

$$V_{\text{load}} := V_S - I_S \cdot Z_{\text{line}} \quad V_{\text{load}} = 356.814 - 72.212i \text{ V}$$

$$|V_{\text{load}}| = 364.048 \text{ V} \quad \arg(V_{\text{load}}) = -11.441 \text{ deg}$$

$$\text{kVA} := \text{kW} \quad \text{kVAR} := \text{kW}$$

We want Q_{cap} equal and opposite to the imaginary part of Q_{load}

$$S_{\text{load}} := (|I_S|)^2 Z_{\text{load}} \quad S_{\text{load}} = 14.273 + 8.156i \text{ kVA}$$

$$Q_{\text{cap}} := -\text{Im}(S_{\text{load}}) \quad Q_{\text{cap}} = -8.156 \text{ kVAR}$$

$$X_{\text{cap}} := \frac{(|V_{\text{load}}|)^2}{|Q_{\text{cap}}|} \quad X_{\text{cap}} = 16.25 \Omega$$

$$C_{\text{cap}} := \frac{1}{2 \cdot \pi \cdot 60 \text{ Hz} \cdot X_{\text{cap}}} \quad C_{\text{cap}} = 163.236 \mu\text{F}$$

$$Z_{\text{eq}} := \left(\frac{1}{Z_{\text{load}}} + \frac{1}{-j \cdot X_{\text{cap}}} \right)^{-1} \quad Z_{\text{eq}} = 9.286 \Omega \quad \text{purely real}$$

3. (30pts) A 1300:460V, 50 kVA single phase transformer supplies a rated kVA load at 0.8 PF lagging at 440V. The impedances referred to the high voltage side are:

$$R_1 := 0.5 \text{ ohm} \quad R_{2p} := 0.5 \text{ ohm} \quad N_1 := 1300$$

$$X_1 := 2.0 \text{ ohm} \quad X_{2p} := 2.0 \text{ ohm} \quad N_2 := 460$$

$$X_m := 400 \text{ ohm} \quad R_c := 1200 \text{ ohm}$$

A. Determine the transformer voltage regulation for this load.

$$V_{\text{load3}} := 440 \text{ V} \quad \text{set angle at } 0$$

$$\text{MagIload} := \frac{50 \text{ kVA}}{V_{\text{load3}}} \quad \text{MagIload} = 113.636 \text{ A}$$

$$\text{angIload} := -\text{acos}(0.8) \quad \text{angIload} = -36.87 \text{ deg}$$

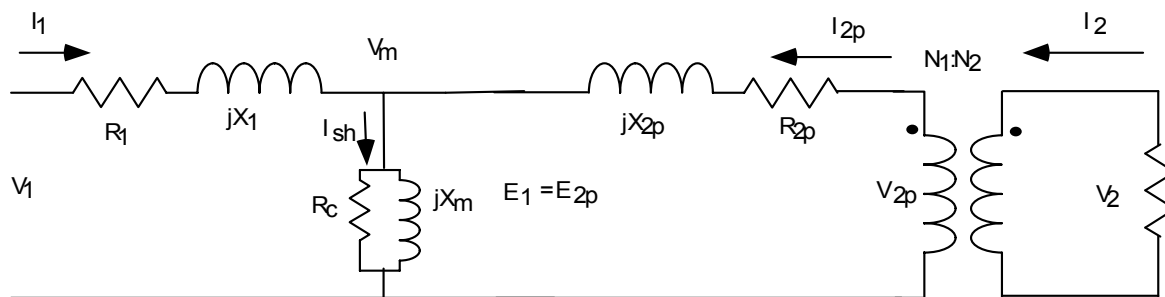
$$I_{\text{load}} := \text{MagIload} \cdot e^{j \cdot \text{angIload}}$$

$$I_2 := -I_{\text{load}}$$

Refer across ideal transformer

$$V_{2P} := \frac{N_1}{N_2} \cdot V_{\text{load3}} \quad V_{2P} = 1.243 \text{ kV}$$

