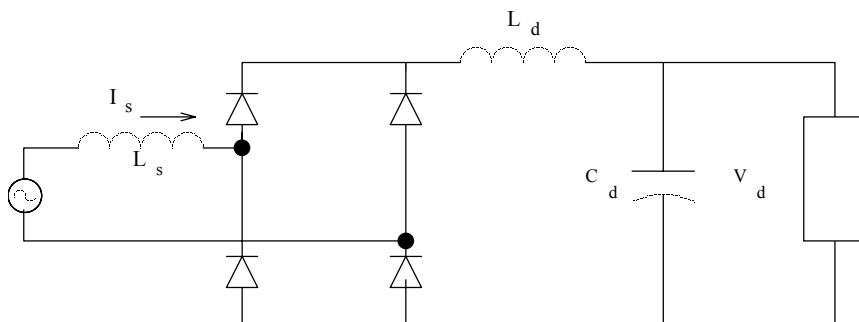


Sample Exam Solution

Problem 1: You are given a single phase diode rectifier, as shown below. Do the following:



$$V_d := 310V \quad X_s := 0.4\text{ohm} \quad \text{at } 400 \text{ Hz}$$

$$V_{\text{spk}} := 360V \quad V_s := \frac{V_{\text{spk}}}{\sqrt{2}} \quad \omega := 2 \cdot \pi \cdot 400\text{Hz}$$

$$L_s := \frac{X_s}{\omega} \quad L_s = 0.2 \text{ mH}$$

A. Assume that $L_d = 0$ and C_d is large. Plot the ac current versus time for one 400 Hz cycle. Determine the angles at which conduction begins in degrees. Also determine the peak dc current.

Since the capacitor voltage is fixed at 310 V, there will be no decrease in V_d due to the voltage drop across L_s , and since no current flows prior to diode turn on in this case, we can find θ_b from $V_d = V_s \cdot \sin(\theta_b)$. Note that we are already given the peak voltage

$$\theta_b := \text{asin}\left(\frac{V_d}{\sqrt{2} \cdot V_s}\right) \quad \theta_b = 59.4 \text{ deg}$$

Note: This exam was originally assigned as a take home exam, so solving for θ_f in order to plot the waveform was not a time issue. In the final in this class you won't need to do so.

Now solve for θ_f , using the equation for the current.

$$\theta_{f1} := 150\text{deg}$$

Given

$$\left[\sqrt{2} \cdot V_s \cdot (\cos(\theta_b) - \cos(\theta_{f1})) - V_d \cdot (\theta_{f1} - \theta_b) \right] = 0$$

$$\theta_f := \text{Find}(\theta_{f1}) \quad \theta_f = 152\text{deg}$$

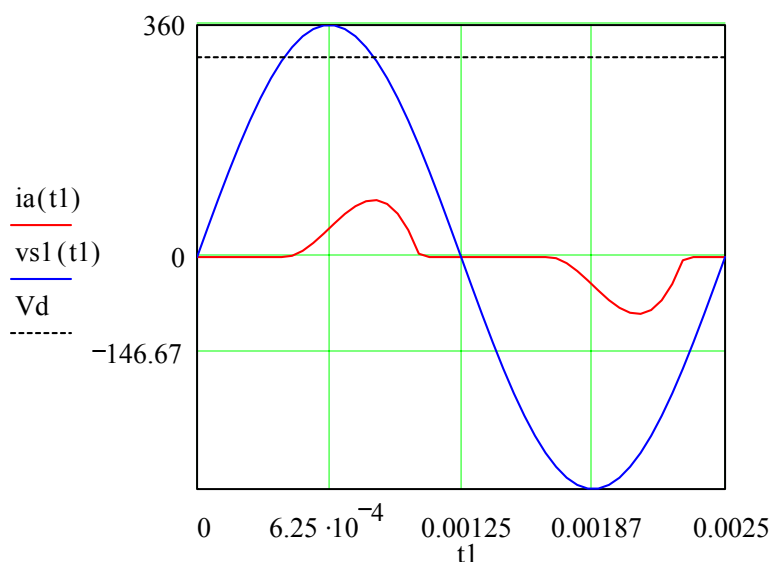
$$\theta_{b2} := \theta_b + \pi \quad \theta_{b2} = 239.4\text{deg}$$