$$I_{2P} := \frac{N_2}{N_1} \cdot I_2 \quad I_{2P} = -32.168 + 24.126i \text{ A} \quad |I_{2P}| = 40.21 \text{ A}$$



$$V_m := V_{2P} - I_{2P} \cdot (R_{2P} + j \cdot X_{2P}) \quad V_m = 1.308 \times 10^3 + 52.273i \text{ V}$$

$$|V_m| = 1.309 \text{ kV} \quad \arg(V_m) = 2.289 \text{ deg}$$

$$I_{sh} := \frac{V_m}{R_c} + \frac{V_m}{j \cdot X_m} \quad I_{sh} = 1.221 - 3.226i \text{ A}$$

Node equation for I1

$$I_1 := -I_{2P} + I_{sh} \quad I_1 = 33.388 - 27.352i \text{ A}$$

$$|I_1| = 43.161 \text{ A} \quad \arg(I_1) = -39.324 \text{ deg}$$

$$V_1 := V_m + I_1 \cdot (R_1 + j \cdot X_1) \quad V_1 = 1.379 \times 10^3 + 105.374i \text{ V}$$

$$|V_1| = 1.383 \text{ kV} \quad \arg(V_1) = 4.369 \text{ deg}$$

$$V_R := \frac{|V_1| - |V_{2P}|}{|V_{2P}|} \quad V_R = 11.239 \%$$

B. Determine the transformer efficiency

$$P_{in} := \text{Re}(V_1 \cdot \overline{I_1}) \quad P_{in} = 43.167 \text{ kW}$$

$$P_{out} := -\text{Re}(V_{load3} \cdot \overline{I_2}) \quad P_{out} = 40 \text{ kW}$$

$$\eta := \frac{P_{out}}{P_{in}} \quad \eta = 92.662 \%$$

Losses

$$P_{\text{loss}} := (|I_1|)^2 \cdot R_1 + (|I_2P|)^2 \cdot R_{2p} + \frac{(|V_m|)^2}{R_c}$$

$$P_{\text{loss}} = 3.167 \text{ kW}$$

4. (25 pts) The current waveforms drawn by a power supply fed by a sinusoidal voltage source have the following harmonic components (in RMS Amperes):

$$I_1 := 100\text{A} \quad I_3 := 50\text{A} \quad I_5 := 20\text{A} \quad I_7 := 14\text{A} \quad I_9 := 11\text{A} \quad I_{11} := 9\text{A}$$

A Calculate true RMS current. Compare this to the fundamental component RMS value and comment.

$$I_{\text{rms}} := \sqrt{I_1^2 + I_3^2 + I_5^2 + I_7^2 + I_9^2 + I_{11}^2}$$

$$I_{\text{rms}} = 115.317 \text{ A}$$

True RMS current is 15% larger

B Assuming the displacement power factor is 0.9 lagging, compute the true power factor.

True power factor is:

$$\text{pf} = \frac{P}{|S|} = \frac{(|V_1| \cdot |I_1| \cdot \cos(\phi_1))}{(|V_{\text{rms}}| \cdot |I_{\text{rms}}|)} = \frac{V_1}{V_{\text{rms}}} \cdot \frac{I_1}{I_{\text{rms}}} \cdot \text{displacement_factor}$$

Perfect sinusoidal voltage:

$$\text{pf} := 1 \cdot \frac{I_1}{I_{\text{rms}}} \cdot 0.9 \quad \text{pf} = 0.78 \quad \text{lagging} \quad \text{lowered due to harmonics}$$

C Compute total harmonic distortion in the current

$$\text{THD} := \sqrt{\frac{(I_3)^2 + (I_5)^2 + (I_7)^2 + (I_9)^2 + (I_{11})^2}{I_1^2}} \quad \text{THD} = 57.428 \%$$

ber?

relative