$$\theta_{f2} := \theta_f + \pi \quad \theta_{f2} = 332\text{deg}$$

Expression for current (conditional so it doesn't reverse)

$$t_1 := 0, 0.00005\text{sec}.. 0.0025\text{sec} \quad v_{s1}(t_1) := \sqrt{2} \cdot V_s \cdot \sin(\omega \cdot t_1)$$

$$i_a(t_1) := \begin{cases} \left[\frac{1}{\omega \cdot (L_s)} \right] \cdot \left[\sqrt{2} \cdot V_s \cdot (\cos(\theta_b) - \cos(\omega \cdot t_1)) - V_d \cdot (\omega \cdot t_1 - \theta_b) \right] & \text{if } \theta_b \leq \omega \cdot t_1 \leq \theta_f \\ \left[\frac{1}{\omega \cdot (L_s)} \right] \cdot \left[\sqrt{2} \cdot V_s \cdot (\cos(\theta_{b2}) - \cos(\omega \cdot t_1)) + V_d \cdot (\omega \cdot t_1 - \theta_{b2}) \right] & \text{if } \theta_{b2} \leq \omega \cdot t_1 \leq \theta_{f2} \\ 0 & \text{otherwise} \end{cases}$$



Find angle of peak current and peak current:

$$\theta_p := \frac{\pi}{2} + \left(\frac{\pi}{2} - \theta_b \right) \quad \theta_p = 120.6 \text{ deg}$$

Convert to seconds:

$$t_{\text{peak}} := \frac{\theta_p}{\omega} \quad t_{\text{peak}} = 8.4 \times 10^{-4} \text{ s}$$

$$i_a(t_{\text{peak}}) = 88.5 \text{ A}$$

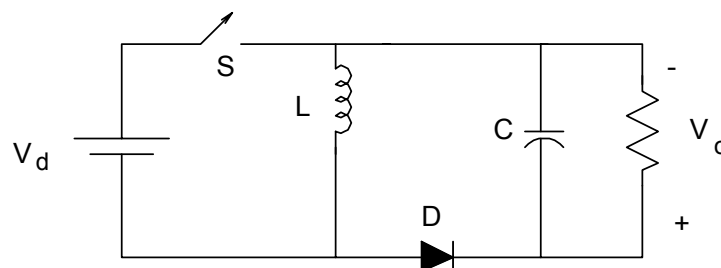
(b) In many cases it is desirable to have continuous conduction. Describe potential benefits to having continuous conduction. How would the circuit need to be modified from the conditions of part A to achieve continuous conduction? Would the voltages need to change?

1. If it is continuous conduction, the peak current will be lower (if the average current is the same). Also the harmonic content of the waveform may improve somewhat.
2. We would want to add enough inductance on the dc side of the circuit to bring it to continuous conduction. Adding additional inductance on the ac side can help somewhat too, but the dc side inductance has the larger impact.
3. There would be commutation overlap due to the ac side inductance, so the average dc voltage would be somewhat lower.

Problem 2: For the converter shown below, determine the following:

(a) What type of converter is it?

Buck-Boost



(b) Duty cycle

$$\begin{aligned} V_d &:= 25\text{V} & L &:= 0.2\text{mH} & R_{out} &:= 3.25\text{ohm} \\ V_o &:= 18\text{V} & f_s &:= 5\text{kHz} & T_s &:= \frac{1}{f_s} \end{aligned}$$

Solve the equation: $\frac{V_o}{V_d} = \frac{D1}{1 - D1}$ for D:

$$D := \frac{V_o}{V_o + V_d} \quad \boxed{D = 0.4}$$

Is it in continuous conduction?

$$I_{ob} := \frac{V_o \cdot (1 - D)^2}{f_s \cdot 2L} \quad I_{ob} = 3 \text{ A}$$

$$I_o := \frac{V_o}{R_{out}} \quad I_o = 5.5 \text{ A} \quad \text{Since } I_o > I_{ob}, \text{ continuous conduction}$$

So the result for D above is correct.

c. We want to limit ΔV_o to 0.5% of the output voltage. Determine the necessary capacitance.

$$\Delta V_o = \frac{I_o \cdot D \cdot T_s}{C}$$

$$\Delta V_o := 0.5\% \cdot V_o \quad \Delta V_o = 0.1 \text{ V}$$

Therefore we can solve for C:

$$C := \frac{I_o \cdot D \cdot T_s}{\Delta V_o} \quad \boxed{C = 5152.1 \mu\text{F}}$$

What would happen if a smaller capacitor was used?

If the size of the capacitor is decreased, the peak to peak ripple voltage would increase, and the current to the load would also show more ripple.

Problem 3

A. You are given a boost converter. You measure the input voltage to be 15 V from a 100W source and have an output current of 4 A. Assuming no power losses determine: input current, output voltage, duty ratio. The filter inductance is 100 μ H and the switching frequency is 10 kHz.

$$V_d := 15\text{V} \quad L := 100\mu\text{H}$$

$$P_{in} := 100\text{W} \quad f_s := 10\text{kHz}$$

$$I_{out} := 4\text{A}$$

$$P_{out} := P_{in} \quad V_{out} := \frac{P_{out}}{I_{out}} \quad \boxed{V_{out} = 25\text{V}}$$

$$I_{in} := \frac{P_{in}}{V_d} \quad \boxed{I_{in} = 6.7\text{A}}$$

$$D := \frac{V_{out} - V_d}{V_{out}} \quad \boxed{D = 0.4}$$

Check continuous:

$$I_{ob} := \frac{V_{out}}{2 \cdot L \cdot f_s} \cdot D \cdot (1 - D)^2 \quad I_{ob} = 1.8\text{A} \quad \text{This is smaller than the load current, so it is in continuous conduction.}$$

B Given a diode rectifier with a large dc filter capacitor, how does the average dc voltage normally relate to the RMS ac voltage if there is now ac side inductance.

$$V_{do} = \frac{2 \cdot \sqrt{2}}{\pi} \cdot V_s \quad \text{where} \quad v_s(t) = \sqrt{2} \cdot V_s \cdot \sin(\omega \cdot t)$$

$$\frac{2 \cdot \sqrt{2}}{\pi} = 0.9$$

or simplifying:

$$V_{do} = 0.9 \cdot V_s$$

If the ac side inductance is called L_s :

$$V_d = V_{do} - \frac{\omega \cdot L_s}{\pi} \cdot I_{dave}$$

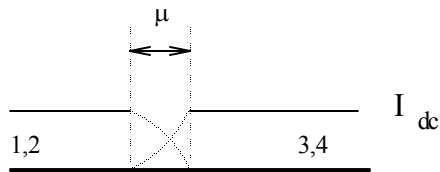
If L_s is 0, then:

$$V_d = 0.9 \cdot V_s$$

Problem 4: Answer the following questions.

(a) What does the commutation overlap angle represent?

The commutation overlap angle (μ or u) represents the impact of the ac side inductance on the transition (or commutation) from one pair of diode to the next in the cycle. If the circuit is in continuous conduction, the current through the ac side inductor will not be zero when the transition occurs. As a result, the current in the inductor will need to go to zero. At the same time the current in the other inductor will be ringing up.



(b) What must be present in the circuit for commutation overlap to occur?

AC side inductance and enough dc side inductance to bring the circuit nearly to continuous conduction.

(c) Will there be commutation overlap if the diode current goes to zero before $\theta = 180\text{deg}$?
Explain

No. Commutation overlap only occurs when the current through the diode needs to be forced to zero (along with the inductor current) at the voltage zero crossing.

(d) How does commutation overlap impact the dc voltage? Explain

The dc voltage is reduced as follows:

$$V_{do} = 0.9 \cdot V_s$$

$$V_d = V_{do} - \frac{\omega \cdot L_s}{\pi} \cdot I_{dave}$$